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High-efficiency filters and filter media for removing particles in air —

Part 4:

Test method for determining leakage of filter elements — Scan method

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 29463-4 was prepared by Technical Committee ISO/TC 142, Cleaning equipment for air and other gases.

ISO 29463 consists of the following parts, under the general title High-efficiency filters and filter media for removing particles in air.

- (standards.iteh.ai) Part 1: Classification, performance, testing and marking
- Part 2: Aerosol production, measuring equipment, particle-counting statistics
- 7558a56d6d58/iso-29463-4-2011 Part 3: Testing flat sheet filter media
- Part 4: Test method for determining leakage of filter element Scan method
- Part 5: Test method for filter elements

Introduction

ISO 29463 (all parts) is derived from EN 1822 (all parts) with extensive changes to meet the requests from non-EU p-members. It contains requirements, fundamental principles of testing and the marking for high-efficiency particulate air filters with efficiencies from 95 % to 99,999 995 % that can be used for classifying filters in general or for specific use by agreement between users and suppliers.

ISO 29463 (all parts) establishes a procedure for the determination of the efficiency of all filters on the basis of a particle counting method using a liquid (or alternatively a solid) test aerosol, and allows a standardized classification of these filters in terms of their efficiency, both local and overall efficiency, which actually covers most requirements of different applications. The difference between ISO 29463 (all parts) and other national standards lies in the technique used for the determination of the overall efficiency. Instead of mass relationships or total concentrations, this technique is based on particle counting at the most penetrating particle size (MPPS), which is, for micro-glass filter mediums, usually in the range of 0,12 µm to 0,25 µm. This method also allows testing ultra-low penetration air filters, which was not possible with the previous test methods because of their inadequate sensitivity. For membrane filter media, separate rules apply, and they are described in ISO 29463-5:2011, Annex B. Although no equivalent test procedures for testing filters with charged media is prescribed, a method for dealing with these types of filters is described in ISO 29463-5:2011, Annex C. Specific requirements for test method, frequency, and reporting requirements can be modified by agreement between supplier and customer. For lower efficiency filters (group H, as described below), alternate leak test methods described in Annex A of this part of ISO 29463 can be used by specific agreement between users and suppliers, but only if the use of these other methods is clearly designated in the filter markings as described in Annex A of this part of ISO 29463.h.ai)

There are differences between ISO 29463 (all parts) and other normative practices common in several countries. For example, many of these rely on total aerosol concentrations rather than individual particles. For information, a brieft summary's of athese g/methods is and 42 their 9 dreference 73 standards are provided in ISO 29463-5:2011, Annex A. 7558a56d6d58/iso-29463-4-2011

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High-efficiency filters and filter media for removing particles in air —

Part 4:

Test method for determining leakage of filter elements — Scan method

1 Scope

This part of ISO 29463 specifies the test procedure of the "scan method", considered to be the reference method, for determining the leakage of filter elements. It is applicable to filters ranging from classes ISO 35 H to ISO 75 U. It also describes the other normative methods, the oil thread leak test (see Annex A) and the photometer leak test (see Annex B), applicable to classes ISO 35 H to ISO 45 H HEPA filters, and the leak test with solid PSL aerosol (see Annex E). It is intended for use in conjunction with ISO 29463-1, ISO 29463-2, ISO 29463-3 and ISO 29463-5. STANDARD PREVIEW

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Normative references 2

The following referenced documents are indispensable for the application of this document. For dated references, only the tredition cited applies. Fordundated references, the latest edition of the referenced document (including any amendments) applies 158/iso-29463-4-201

ISO 5167-1, Measurement of fluid flow by means of pressure differential devices inserted in circular crosssection conduits running full — Part 1: General principles and requirements

ISO 29463-1:2011, High-efficiency filters and filter media for removing particles in air — Part 1: Classification, performance, testing and marking

ISO 29463-2:2011, High-efficiency filters and filter media for removing particles in air — Part 2: Aerosol production, measuring equipment, particle-counting statistics

ISO 29463-3, High-efficiency filters and filter media for removing particles in air — Part 3: Testing flat sheet filter media

ISO 29463-5:2011, High-efficiency filters and filter media for removing particles in air — Part 5: Test method for filter elements

ISO 29464¹), Cleaning equipment for air and other gases — Terminology

¹⁾ To be published.

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 29463-1, ISO 29463-2, ISO 29463-3, ISO 29463-5, ISO 29464 and the following apply.

3.1

sampling duration

time period during which the particles in the sample are counted upstream and downstream

3.2

total particle count method

particle counting method in which the total number of particles in a certain sample volume is determined without classification according to size

EXAMPLE By using a condensation nucleus counter.

3.3

particle counting and sizing method

particle counting method which allows both the determination of the number of particles and also the classification of the particles according to size

EXAMPLE By using an optical particle counter.

3.4

particle flow rate

number of particles that are measured or that flow past a specified cross-section per unit time

3.5

36

particle flow distribution

distribution of the particle flow over a plane at right angles to the direction of flow

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aerosol photometer

light-scattering airborne particle mass concentration measuring apparatus, which uses a forward-scatteringlight optical chamber to make measurements

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Principle 4

For most high-efficiency filter applications, a leak-free filter is essential. The reference leakage test serves to test the filter element for local penetration values and determine whether it exceeds permissible levels (see ISO 29463-1). For group H filters, alternatives to the reference scan method provide equivalent filter leakage determination and are described as alternate methods in Annexes A, B, E and F. Although not considered equivalent, the particle count method using 0,3 µm to 0,5 µm PSL given in Annex F may be used instead of the oil thread method (see Annex A).

For leakage testing, the test filter is installed in the mounting assembly and subjected to a test airflow corresponding to the nominal airflow rate. After measuring the pressure differential at the nominal air flow volume flow rate, the filter is purged and the test aerosol produced by the aerosol generator is mixed with the prepared test air along a mixing duct, so that it is spread homogeneously over the cross-section of the duct.

The particle flow rate on the downstream side of the test filter is smaller than the particle flow rate reaching the filter on the upstream side by the mean penetration factor.

The manufacturing irregularities of the filter media or leaks lead to a variation of the particle flow rate over the filter face area. In addition, leaks at the boundary areas and within the components of the test filter (sealant, filter frame, seal of the filter mounting assembly) can lead locally to an increase in the particle flow rate on the downstream side of the test filter.

For the leakage test, the particle flow distribution shall be determined on the downstream side of the filter in order to check where the limit values are exceeded. The coordinates of these positions shall be recorded.

The scanning tracks shall also cover the area of the filter frame, the corners, the sealant between filter frame and the gasket, so that possible leaks in these areas can also be detected. It is advisable to scan filters for leaks with their original gasket mounted and in the same mounting position and airflow direction as they are installed on site.

In order to measure the downstream particle flow distribution, a probe with defined geometry shall be used on the downstream side to take a specified partial flow as sample. From this partial flow, a sample volume flow rate shall be directed to a particle counter, which counts the particles and displays the results as a function of time. During the testing, the probe moves at a defined speed in adjoining or overlapping tracks without gaps (see C.3.2 and C.3.3) close to the downstream side of the filter element. The measuring period for the downstream particle flow distribution can be shortened by using several measuring systems (partial flow extractors/particle counters) operating in parallel.

The measurement of the coordinates of the probe, a defined probe speed, and measurement of the particle flow rate at sufficiently short intervals allow the localization of leaks. In a further test step, the local penetration shall be measured at this position using a stationary probe.

The leakage tests shall always be conducted using MPPS particles (see ISO 29463-3), except for filters with membrane medium in accordance with Annex E. The size distribution of the aerosol particles can be checked using a particle size analysis system (for example, a differential mobility particle sizer, DMPS).

The leakage testing can be carried out using either a mono-disperse or poly-disperse test aerosol. It shall be ensured that the mean particle diameter corresponds to the most penetrating particle size (MPPS) particle diameter, at which the filter medium has its minimum efficiency.

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When testing with a mono-disperse aerosol, the total particle counting method may be used with a condensation particle counter (CPC) or an optical particle counter (OPC; e.g. a laser particle counter).

When using a poly-disperse aerosol, an optical particle counter that counts the particles and measures their size distribution shall be used.

5 Test filter

A test filter shall be used for the leak testing that does not show any visible signs of damage or other irregularities and that can be sealed in position and subjected to air flow in accordance with requirements. The temperature of the test filter during the tests shall correspond to the temperature of the test air. The test filter element shall be handled with care and shall be clearly and permanently marked with the following details:

- a) designation of the test filter element;
- b) upstream side of the filter element.

6 Test apparatus

6.1 Set-up of the test apparatus

Figure 1 shows the set-up of the test apparatus. This layout is valid for tests with a mono-disperse or with a poly-disperse aerosol. The only differences between these lie in the technique used to measure the particles and the way the aerosol is generated.



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Key

- 1 pre-filter for the test air
- 2 fan with speed regulator
- 3 air heater
- 4 aerosol inlet in the duct
- 5 aerosol generator with conditioning of supply air and aerosol flow regulator
- 6 measurement of atmospheric pressure, temperature and relative humidity
- 7 upstream side mixing section
- 8 sampling point for upstream particle counting
- 9 dilution system (optional)
- 10 particle counter, upstream
- 11 sheath flow (optional)
- 12 test filter
- 13 sampling point and partial flow extraction, downstream
- 14 traversing system for probe
- 15 volume flow rate measurement
- 16 particle counter, downstream
- 17 computer for control and data storage
- 18 measuring system to check the test aerosol
- 19 measurement of differential pressure

Figure 1 — Diagram of test apparatus



An example of a test rig, without particle measuring equipment, is shown in Figure 2.

- 15 sampling point for particle size analysis
- 16 sampling point, upstream
- 17 high-efficiency air filter for the sheath air
- 18 measurement of pressure drop
- 19 measurement of sheath air speed
- 20 test filter
- 21 flow equalizer for the sheath airflow
- 22 filter mounting assembly
- 23 screening (linked to the filter mounting assembly during the testing)
- 24 traversing probe arm with downstream sampling probe
- 25 probe traversing system
- 26 downstream sampling point

Figure 2 — Test duct for scan testing

The basic details for the generation and neutralization of the aerosol, together with the details of suitable types of equipment and detailed descriptions of measuring instruments needed for the testing, are given in ISO 29463-2.

6.2 Test duct

6.2.1 Test air conditioning

The test air conditioning unit contains the equipment required to condition the test airflow (see Clause 7).

The test airflow shall be so prepared that it is in accordance with Clause 7 and does not exceed the limit values specified during the course of the efficiency testing.

6.2.2 Adjustment of the volume flow rate

It shall be possible by means of a suitable provision (e.g. changes to the speed of the fan, or by dampers) to produce the volume flow rate with a reproducibility of ± 3 %. The nominal volume flow rate shall then remain in this range throughout the testing.

6.2.3 Measurement of the volume flow rate

The volume flow rate shall be measured using a standardized or calibrated method (e.g. measurement of the pressure drop using standardized damper equipment such as orifice plates, nozzles, Venturi tubes in accordance with ISO 5167-1).

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The limit error of measurement shall not exceed 5 % of the measured value.

6.2.4 Aerosol mixing duct

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The aerosol input and the mixing duct (see example in Figure 2) shall be so constructed that the aerosol concentration measured at individual points of the duct cross-section directly in front of the test filter does not deviate by more than 10 % from the mean value obtained from at least 10 measuring points spread evenly over the duct cross-section.

6.2.5 Test filter mounting assembly

The test filter mounting assembly shall ensure that the test filter can be sealed and subjected to flow in accordance with requirements. It shall not obstruct any part of the media area of the filter.

It is advisable to scan filters for leaks in the same mounting position and airflow direction as they are installed on site.

6.2.6 Measuring points for the pressure difference

The measuring points for pressure shall be so arranged that the mean value of the difference between static pressure in the upstream flow and the pressure of the surrounding air can be measured. The plane of the pressure measurements shall be positioned in a region of uniform flow.

In rectangular or square test ducts, smooth holes with a diameter of 1 mm to 2 mm for the pressure measurements shall be bored in the middle of the duct walls, normal to the direction of flow. The four measurement holes shall be interconnected with a circular pipe.

6.2.7 Sampling, upstream

Samples are taken upstream by means of one or more sampling probes in front of the test filter. The probe diameter shall be chosen such that, at an average flow velocity, isokinetic conditions pertain at the given volume flow rate for the sample. Sampling errors that arise due to higher or lower flow velocities in the duct can be disregarded due to the small size of the particles in the test aerosol. The tubing connections to the particle counter shall be as short as possible.

The sampling shall be representative, i.e. the aerosol concentration measured from the sample shall not deviate by more than 10 % from the mean value determined in accordance with 6.2.4.

The mean aerosol concentrations determined at the upstream and downstream sampling points without the test filter in position shall not differ from each other by more than 5 %.

6.2.8 Screening

The downstream side of the test filter shall be completely screened from impurities in the surrounding air. Furthermore, for the correct detection and localization of leaks in the edges of the filter, in the gasket, the filter frame or the sealant, the particles emitted in these sections shall be swept away from the section that is covered by scanning. This can be achieved, for example, if the outer sides of the filter frame are enclosed by a shrouding flow of particle-free air flowing in the downstream direction.

The scanning tracks shall also cover the area of the filter frame, the corners, and the sealant between filter frame and the gasket so that possible leaks in these areas are detected. A validation of the test rig shall be performed to verify that leaks in these areas are detected with the same probability and sensitivity as media leaks, being located in the middle of the filter DARD PREVIEW

6.3 Scanning assembly (standards.iteh.ai)

In addition to the automated testing for leaks, manual scanning is also permitted, provided that there is adherence to the most important parameters for the test procedure.

However, when the probe is moved manually, it is not possible to avoid irregularities, since the movement over the filter surface cannot be smooth and even. As a result, quantitative assessments are usually possible only to a limited extent, if at all. Furthermore, it is extremely time-consuming to keep a record of the coordinates of leaks and particularly to evaluate the particle counts.

The remainder of 6.3 describes an automatic scanning apparatus.

6.3.1 Sampling — Downstream

The sampling conditions affect the local resolution for the determination of the particle flow distribution on the downstream side. In order to ensure the comparability of the measurements for the local value of the penetration, the sampling shall be carried out under standardized conditions.

The geometry of the probe aperture may be rectangular or circular. The relationship between the sides of a rectangular probe shall not exceed 15 to 1. The inlet area of the probe shall be $9 \text{ cm}^2 \pm 1 \text{ cm}^2$. The volume flow rate in the probe shall be chosen so that the speed at the probe aperture does not differ by more than 25 % from the face velocity of the filter (see C.5).

If the probes have a rectangular aperture, then the measuring time can be shortened by using several probes next to each other (for several particle counters).

The probe shall be positioned at a distance of 10 mm to 50 mm from the downstream face of the filter element.

For specially constructed filter forms and extremely high face velocities, it is permissible to deviate from the dimensional requirements specified here. However, it is then possible to arrive at only a conditional determination of the local efficiency within the meaning of this part of ISO 29463.

The alternative method of testing with the aerosol photometer is found in Annex B.