SLOVENSKI STANDARD
SIST ISO 899-2:1996

01-junij-1996

Polimerni materiali - Določanje lezenja - 2. del: Lezenje pri tritočkovni upogibni obremenitvi

Plastics -- Determination of creep behaviour -- Part 2: Flexural creep by three-point loading

Plastiques -- Détermination du comportement au fluage -- Partie 2: Fluage en flexion par mise en charge en trois points

Ta slovenski standard je istoveten z: ISO 899-2:1993

ICS:

83.080.01	Polimerni materiali na splošno	Plastics in general

SIST ISO 899-2:1996 en

INTERNATIONAL STANDARD

ISO 899-2

First edition
1993-12-15

Plastics — Determination of creep behaviour —

Part 2:
Flexural creep by three-point loading

Plastiques — Détermination du comportement au fluage —
Partie 2: Fluage en flexion par mise en charge en trois points

Reference number
ISO 899-2:1993(E)

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

International Standard ISO 899-2 was prepared by Technical Committee ISO/TC 61, *Plastics*, Sub-Committee SC 2, *Mechanical properties*.

Together with ISO 899-1, it cancels and replaces ISO 899:1981 and ISO 6602:1985, which have been technically revised.

ISO 899 consists of the following parts, under the general title *Plastics — Determination of creep behaviour*:

— *Part 1: Tensile creep*

— *Part 2: Flexural creep by three-point loading*

Annexes A and B of this part of ISO 899 are for information only.

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Printed in Switzerland

Plastics — Determination of creep behaviour —

Part 2:
Flexural creep by three-point loading

1 Scope

1.1 This part of ISO 899 specifies a method for determining the flexural creep of plastics in the form of standard test specimens under specified conditions such as those of pretreatment, temperature and humidity. It applies only to a simple freely supported beam loaded at mid-span (three-point-loading test).

1.2 The method is suitable for use with rigid and semi-rigid non-reinforced, filled and fibre-reinforced plastics materials (see ISO 472 for definitions) in the form of rectangular bars moulded directly or cut from sheets or moulded articles.

NOTE 1 The method may be unsuitable for certain fibre-reinforced materials due to differences in fibre orientation.

1.3 The method is intended to provide data for engineering-design and research and development purposes.

1.4 Flexural creep may vary significantly with differences in specimen preparation and dimensions and in the test environment. The thermal history of the test specimen can also have profound effects on its creep behaviour (see annex A). Consequently, when precise comparative results are required, these factors must be carefully controlled.

1.5 If flexural-creep properties are to be used for engineering-design purposes, the plastics materials should be tested over a broad range of stresses, times and environmental conditions.

1.6 The method may not be suitable for determining the flexural creep of rigid cellular plastics (attention is drawn in this respect to ISO 1209-1:1990, *Cellular plastics, rigid — Flexural tests — Part 1: Bending test*, and ISO 1209-2:1990, *Cellular plastics, rigid — Flexural tests — Part 2: Determination of flexural properties*).

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this part of ISO 899. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this part of ISO 899 are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 178:1993, *Plastics — Determination of flexural properties.*

ISO 291:1977, *Plastics — Standard atmospheres for conditioning and testing.*

ISO 472:1988, *Plastics — Vocabulary.*

3 Definitions

For the purposes of this part of ISO 899, the definitions given in ISO 472 and the following definitions apply.

3.1 creep: The increase in strain with time when a constant stress is applied.

3.2 flexural stress, σ**:** The surface stress in the mid-span section of the test specimen. It is calculated from the relationship given in 7.1.2.

3.3 deflection, s_t**:** The distance, in millimetres, through which the top or bottom surface of the test specimen at mid-span deviates, during flexure, from its position before application of the test load to its position at time t.

3.4 flexural-creep strain, ε_t**:** The strain at the surface of the test specimen produced by a stress at any given time t during a creep test, calculated in accordance with 7.1.3. It is expressed as a dimensionless ratio or as a percentage.

3.5 flexural-creep modulus, E_t**:** The ratio of flexural stress to flexural-creep strain, calculated as in 7.1.1.

3.6 isochronous stress-strain curve: A Cartesian plot of stress versus creep strain, at a specific time after application of the test load.

3.7 time to rupture: The period of time which elapses between the point in time at which the specimen is fully loaded and the rupture point.

3.8 creep-strength limit: That initial stress which will just cause rupture ($\sigma_{B,t}$) or will produce a specified strain ($\sigma_{\varepsilon,t}$) at a specified time t, at a given temperature and relative humidity.

4 Apparatus

4.1 Test rack, comprising a rigid frame with two supports, one for each end of the test specimen, the distance between the supports being adjustable to (16 ± 1) times the thickness (height) of the specimen (see figure 1) for normal specimens or greater than 17 times the thickness (height) of the specimen for very thick, unidirectional specimens (see 6.2). The test rack shall be level, and sufficient space shall be allowed below the specimen for the specimen to flex under dead-weight loading at mid-span.

The radius R_1 of the loading edge and the radius R_2 of the supports shall conform to the values given in table 1.

Table 1

Values in millimetres

Thickness of test specimen	Radius of loading edge R_1	Radius of supports R_2
⩽ 3	5 ± 0,1	2 ± 0,2
> 3	5 ± 0,1	5 ± 0,2

4.2 Loading system, capable of ensuring that the load is applied smoothly, without causing transient overloading, and that the load is maintained to within ± 1 % of the desired load. In creep-to-rupture tests, provision shall be made to prevent any shocks which occur at the moment of rupture being transmitted to adjacent loading systems. The loading mechanism shall allow rapid, smooth and reproducible loading.

4.3 Deflection-measuring device, comprising any contactless or contact device capable of measuring the deflection of the specimen under load without influencing the specimen behaviour by mechanical effects (e.g. undesirable deformations, notches), other physical effects (e.g. heating of the specimen) or chemical effects. The accuracy of the deflection-measuring device shall be within ± 1 % of the final deflection.

4.4 Time-measurement device, accurate to 0,1 %.

4.5 Micrometer, reading to 0,01 mm or closer, for measuring the thickness and width of the test specimen.

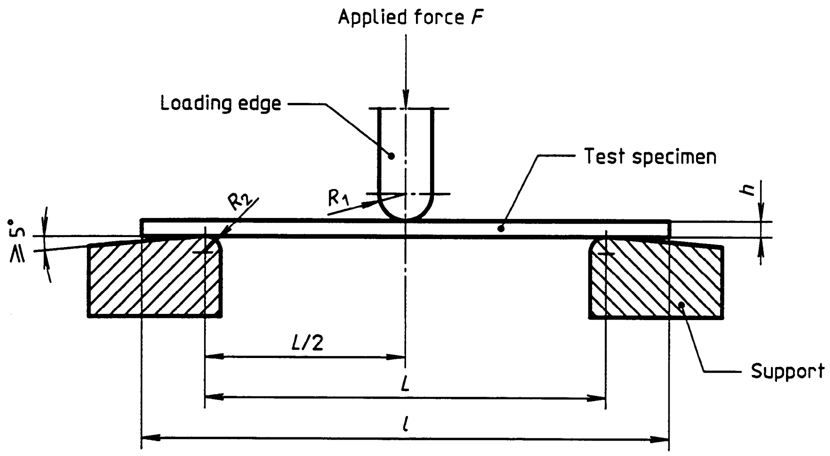

Figure 1 — Characteristics of flexural-creep apparatus

4.6 Vernier calipers, accurate to 0,1 % of the span between the test supports or better, for determining the span.

5 Test specimens

Use test specimens of the same shape and dimensions as specified for the determination of flexural properties (see ISO 178).

6 Procedure

6.1 Conditioning and test atmosphere

Condition the test specimens as specified in the International Standard for the material under test. In the absence of any information on conditioning, use the most appropriate set of conditions specified in ISO 291, unless otherwise agreed upon by the interested parties.

NOTE 2 The creep behaviour will be affected not only by the thermal history of the specimen under test, but also by the temperature and (where applicable) humidity used in conditioning.

Conduct the test in the same atmosphere as used for conditioning, unless otherwise agreed upon by the interested parties, e.g. for testing at elevated or low temperatures. Ensure that the variation in temperature during the duration of the test remains within ± 2 °C.

6.2 Measurement of test-specimen dimensions and distance between supports

Measure the dimensions of the conditioned test specimens.

For normal test specimens, adjust the distance L between the test-specimen supports to

$$(16 \pm 1)h$$

where h is the thickness of the specimen.

In the case of very thick, unidirectional fibre-reinforced test specimens, a distance between the supports may be adjusted to a value $> 17h$ if necessary to avoid delamination in shear.

Measure the distance between the supports to within ± 0,5 %.

6.3 Mounting the test specimens

Mount a conditioned and measured specimen symmetrically with its long axis at right angles to the supports and set up the deflection-measuring device as required.

6.4 Selection of stress value

Select a stress value appropriate to the application envisaged for the material under test, and calculate, using the equation given in 7.1.2, the test load to be applied to the test specimen.

Choose the stress such that the deflection is not greater than 0,1 times the distance between the supports at any time during the test.

6.5 Loading procedure

6.5.1 Preloading

When it is necessary to preload the test specimen prior to increasing the load to the test load, take care to ensure that the preload does not influence the test results. Do not apply the preload until the temperature and humidity of the test specimen (positioned in the test apparatus) correspond to the test conditions.

Set the deflection-measuring device to zero after application of the preload; the preload shall act during the whole duration of the test.

6.5.2 Loading

Load the test specimen progressively so that full loading of the test specimen is reached between 1 s and 5 s after the beginning of the application of the load. Use the same rate of loading for each of a series of tests on one material.

Take the total load (including the preload) to be the test load.

6.6 Deflection-measurement schedule

Record the point in time at which the specimen is fully loaded as $t = 0$. Unless the deflection is automatically and/or continuously recorded, choose the times for making individual measurements as a function of the creep curve obtained from the particular material under test. It is preferable to use the following measurement schedule:

1 min, 3 min, 6 min, 12 min and 30 min;

1 h, 2 h, 5 h, 10 h, 20 h, 50 h, 100 h, 200 h, 500 h, 1 000 h, etc.

If discontinuities are suspected or encountered in the creep-strain versus time plot, take readings more frequently than recommended above.

6.7 Time measurement

Measure, to within ± 0,1 % or ± 2 s (whichever is the less severe tolerance), the total time which has elapsed up to each creep measurement.

6.8 Temperature and humidity control

Unless temperature and relative humidity (where applicable) are recorded automatically, record them at the beginning of the test and then at least three times a day initially. When it has become evident that the conditions are stable within the specified limits, they may be checked less frequently.

7 Expression of results

7.1 Method of calculation

7.1.1 Calculate the flexural-creep modulus E_t, expressed in megapascals, at each of the selected measurement times using the following equation:

$$E_t = \frac{L^3 \cdot F}{4b \cdot h^3 \cdot s_t}$$

where

L is the distance, in millimetres, between the test-specimen supports;

F is the applied force, in newtons;

b is the width, in millimetres, of the test specimen;

h is the thickness (height), in millimetres, of the test specimen;

s_t is the deflection, in millimetres, at mid-span at time t.

7.1.2 Calculate the flexural stress σ, expressed in megapascals, using the following equation:

$$\sigma = \frac{3F \cdot L}{2b \cdot h^2}$$

where

F is the applied force, in newtons;

L is the distance, in millimetres, between the test-specimen supports;

b is the width, in millimetres, of the test specimen;

h is the thickness (height), in millimetres, of the test specimen.

7.1.3 Calculate the flexural creep strain ε_t using the following equation:

$$\varepsilon_t = \frac{6s_t \cdot h}{L^2}$$ as a dimensionless ratio

or

$$\varepsilon_t = \frac{600s_t \cdot h}{L^2}$$ as a percentage

where

s_t is the deflection, in millimetres, at mid-span at time t;

h is the thickness (height), in millimetres, of the test specimen;

L is the distance, in millimetres, between the test-specimen supports.

7.2 Presentation of results

7.2.1 Creep curves

If testing is carried out at different temperatures, the raw data should preferably be presented, for each temperature, as a series of creep curves showing the flexural strain plotted against the logarithm of time,

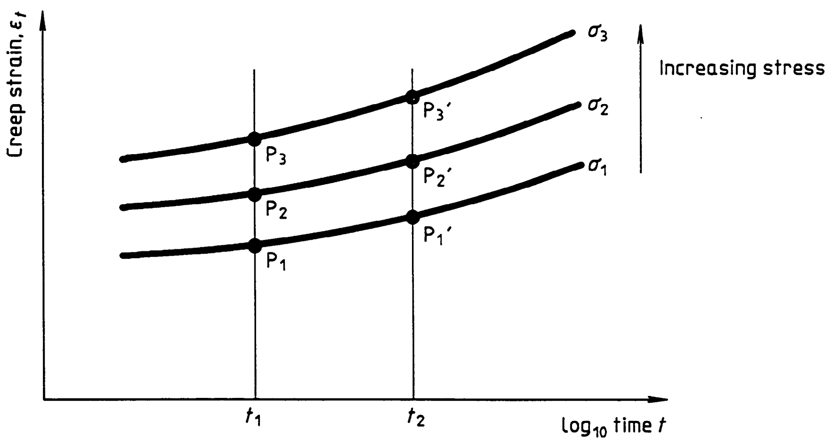

Figure 2 — Creep curves

one curve being plotted for each initial stress used (see figure 2).

The data may also be presented in other ways, e.g. as described in 7.2.2 and 7.2.3, to provide information required for particular applications.

7.2.2 Creep-modulus/time curves

For each initial stress used, the flexural-creep modulus, calculated in accordance with 7.1.1, may be plotted against the logarithm of the time under load (see figure 3).

If testing is carried out at different temperatures, plot a series of curves for each temperature.

7.2.3 Isochronous stress-strain curves

An isochronous stress-strain curve is a Cartesian plot showing how the strain depends on the applied load, at a specific point in time after application of the load. Several curves are normally plotted, corresponding to times under load of 1 h, 10 h, 100 h, 1 000 h, and 10 000 h. Since each creep test gives only one point on each curve, it is necessary to carry out the test at at least three different stresses, and preferably more, to obtain an isochronous curve.

To obtain an isochronous stress-strain curve for a particular time under load (say 10 h) from a series of creep curves as shown in figure 1, read off, from each creep curve, the strain at 10 h, and plot these strain values (x-axis) against the corresponding stress values (y-axis). Repeat the process for other times to obtain a series of isochronous curves (see figure 4).

If testing is carried out at different temperatures, plot a series of curves for each temperature.

7.2.4 Three-dimensional representation

A relationship of the form $\varepsilon = f(t, \sigma)$ exists between the different types of curve (see figures 2 to 4) that can be derived from the raw creep-test data. This relationship can be represented as a surface in a three-dimensional space (see reference [1], annex B).

All the curves that can be derived from the raw creep-test data form part of this surface. Because of the experimental errors inherent in each measurement, the points corresponding to the actual measurements normally do not lie on the curves but just off them.

The surface $\varepsilon = f(t, \sigma)$ can therefore be generated by deriving a number of the curves which form it, but a number of sophisticated smoothing operations are usually necessary. Computer techniques permit this to be done rapidly and reliably.

7.2.5 Creep-to-rupture curves

Creep-to-rupture curves permit the prediction of the time to failure at any stress. They may be plotted as stress against log time (see figure 5) or log stress against log time.

7.3 Precision

The precision of this test method is not known because interlaboratory data are not available. When interlaboratory data are obtained, a precision statement will be added at the next revision.

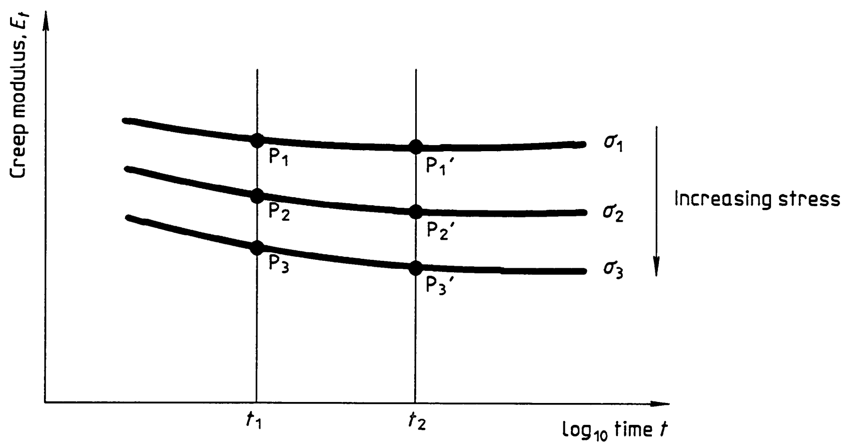

Figure 3 — Creep-modulus/time curves