

SLOVENSKI STANDARD SIST ISO 9705-1:2018

01-september-2018

Nadomešča:

SIST ISO 9705:1995

Preskusi odziva na ogenj - Sobni preskus proizvodov za oblogo zidov in stropov - 1. del: Preskusna metoda za konfiguracijo majhnih prostorov (ISO 9705-1:2016)

Reaction to fire tests -- Room corner test for wall and ceiling lining products -- Part 1: Test method for a small room configuration

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Essais de réaction au feu -- Essai dans le coin d'une pièce pour les produits de revêtement pour murs et plafonds -- Partie 19 Méthode d'essai pour une configuration de petite pièce https://standards.itch.ai/catalog/standards/sist/6238dc56-0c64-46db-a1db-21a5c41cb522/sist-iso-9705-1-2018

Ta slovenski standard je istoveten z: ISO 9705-1:2016

ICS:

13.220.50	Požarna odpornost gradbenih materialov in elementov	Fire-resistance of building materials and elements
91.060.10	Stene. Predelne stene. Fasade	Walls. Partitions. Facades
91.060.30	Stropi. Tla. Stopnice	Ceilings. Floors. Stairs

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INTERNATIONAL STANDARD

ISO 9705-1

First edition 2016-02-15

Reaction to fire tests — Room corner test for wall and ceiling lining products —

Part 1:

Test method for a small room configuration PREVIEW

S Essais de réaction au feu — Essai dans le coin d'une pièce pour les produits de revêtement pour murs et plafonds —

Partie 1: Méthode d'essai pour une configuration de petite pièce

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Reference number ISO 9705-1:2016(E)

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT), see the following URL: Foreword — Supplementary information.

The committee responsible for this document is ISO/TC 92, Fire safety, Subcommittee SC 1, Fire initiation and growth.

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This first edition of 150/9705:13 cancels and replaces 150/9705:1993, which has been technically revised. It also incorporates the Corrigendum 450/9705:1993/Cor 1:1993.

ISO 9705 consists of the following parts, under the general title *Reaction to fire tests* — *Room corner test for wall and ceiling lining products*:

- Part 1: Test method for a small room configuration
- *Part 2: Technical background and guidance* [Technical Report]

Introduction

This part of ISO 9705 is intended to describe the fire behaviour of a product under controlled laboratory conditions.

The test method may be used as part of a fire hazard assessment which takes into account all of the factors which are pertinent to an assessment of the fire hazard of a particular end use.

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Reaction to fire tests — Room corner test for wall and ceiling lining products —

Part 1:

Test method for a small room configuration

WARNING — So that suitable precautions can be taken to safeguard health, the attention of all concerned in fire tests is drawn to the possibility that toxic or harmful gases can be evolved during combustion of test specimens. The test procedures involve high temperatures and combustion processes from ignition to a fully developed room fire. Therefore, hazards can exist for burns, ignition of extraneous objects or clothing. The operators should use protective clothing, helmet, face-shield and equipment for avoiding exposure to toxic gases. Means of extinguishing a fully developed fire should be available.

1 Scope

This part of ISO 9705 specifies the test method to evaluate the reaction of wall and ceiling products to fire when installed at the surface of a small room and exposed directly to a specified ignition source. The test represents a fire scenario which starts under well-ventilated conditions in a corner of a specified room with a single open doorway.

Tests performed in accordance with the method specified in this part of ISO 9705 provide data for the early stages of a fire from ignition up to flashover. The method does not evaluate the fire resistance of products.

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The method is not intended to **evaluate floor-coverings2** This method is not suitable for sandwich panel building systems, pipe insulation and façades for which specific ISO standards (i.e. ISO 13784, ISO 20632 and ISO 13785, respectively) are available.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 13943, Fire safety — Vocabulary

EN 13238, Reaction to fire tests for building products — Conditioning procedures and general rules for selection of substrates

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 13943 and the following apply.

3.1

exposed surface

surface of the product subjected to the heating conditions of the test

3.2

material

single substance or uniformly dispersed mixture

EXAMPLE This includes metal, stone, timber, concrete, mineral fibre, and polymers.

3.3

product

material, composite or assembly about which information is required

3.4

specimen

representative piece of the product which is to be tested together with any substrate or treatment

Note 1 to entry: The specimen may include an air gap.

3.5

wall and ceiling lining product

wall and ceiling products, installed at the surface of a room and exposed directly to a specified ignition source

3.6

flashover

point in the fire history when the sum of the heat release rate from the ignition source and the product reaches 1 000 kW

Note 1 to entry: Heat release rate calculated as a 30-second sliding average, HRR_{smooth}, as given in Annex E.

3.7

Fire Growth Rate

FIGRA

growth rate of the fire during a specified time period RD PREVIEW

3.8

Smoke Growth Rate

SMOGRA

growth rate of the smoke during a specified time period 05-1:2018

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3.9 burning droplets

continuous occurrence of flaming droplets/particles from the specimen for at least 10 s or until a pool fire forms on the floor

4 Principle

The hazard of fire growth is evaluated by the measurement of the rate of heat release of the fire based on calculation of oxygen consumption.

The hazard of reduced visibility is estimated by the measurement of production of light-obscuring smoke.

Phenomena attributed to the fire growth, for example flame spread and emission of burning droplets, are visually documented by photographic and/or video recording.

NOTE If further information is required, measurements, for example of heat flux to the floor, toxic gas species, the gas temperature in the room and the mass flow in and out the doorway, can be performed. See also ISO/TR 9705-2.

5 Fire test room

5.1 Dimensions

The room (see Figure 1) shall consist of four walls at right angles, a floor and a ceiling and shall have the following inner dimensions:

a) length: $3.6 \text{ m} \pm 0.05 \text{ m}$;

b) width: $2.4 \text{ m} \pm 0.05 \text{ m}$;

c) height: $2.4 \text{ m} \pm 0.05 \text{ m}$.

The room shall be placed indoors in an essentially draught free, heated space, large enough to ensure that there is no influence on the test fire. In order to facilitate the mounting of the instruments of the ignition source, the test room may be placed so that the floor can be reached from beneath.

5.2 Doorway

There shall be a doorway in the centre of one of the $2,4 \text{ m} \times 2,4 \text{ m}$ walls and no other wall, floor or ceiling shall have any openings that allow ventilation. The doorway shall have the following dimensions:

a) width: $0.8 \text{ m} \pm 0.01 \text{ m}$;

b) height: $2.0 \text{ m} \pm 0.01 \text{ m}$.

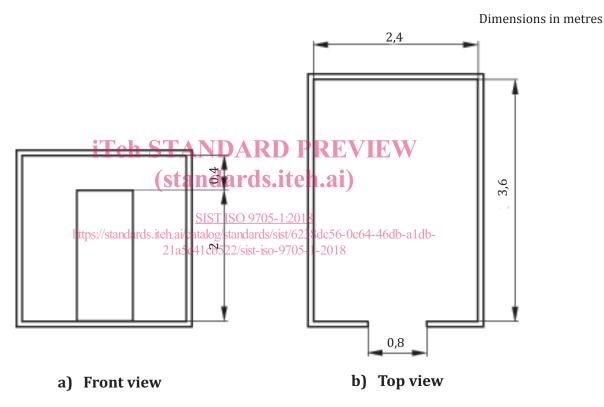


Figure 1 — Fire test room

5.3 Construction material

The test room shall be constructed of non-combustible material with a density of (600 ± 200) kg/m³. The minimum thickness of the construction shall be 20 mm.

6 Ignition source

6.1 General

The ignition source design is specified in Annex A.

The ignition source shall be a propane gas burner having a nominal 170 mm × 170 mm square top surface layer of a porous, inert material. The top portion of the porous material shall be a minimum 45 mm of sand. The construction shall be such that an even gas flow is achieved over the entire opening area.

The burner shall be ignited with a remote-controlled ignition device, for example a pilot burner or a spark igniter. The burner shall be provided with controls for gas supply shut-off if flameout occurs or if there is a gas leak.

Because the propane gas burner consumes relatively large amounts of gas, the attention is therefore drawn to the following warning.

WARNING — All equipment such as tubes, couplings, flowmeters, etc. shall be approved for propane. The installations shall be performed in accordance with existing regulations.

6.2 Location

The burner shall be placed on the floor in a corner opposite to the doorway wall. The top surface of the burner through which the gas is supplied shall be located horizontally, (146 ± 3) mm off the floor, and the burner enclosure shall be in contact with both walls in the corner.

6.3 Gas

The burner shall be supplied with natural grade propane (95 % purity). The gas flow to the burner shall be measured throughout the test with an accuracy of at least ± 3 %. The heat output to the burner shall be controlled within ± 5 % of the prescribed value. Flow rates of gas shall be calculated using a net heat of combustion of propane of 46.4 MJ/kg.

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6.4 Heat output

The net heat output shall be 100 kW during the first 10 min after ignition and then shall be increased to 300 kW for a further 10 min. 21a5c41cb522/sist-iso-9705-1-2018

7 Hood and exhaust duct

The system for collecting the combustion products shall have a capacity and be designed in such a way that all of the combustion products leaving the fire room through the doorway during a test are collected. The system shall not disturb the fire-induced flow in the doorway. The maximum exhaust capacity shall be at least $3.5~{\rm m}^3{\rm s}^{-1}$ at normal pressure and a temperature of $25~{\rm °C}$.

NOTE An example of one design of hood and an exhaust duct is given in Annex C.

8 Instrumentation in the exhaust duct

8.1 General

This Clause specifies minimum requirements for instrumentation in the exhaust duct. Additional information and designs can be found in Annex D.

8.2 Volume flow rate

The volume flow rate in the exhaust duct shall be measured to an accuracy of at least ± 5 %.

The response time of the measurement system to a stepwise change of the duct flow rate shall be a maximum of 3 s at 90 % of the final value.

8.3 Gas analysis

8.3.1 Sampling line

The gas samples shall be taken in the exhaust duct at a position where the combustion products are uniformly mixed. The sampling line shall be made from an inert material which will not influence the concentration of the gas species to be analysed (see Annex D).

8.3.2 Oxygen

The O_2 analyser shall be of the paramagnetic type or equivalent in performance and capable of measuring a range of at least 0 Vol % to 21 Vol % oxygen ($Volume_{02}/Volume_{air}$). The uncertainty of measurement shall be \leq 0,1 Vol % O_2 or better. The stability of the analyser shall be within 0,01 Vol % O_2 over a period of 30 min (measured as recommended in accordance with D.3.2). The output from the analyser and also the data acquisition system shall have a resolution of 0,01 Vol % O_2 or better.

8.3.3 Carbon dioxide

The CO_2 analyser shall be of the IR type or equivalent in performance and capable of measuring a range of at least 0 Vol % to 10 Vol % carbon dioxide. The uncertainty of measurement shall be \leq 0,1 Vol % CO_2 up to 5 Vol % CO_2 and \leq 0,2 Vol % CO_2 from 5 to 10 Vol % CO_2 . The linearity of the analyser shall be 1 % of full scale or better. The output from the analyser and also the data acquisition system shall have a resolution of 0,01 Vol % CO_2 or better.

8.4 Optical density Teh STANDARD PREVIEW (standards.iteh.ai)

8.4.1 General

The optical density of the smoke is determined by measuring the light obscuration with a system consisting of a lamp, lenses, an aperture and a photocell (see Figure 2) or with a laser system as given in Annex H.

8.4.2 Lamp

The lamp shall be of the incandescent filament type and shall operate at a colour temperature of $(2\ 900\ \pm\ 100)$ K. The lamp shall be supplied with stabilized direct current, stable within $\pm 0.5\ \%$ (including temperature, short-term and long-term stability).

8.4.3 Lenses

The lens system shall align the light to a parallel beam with a diameter, *D*, of at least 20 mm.

8.4.4 Aperture

The aperture shall be placed at the focus of the lens L_2 as shown in Figure 2 and it shall have a diameter, d, chosen with regard to the focal length, f, of L_2 so that d/f is less than 0,04. Other solutions to avoid light scattering are allowed.

8.4.5 Detector

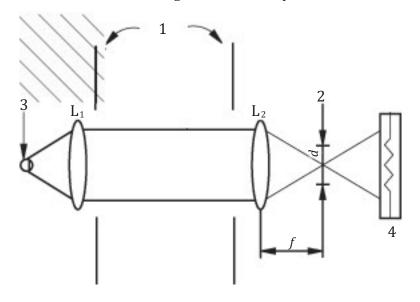
The detector shall have a spectrally distributed response agreeing with the CIE¹, $V(\lambda)$ -function (the CIE photopic curves) to an accuracy of at least ± 5 %.

The detector output shall be linear within 5 % or 0,01 of the measured optical density value, over an output range of at least two decades. A routine to check this requirement is given in $\underline{D.4.2.3}$.

¹⁾ Commission Internationale d'Eclairage.

8.4.6 Location

The light beam shall cross the exhaust duct along its diameter at a position where the smoke is homogenous.



Key

- 1 wall of exhaust duct
- 2 aperture
- 3 lamp
- 4 detector

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Figure 250ptical system

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9 System performance

9.1 System response

9.1.1 Procedure

The delay times and response times of the gas analysis system shall be checked for a stepwise change of the heat output from the burner according to <u>Table 1</u>. The burner shall be placed centrally 3,5 m below the centre line of the duct. Measurements shall be taken every 3 s. The volume flow rate of the exhaust system shall be set to $(2,5 \pm 0,5)$ m³s⁻¹.

Step Number	Time min	Heat output kW
1	0 to 2	0
2	2 to 7	100
3	7 to 12	300
4	12 to 17	100
5	17 to 19	0

Table 1 — Burner heat output profile

9.1.2 Delay times

The delay time of the oxygen analyser is found as the time difference between a 3 K change in the duct temperature and a 0,05 % change in the oxygen concentration. The delay time of the carbon dioxide analyser is found as the time difference between a 3 K change in the duct temperature and a 0,02 % change in the carbon dioxide concentration. Neither delay time shall exceed 30 s. The data shall be corrected on the basis of these delay times before calculating the heat release rate.

9.1.3 Response times

The response times are found as the time between a 10 % and 90 % change in the measured oxygen or carbon dioxide level. The response times shall not exceed 18 s.

9.1.4 Calculations

Based on the unshifted data, calculate:

- a) for each step:
 - 1) t_{gas} , the start time of the step as the time of the first data point at which the propane flow has changed by 100 mg/s in comparison with the mean value in the last 2 min of the previous step;
 - 2) $t_{\rm T}$, the time of the first data point at which the temperature $T_{\rm S}$ has changed 3,0 K in comparison with the mean value in the last 2 min of the previous step;
 - 3) t_{02} , the time of the first data point at which the oxygen concentration has changed 0,05 % in comparison with the mean value in the last 2 min of the previous step;
 - 4) t_{CO2} , the time of the first data point at which the carbon dioxide concentration has changed 0,02 % in comparison with the mean value in the last 2 min of the previous step;
 - 5) $t_{02,10}$ %, the time of the first data point at which the oxygen concentration has reached 10 % of its deflection using the mean values in the last 2 min of the previous and the current step;
 - 6) $t_{02.90}$ %, analogous to $t_{02.10}$ %, however for 90 % instead of 10 % deflection;
 - 7) $t_{\text{CO2,10}}$ %, the time of the first data point at which the carbon dioxide concentration has reached 10 % of its deflection using the mean values in the last 2 min of the previous and the current step;
 - 8) $t_{CO2,90\%}$, analogous to $t_{CO2,10\%}$, however for 90% instead of 10% deflection;
- b) the delay time of the oxygen analyser as the mean of t_{02} $t_{\rm T}$ found for steps 2, 3, 4 and 5;
- c) the delay time of the carbon dioxide analyser as the mean of $t_{\rm CO2}$ $t_{\rm T}$ found for steps 2, 3, 4 and 5;
- d) the response time of the oxygen analyser as the mean of $t_{02.90\%}$ $t_{02.10\%}$ found for steps 2, 3, 4 and 5;
- e) the response time of the carbon dioxide analyser as the mean of $t_{CO2,90\%}$ $t_{CO2,10\%}$ found for steps 2, 3, 4 and 5;

9.2 Daily Check

A calibration test shall be performed prior to each test or continuous test series.

NOTE Formulae for calculations are given in Annex E.

The calibration shall be performed with the burner heat outputs given in <u>Table 1</u>, with the burner placed centrally 3,5 m below the centre line of the duct. Measurements shall be taken every 3 s and shall be started 2 min prior to ignition of the burner. At steady-state conditions, the difference between the mean heat release rate (HRR_{total}) over 1 min (during the time interval between 180 s and 240 s