



Designation: D 790 – 07

Standard Test Methods for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials¹

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This standard has been approved for use by agencies of the Department of Defense.

1. Scope*

1.1 These test methods cover the determination of flexural properties of unreinforced and reinforced plastics, including high-modulus composites and electrical insulating materials in the form of rectangular bars molded directly or cut from sheets, plates, or molded shapes. These test methods are generally applicable to both rigid and semirigid materials. However, flexural strength cannot be determined for those materials that do not break or that do not fail in the outer surface of the test specimen within the 5.0 % strain limit of these test methods. These test methods utilize a three-point loading system applied to a simply supported beam. A four-point loading system method can be found in Test Method D 6272.

1.1.1 *Procedure A*, designed principally for materials that break at comparatively small deflections.

1.1.2 *Procedure B*, designed particularly for those materials that undergo large deflections during testing.

1.1.3 Procedure A shall be used for measurement of flexural properties, particularly flexural modulus, unless the material specification states otherwise. Procedure B may be used for measurement of flexural strength only. Tangent modulus data obtained by Procedure A tends to exhibit lower standard deviations than comparable data obtained by means of Procedure B.

1.2 Comparative tests may be run in accordance with either procedure, provided that the procedure is found satisfactory for the material being tested.

1.3 The values stated in SI units are to be regarded as the standard. The values provided in brackets are for information only.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

NOTE 1—These test methods are not technically equivalent to ISO 178.

¹ These test methods are under the jurisdiction of ASTM Committee D20 on Plastics and are the direct responsibility of Subcommittee D20.10 on Mechanical Properties.

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2. Referenced Documents

2.1 ASTM Standards:²

D 618 Practice for Conditioning Plastics for Testing

D 638 Test Method for Tensile Properties of Plastics

D 883 Terminology Relating to Plastics

D 4000 Classification System for Specifying Plastic Materials

D 4101 Specification for Polypropylene Injection and Extrusion Materials

D 5947 Test Methods for Physical Dimensions of Solid Plastics Specimens

D 6272 Test Method for Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials by Four-Point Bending

E 4 Practices for Force Verification of Testing Machines

E 691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

2.2 ISO Standard:³

ISO 178 Plastics—Determination of Flexural Properties

3. Terminology

3.1 *Definitions*—Definitions of terms applying to these test methods appear in Terminology D 883 and Annex A1 of Test Method D 638.

4. Summary of Test Method

4.1 A bar of rectangular cross section rests on two supports and is loaded by means of a loading nose midway between the supports. A support span-to-depth ratio of 16:1 shall be used unless there is reason to suspect that a larger span-to-depth ratio may be required, as may be the case for certain laminated materials (see Section 7 and Note 7 for guidance).

4.2 The specimen is deflected until rupture occurs in the outer surface of the test specimen or until a maximum strain (see 12.7) of 5.0 % is reached, whichever occurs first.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, http://www.ansi.org.

*A Summary of Changes section appears at the end of this standard.

4.3 Procedure A employs a strain rate of 0.01 mm/mm/min [0.01 in./in./min] and is the preferred procedure for this test method, while Procedure B employs a strain rate of 0.10 mm/mm/min [0.10 in./in./min].

5. Significance and Use

5.1 Flexural properties as determined by these test methods are especially useful for quality control and specification purposes.

5.2 Materials that do not fail by the maximum strain allowed under these test methods (3-point bend) may be more suited to a 4-point bend test. The basic difference between the two test methods is in the location of the maximum bending moment and maximum axial fiber stresses. The maximum axial fiber stresses occur on a line under the loading nose in 3-point bending and over the area between the loading noses in 4-point bending.

5.3 Flexural properties may vary with specimen depth, temperature, atmospheric conditions, and the difference in rate of straining as specified in Procedures A and B (see also [Note 7](#)).

5.4 Before proceeding with these test methods, reference should be made to the ASTM specification of the material being tested. Any test specimen preparation, conditioning, dimensions, or testing parameters, or combination thereof, covered in the ASTM material specification shall take precedence over those mentioned in these test methods. Table 1 in Classification System [D 4000](#) lists the ASTM material specifications that currently exist for plastics.

6. Apparatus

6.1 *Testing Machine*— A properly calibrated testing machine that can be operated at constant rates of crosshead motion over the range indicated, and in which the error in the load measuring system shall not exceed $\pm 1\%$ of the maximum load expected to be measured. It shall be equipped with a deflection measuring device. The stiffness of the testing machine shall be such that the total elastic deformation of the system does not exceed 1% of the total deflection of the test specimen during testing, or appropriate corrections shall be made. The load indicating mechanism shall be essentially free from inertial lag

at the crosshead rate used. The accuracy of the testing machine shall be verified in accordance with Practices [E 4](#).

6.2 *Loading Noses and Supports*—The loading nose and supports shall have cylindrical surfaces. The default radii of the loading nose and supports shall be 5.0 ± 0.1 mm [0.197 ± 0.004 in.] unless otherwise specified in an ASTM material specification or as agreed upon between the interested parties. When the use of an ASTM material specification, or an agreed upon modification, results in a change to the radii of the loading nose and supports, the results shall be clearly identified as being obtained from a modified version of this test method and shall include the specification (when available) from which the modification was specified, for example, Test Method [D 790](#) in accordance with Specification [D 4101](#).

6.2.1 *Other Radii for Loading Noses and Supports*—When other than default loading noses and supports are used, in order to avoid excessive indentation, or failure due to stress concentration directly under the loading nose, they must comply with the following requirements: they shall have a minimum radius of 3.2 mm [$1/8$ in.] for all specimens. For specimens 3.2 mm or greater in depth, the radius of the supports may be up to 1.6 times the specimen depth. They shall be this large if significant indentation or compressive failure occurs. The arc of the loading nose in contact with the specimen shall be sufficiently large to prevent contact of the specimen with the sides of the nose. The maximum radius of the loading nose shall be no more than four times the specimen depth.

6.3 *Micrometers*— Suitable micrometers for measuring the width and thickness of the test specimen to an incremental discrimination of at least 0.025 mm [0.001 in.] should be used. All width and thickness measurements of rigid and semirigid plastics may be measured with a hand micrometer with ratchet. A suitable instrument for measuring the thickness of nonrigid test specimens shall have: a contact measuring pressure of 25 ± 2.5 kPa [3.6 ± 0.36 psi], a movable circular contact foot 6.35 ± 0.025 mm [0.250 ± 0.001 in.] in diameter and a lower fixed anvil large enough to extend beyond the contact foot in all directions and being parallel to the contact foot within 0.005 mm [0.002 in.] over the entire foot area. Flatness of foot and anvil shall conform to the portion of the Calibration section of Test Methods [D 5947](#).

7. Test Specimens

7.1 The specimens may be cut from sheets, plates, or molded shapes, or may be molded to the desired finished dimensions. The actual dimensions used in Section [4.2](#), Calculation, shall be measured in accordance with Test Methods [D 5947](#).

NOTE 2—Any necessary polishing of specimens shall be done only in the lengthwise direction of the specimen.

7.2 *Sheet Materials (Except Laminated Thermosetting Materials and Certain Materials Used for Electrical Insulation, Including Vulcanized Fiber and Glass Bonded Mica)*:

7.2.1 *Materials 1.6 mm [$1/16$ in.] or Greater in Thickness*— For flatwise tests, the depth of the specimen shall be the thickness of the material. For edgewise tests, the width of the specimen shall be the thickness of the sheet, and the depth shall not exceed the width (see Notes [3](#) and [4](#)). For all tests, the

TABLE 1 Flexural Strength

Material	Mean, 10^3 psi	Values Expressed in Units of % of 10^3 psi			
		V_r^A	V_R^B	r^C	R^D
ABS	9.99	1.59	6.05	4.44	17.2
DAP thermoset	14.3	6.58	6.58	18.6	18.6
Cast acrylic	16.3	1.67	11.3	4.73	32.0
GR polyester	19.5	1.43	2.14	4.05	6.08
GR polycarbonate	21.0	5.16	6.05	14.6	17.1
SMC	26.0	4.76	7.19	13.5	20.4

^A V_r = within-laboratory coefficient of variation for the indicated material. It is obtained by first pooling the within-laboratory standard deviations of the test results from all of the participating laboratories: $S_r = [((s_1)^2 + (s_2)^2 + \dots + (s_n)^2)/n]^{1/2}$ then $V_r = (S_r \text{ divided by the overall average for the material}) \times 100$.

^B V_R = between-laboratory reproducibility, expressed as the coefficient of variation: $S_R = \{(S_r^2 + S_L^2)\}^{1/2}$ where S_L is the standard deviation of laboratory means. Then: $V_R = (S_R \text{ divided by the overall average for the material}) \times 100$.

^C r = within-laboratory critical interval between two test results = $2.8 \times V_r$.

^D R = between-laboratory critical interval between two test results = $2.8 \times V_R$.

support span shall be 16 (tolerance ± 1) times the depth of the beam. Specimen width shall not exceed one fourth of the support span for specimens greater than 3.2 mm [$\frac{1}{8}$ in.] in depth. Specimens 3.2 mm or less in depth shall be 12.7 mm [$\frac{1}{2}$ in.] in width. The specimen shall be long enough to allow for overhanging on each end of at least 10 % of the support span, but in no case less than 6.4 mm [$\frac{1}{4}$ in.] on each end. Overhang shall be sufficient to prevent the specimen from slipping through the supports.

NOTE 3—Whenever possible, the original surface of the sheet shall be unaltered. However, where testing machine limitations make it impossible to follow the above criterion on the unaltered sheet, one or both surfaces shall be machined to provide the desired dimensions, and the location of the specimens with reference to the total depth shall be noted. The value obtained on specimens with machined surfaces may differ from those obtained on specimens with original surfaces. Consequently, any specifications for flexural properties on thicker sheets must state whether the original surfaces are to be retained or not. When only one surface was machined, it must be stated whether the machined surface was on the tension or compression side of the beam.

NOTE 4—Edgewise tests are not applicable for sheets that are so thin that specimens meeting these requirements cannot be cut. If specimen depth exceeds the width, buckling may occur.

7.2.2 Materials Less than 1.6 mm [$\frac{1}{16}$ in.] in Thickness—The specimen shall be 50.8 mm [2 in.] long by 12.7 mm [$\frac{1}{2}$ in.] wide, tested flatwise on a 25.4-mm [1-in.] support span.

NOTE 5—Use of the formulas for simple beams cited in these test methods for calculating results presumes that beam width is small in comparison with the support span. Therefore, the formulas do not apply rigorously to these dimensions.

NOTE 6—Where machine sensitivity is such that specimens of these dimensions cannot be measured, wider specimens or shorter support spans, or both, may be used, provided the support span-to-depth ratio is at least 14 to 1. All dimensions must be stated in the report (see also **Note 5**).

7.3 Laminated Thermosetting Materials and Sheet and Plate Materials Used for Electrical Insulation, Including Vulcanized Fiber and Glass-Bonded Mica—For paper-base and fabric-base grades over 25.4 mm [1 in.] in nominal thickness, the specimens shall be machined on both surfaces to a depth of 25.4 mm. For glass-base and nylon-base grades, specimens over 12.7 mm [$\frac{1}{2}$ in.] in nominal depth shall be machined on both surfaces to a depth of 12.7 mm. The support span-to-depth ratio shall be chosen such that failures occur in the outer fibers of the specimens, due only to the bending moment (see **Note 7**). Therefore, a ratio larger than 16:1 may be necessary (32:1 or 40:1 are recommended). When laminated materials exhibit low compressive strength perpendicular to the laminations, they shall be loaded with a large radius loading nose (up to four times the specimen depth to prevent premature damage to the outer fibers).

7.4 Molding Materials (Thermoplastics and Thermosets)—The recommended specimen for molding materials is 127 by 12.7 by 3.2 mm [5 by $\frac{1}{2}$ by $\frac{1}{8}$ in.] tested flatwise on a support span, resulting in a support span-to-depth ratio of 16 (tolerance ± 1). Thicker specimens should be avoided if they exhibit significant shrink marks or bubbles when molded.

7.5 High-Strength Reinforced Composites, Including Highly Orthotropic Laminates—The span-to-depth ratio shall be chosen such that failure occurs in the outer fibers of the specimens and is due only to the bending moment (see **Note 7**). A

span-to-depth ratio larger than 16:1 may be necessary (32:1 or 40:1 are recommended). For some highly anisotropic composites, shear deformation can significantly influence modulus measurements, even at span-to-depth ratios as high as 40:1. Hence, for these materials, an increase in the span-to-depth ratio to 60:1 is recommended to eliminate shear effects when modulus data are required, it should also be noted that the flexural modulus of highly anisotropic laminates is a strong function of ply-stacking sequence and will not necessarily correlate with tensile modulus, which is not stacking-sequence dependent.

NOTE 7—As a general rule, support span-to-depth ratios of 16:1 are satisfactory when the ratio of the tensile strength to shear strength is less than 8 to 1, but the support span-to-depth ratio must be increased for composite laminates having relatively low shear strength in the plane of the laminate and relatively high tensile strength parallel to the support span.

8. Number of Test Specimens

8.1 Test at least five specimens for each sample in the case of isotropic materials or molded specimens.

8.2 For each sample of anisotropic material in sheet form, test at least five specimens for each of the following conditions. Recommended conditions are flatwise and edgewise tests on specimens cut in lengthwise and crosswise directions of the sheet. For the purposes of this test, “lengthwise” designates the principal axis of anisotropy and shall be interpreted to mean the direction of the sheet known to be stronger in flexure. “Crosswise” indicates the sheet direction known to be the weaker in flexure and shall be at 90° to the lengthwise direction.

9. Conditioning

9.1 *Conditioning*—Condition the test specimens at $23 \pm 2^\circ\text{C}$ [$73.4 \pm 3.6^\circ\text{F}$] and $50 \pm 5\%$ relative humidity for not less than 40 h prior to test in accordance with Procedure A of Practice **D 618** unless otherwise specified by contract or the relevant ASTM material specification. Reference pre-test conditioning, to settle disagreements, shall apply tolerances of $\pm 1^\circ\text{C}$ [1.8°F] and $\pm 2\%$ relative humidity.

9.2 *Test Conditions*—Conduct the tests at $23 \pm 2^\circ\text{C}$ [$73.4 \pm 3.6^\circ\text{F}$] and $50 \pm 5\%$ relative humidity unless otherwise specified by contract or the relevant ASTM material specification. Reference testing conditions, to settle disagreements, shall apply tolerances of $\pm 1^\circ\text{C}$ [1.8°F] and $\pm 2\%$ relative humidity.

10. Procedure

10.1 Procedure A:

10.1.1 Use an untested specimen for each measurement. Measure the width and depth of the specimen to the nearest 0.03 mm [0.001 in.] at the center of the support span. For specimens less than 2.54 mm [0.100 in.] in depth, measure the depth to the nearest 0.003 mm [0.0005 in.]. These measurements shall be made in accordance with Test Methods **D 5947**.

10.1.2 Determine the support span to be used as described in Section 7 and set the support span to within 1 % of the determined value.

10.1.3 For flexural fixtures that have continuously adjustable spans, measure the span accurately to the nearest 0.1 mm

[0.004 in.] for spans less than 63 mm [2.5 in.] and to the nearest 0.3 mm [0.012 in.] for spans greater than or equal to 63 mm [2.5 in.]. Use the actual measured span for all calculations. For flexural fixtures that have fixed machined span positions, verify the span distance the same as for adjustable spans at each machined position. This distance becomes the span for that position and is used for calculations applicable to all subsequent tests conducted at that position. See [Annex A2](#) for information on the determination of and setting of the span.

10.1.4 Calculate the rate of crosshead motion as follows and set the machine for the rate of crosshead motion as calculated by Eq 1:

$$R = ZL^2/6d \quad (1)$$

where:

R = rate of crosshead motion, mm [in.]/min,
 L = support span, mm [in.],
 d = depth of beam, mm [in.], and
 Z = rate of straining of the outer fiber, mm/mm/min [in./in./min]. Z shall be equal to 0.01.

In no case shall the actual crosshead rate differ from that calculated using Eq 1, by more than $\pm 10\%$.

10.1.5 Align the loading nose and supports so that the axes of the cylindrical surfaces are parallel and the loading nose is midway between the supports. The parallelism of the apparatus may be checked by means of a plate with parallel grooves into which the loading nose and supports will fit when properly aligned (see [A2.3](#)). Center the specimen on the supports, with the long axis of the specimen perpendicular to the loading nose and supports.

10.1.6 Apply the load to the specimen at the specified crosshead rate, and take simultaneous load-deflection data. Measure deflection either by a gage under the specimen in contact with it at the center of the support span, the gage being mounted stationary relative to the specimen supports, or by measurement of the motion of the loading nose relative to the supports. Load-deflection curves may be plotted to determine the flexural strength, chord or secant modulus or the tangent modulus of elasticity, and the total work as measured by the area under the load-deflection curve. Perform the necessary toe compensation (see [Annex A1](#)) to correct for seating and indentation of the specimen and deflections in the machine.

10.1.7 Terminate the test when the maximum strain in the outer surface of the test specimen has reached 0.05 mm/mm [in./in.] or at break if break occurs prior to reaching the maximum strain (Notes [8](#) and [9](#)). The deflection at which this strain will occur may be calculated by letting r equal 0.05 mm/mm [in./in.] in Eq 2:

$$D = rL^2/6d \quad (2)$$

where:

D = midspan deflection, mm [in.],
 r = strain, mm/mm [in./in.],
 L = support span, mm [in.], and
 d = depth of beam, mm [in.].

NOTE 8—For some materials that do not yield or break within the 5% strain limit when tested by Procedure A, the increased strain rate allowed by Procedure B (see [10.2](#)) may induce the specimen to yield or break, or both, within the required 5% strain limit.

NOTE 9—Beyond 5% strain, this test method is not applicable. Some other mechanical property might be more relevant to characterize materials that neither yield nor break by either Procedure A or Procedure B within the 5% strain limit (for example, Test Method [D 638](#) may be considered).

10.2 Procedure B:

10.2.1 Use an untested specimen for each measurement.

10.2.2 Test conditions shall be identical to those described in [10.1](#), except that the rate of straining of the outer surface of the test specimen shall be 0.10 mm/mm [in./in.]/min.

10.2.3 If no break has occurred in the specimen by the time the maximum strain in the outer surface of the test specimen has reached 0.05 mm/mm [in./in.], discontinue the test (see [Note 9](#)).

11. Retests

11.1 Values for properties at rupture shall not be calculated for any specimen that breaks at some obvious, fortuitous flaw, unless such flaws constitute a variable being studied. Retests shall be made for any specimen on which values are not calculated.

12. Calculation

12.1 Toe compensation shall be made in accordance with [Annex A1](#) unless it can be shown that the toe region of the curve is not due to the take-up of slack, seating of the specimen, or other artifact, but rather is an authentic material response.

12.2 *Flexural Stress* (σ_f)—When a homogeneous elastic material is tested in flexure as a simple beam supported at two points and loaded at the midpoint, the maximum stress in the outer surface of the test specimen occurs at the midpoint. This stress may be calculated for any point on the load-deflection curve by means of the following equation (see Notes [10-12](#)):

$$\sigma_f = 3PL/2bd^2 \quad (3)$$

where:

σ = stress in the outer fibers at midpoint, MPa [psi],
 P = load at a given point on the load-deflection curve, N [lbf],
 L = support span, mm [in.],
 b = width of beam tested, mm [in.], and
 d = depth of beam tested, mm [in.].

NOTE 10—Eq 3 applies strictly to materials for which stress is linearly proportional to strain up to the point of rupture and for which the strains are small. Since this is not always the case, a slight error will be introduced if Eq 3 is used to calculate stress for materials that are not true Hookean materials. The equation is valid for obtaining comparison data and for specification purposes, but only up to a maximum fiber strain of 5% in the outer surface of the test specimen for specimens tested by the procedures described herein.

NOTE 11—When testing highly orthotropic laminates, the maximum stress may not always occur in the outer surface of the test specimen.⁴ Laminated beam theory must be applied to determine the maximum

⁴ For a discussion of these effects, see Zweben, C., Smith, W. S., and Wardle, M. W., "Test Methods for Fiber Tensile Strength, Composite Flexural Modulus and Properties of Fabric-Reinforced Laminates," *Composite Materials: Testing and Design (Fifth Conference)*, ASTM STP 674, 1979, pp. 228–262.

tensile stress at failure. If Eq 3 is used to calculate stress, it will yield an apparent strength based on homogeneous beam theory. This apparent strength is highly dependent on the ply-stacking sequence of highly orthotropic laminates.

NOTE 12—The preceding calculation is not valid if the specimen slips excessively between the supports.

12.3 *Flexural Stress for Beams Tested at Large Support Spans* (σ_f)—If support span-to-depth ratios greater than 16 to 1 are used such that deflections in excess of 10 % of the support span occur, the stress in the outer surface of the specimen for a simple beam can be reasonably approximated with the following equation (see Note 13):

$$\sigma_f = (3PL/2bd^2)[1 + 6(D/L)^2 - 4(d/L)(D/L)] \quad (4)$$

where:

σ_f , P , L , b , and d are the same as for Eq 3, and

D = deflection of the centerline of the specimen at the middle of the support span, mm [in.].

NOTE 13—When large support span-to-depth ratios are used, significant end forces are developed at the support noses which will affect the moment in a simple supported beam. Eq 4 includes additional terms that are an approximate correction factor for the influence of these end forces in large support span-to-depth ratio beams where relatively large deflections exist.

12.4 *Flexural Strength* (σ_{fM})—Maximum flexural stress sustained by the test specimen (see Note 11) during a bending test. It is calculated according to Eq 3 or Eq 4. Some materials that do not break at strains of up to 5 % may give a load deflection curve that shows a point at which the load does not increase with an increase in strain, that is, a yield point (Fig. 1,

Curve B), Y . The flexural strength may be calculated for these materials by letting P (in Eq 3 or Eq 4) equal this point, Y .

12.5 *Flexural Offset Yield Strength*—Offset yield strength is the stress at which the stress-strain curve deviates by a given strain (offset) from the tangent to the initial straight line portion of the stress-strain curve. The value of the offset must be given whenever this property is calculated.

NOTE 14—This value may differ from flexural strength defined in 12.4. Both methods of calculation are described in the annex to Test Method D 638.

12.6 *Flexural Stress at Break* (σ_{fB})—Flexural stress at break of the test specimen during a bending test. It is calculated according to Eq 3 or Eq 4. Some materials may give a load deflection curve that shows a break point, B , without a yield point (Fig. 1, Curve a) in which case $\sigma_{fB} = \sigma_{fM}$. Other materials may give a yield deflection curve with both a yield and a break point, B (Fig. 1, Curve b). The flexural stress at break may be calculated for these materials by letting P (in Eq 3 or Eq 4) equal this point, B .

12.7 *Stress at a Given Strain*—The stress in the outer surface of a test specimen at a given strain may be calculated in accordance with Eq 3 or Eq 4 by letting P equal the load read from the load-deflection curve at the deflection corresponding to the desired strain (for highly orthotropic laminates, see Note 11).

12.8 *Flexural Strain*, ϵ_f —Nominal fractional change in the length of an element of the outer surface of the test specimen at midspan, where the maximum strain occurs. It may be calculated for any deflection using Eq 5:

$$\epsilon_f = 6Dd/L^2 \quad (5)$$

where:

ϵ_f = strain in the outer surface, mm/mm [in./in.],

D = maximum deflection of the center of the beam [in.],

L = support span, mm [in.], and

d = depth, mm [in.].

12.9 *Modulus of Elasticity*:

12.9.1 *Tangent Modulus of Elasticity*—The tangent modulus of elasticity, often called the “modulus of elasticity,” is the ratio, within the elastic limit, of stress to corresponding strain. It is calculated by drawing a tangent to the steepest initial straight-line portion of the load-deflection curve and using Eq 6 (for highly anisotropic composites, see Note 15).

$$E_B = L^3m/4bd^3 \quad (6)$$

where:

E_B = modulus of elasticity in bending, MPa [psi],

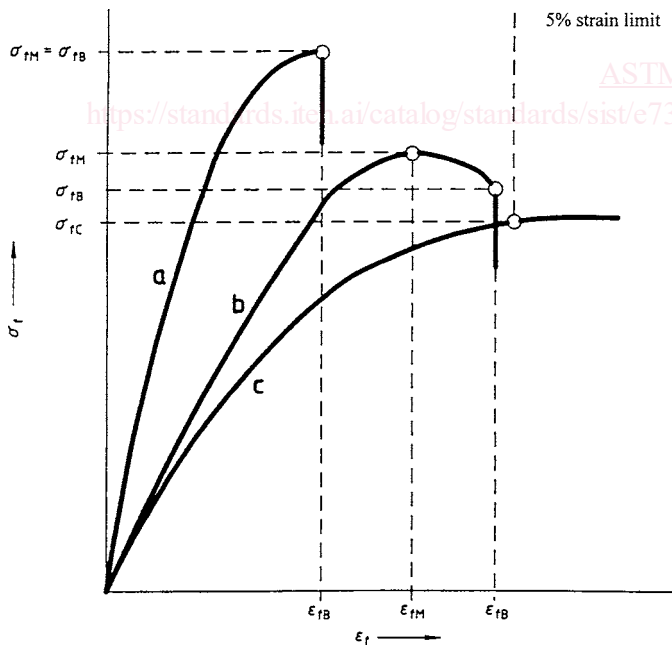
L = support span, mm [in.],

b = width of beam tested, mm [in.],

d = depth of beam tested, mm [in.], and

m = slope of the tangent to the initial straight-line portion of the load-deflection curve, N/mm [lbf/in.] of deflection.

NOTE 15—Shear deflections can seriously reduce the apparent modulus of highly anisotropic composites when they are tested at low span-to-depth ratios.⁴ For this reason, a span-to-depth ratio of 60 to 1 is



NOTE—Curve a: Specimen that breaks before yielding.
 Curve b: Specimen that yields and then breaks before the 5 % strain limit.
 Curve c: Specimen that neither yields nor breaks before the 5 % strain limit.

FIG. 1 Typical Curves of Flexural Stress (σ_f) Versus Flexural Strain (ϵ_f)

recommended for flexural modulus determinations on these composites. Flexural strength should be determined on a separate set of replicate specimens at a lower span-to-depth ratio that induces tensile failure in the outer fibers of the beam along its lower face. Since the flexural modulus of highly anisotropic laminates is a critical function of ply-stacking sequence, it will not necessarily correlate with tensile modulus, which is not stacking-sequence dependent.

12.9.2 Secant Modulus—The secant modulus is the ratio of stress to corresponding strain at any selected point on the stress-strain curve, that is, the slope of the straight line that joins the origin and a selected point on the actual stress-strain curve. It shall be expressed in megapascals [pounds per square inch]. The selected point is chosen at a prespecified stress or strain in accordance with the appropriate material specification or by customer contract. It is calculated in accordance with Eq 6 by letting m equal the slope of the secant to the load-deflection curve. The chosen stress or strain point used for the determination of the secant shall be reported.

12.9.3 Chord Modulus (E_f)—The chord modulus may be calculated from two discrete points on the load deflection curve. The selected points are to be chosen at two prespecified stress or strain points in accordance with the appropriate material specification or by customer contract. The chosen stress or strain points used for the determination of the chord modulus shall be reported. Calculate the chord modulus, E_f using the following equation:

$$E_f = (\sigma_{f2} - \sigma_{f1}) / (\epsilon_{f2} - \epsilon_{f1}) \quad (7)$$

where:

σ_{f2} and σ_{f1} are the flexural stresses, calculated from Eq 3 or Eq 4 and measured at the predefined points on the load deflection curve, and ϵ_{f2} and

ϵ_{f1} are the flexural strain values, calculated from Eq 5 and measured at the predetermined points on the load deflection curve.

12.10 Arithmetic Mean—For each series of tests, the arithmetic mean of all values obtained shall be calculated to three significant figures and reported as the “average value” for the particular property in question.

12.11 Standard Deviation—The standard deviation (estimated) shall be calculated as follows and be reported to two significant figures:

$$s = \sqrt{(\sum X^2 - n\bar{X}^2) / (n - 1)} \quad (8)$$

where:

s = estimated standard deviation,

X = value of single observation,

n = number of observations, and

\bar{X} = arithmetic mean of the set of observations.

13. Report

13.1 Report the following information:

13.1.1 Complete identification of the material tested, including type, source, manufacturer’s code number, form, principal dimensions, and previous history (for laminated materials, ply-stacking sequence shall be reported),

13.1.2 Direction of cutting and loading specimens, when appropriate,

13.1.3 Conditioning procedure,

13.1.4 Depth and width of specimen,

13.1.5 Procedure used (A or B),

13.1.6 Support span length,

13.1.7 Support span-to-depth ratio if different than 16:1,

13.1.8 Radius of supports and loading noses, if different than 5 mm. When support and/or loading nose radii other than 5 mm are used, the results shall be identified as being generated by a modified version of this test method and the referring specification referenced as to the geometry used.

13.1.9 Rate of crosshead motion,

13.1.10 Flexural strain at any given stress, average value and standard deviation,

13.1.11 If a specimen is rejected, reason(s) for rejection,

13.1.12 Tangent, secant, or chord modulus in bending, average value, standard deviation, and the strain level(s) used if secant or chord modulus,

13.1.13 Flexural strength (if desired), average value, and standard deviation,

13.1.14 Stress at any given strain up to and including 5 % (if desired), with strain used, average value, and standard deviation,

13.1.15 Flexural stress at break (if desired), average value, and standard deviation,

13.1.16 Type of behavior, whether yielding or rupture, or both, or other observations, occurring within the 5 % strain limit, and

13.1.17 Date of specific version of test used.

14. Precision and Bias ⁵

14.1 **Tables 1 and 2** are based on a round-robin test conducted in 1984, in accordance with Practice **E 691**, involving six materials tested by six laboratories using Procedure A. For each material, all the specimens were prepared at one source. Each “test result” was the average of five individual determinations. Each laboratory obtained two test results for each material.

NOTE 16—Caution: The following explanations of r and R (**14.2-14.2.3**) are intended only to present a meaningful way of considering the

⁵ Supporting data are available from ASTM Headquarters. Request RR: D20 – 1128.

TABLE 2 Flexural Modulus

Material	Mean, 10 ³ psi	Values Expressed in units of % of 10 ³ psi			
		V_r^A	V_R^B	r^C	R^D
ABS	338	4.79	7.69	13.6	21.8
DAP thermoset	485	2.89	7.18	8.15	20.4
Cast acrylic	810	13.7	16.1	38.8	45.4
GR polyester	816	3.49	4.20	9.91	11.9
GR polycarbonate	1790	5.52	5.52	15.6	15.6
SMC	1950	10.9	13.8	30.8	39.1

^A V_r = within-laboratory coefficient of variation for the indicated material. It is obtained by first pooling the within-laboratory standard deviations of the test results from all of the participating laboratories: $S_r = [((s_1)^2 + (s_2)^2 + \dots + (s_n)^2) / n]^{1/2}$ then $V_r = (S_r / \bar{S}_r)$ divided by the overall average for the material) $\times 100$.

^B V_R = between-laboratory reproducibility, expressed as the coefficient of variation: $S_R = (S_r^2 + S_L^2)^{1/2}$ where S_L is the standard deviation of laboratory means. Then: $V_R = (S_R / \bar{S}_r)$ divided by the overall average for the material) $\times 100$.

^C r = within-laboratory critical interval between two test results = $2.8 \times V_r$.

^D R = between-laboratory critical interval between two test results = $2.8 \times V_R$.