

## SLOVENSKI STANDARD SIST-TP CEN/TR 14585-3:2018

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Valoviti kovinski cevni sestavi v tlačnih cevovodih - 3. del: Metode načrtovanja

Corrugated metal hose assemblies for pressure applications - Part 3: Design methods

Gewellte Metallschlauchleitungen für Druckanwendungen - Teil 3: Auslegungsverfahren

Tuyauteries métalliques flexibles onduleuses pour applications sous pression - Partie 3: Méthode de conception

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## Corrugated metal hose assemblies for pressure applications - Part 3: Design method

Tuyauteries métalliques flexibles onduleuses pour applications sous pression - Partie 3: Méthode de conception

Gewellte Metallschlauchleitungen für Druckanwendungen - Teil 3: Auslegungsverfahren

This Technical Report was approved by CEN on 25 September 2017. It has been drawn up by the Technical Committee CEN/TC 342.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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## **European foreword**

This document (CEN/TR 14585-3:2017) has been prepared by Technical Committee CEN/TC 342 "Metal hose, hose assemblies, bellows and expansion joints", the secretariat of which is held by SNV.

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#### Introduction

Technical Committee CEN/TC 342 "Metal hose, hose assemblies, bellows and expansion joints" is carrying out a revision of EN 14585-1:2006 and CEN/TR 14585-2:2006 to include calculation methods for the combined structure of hose and braid for:

- pressure resistance;
- fatigue life;
- allowable displacements.

The selection of materials for corrosive environments and the calculation of fluid pressure drops are also being included.

It is appreciated that these studies are ambitious and will involve much new analyses so that this revision will take some time.

Whilst continuing to work on this revision, CEN/TC 342 decided that the key aspects of the calculation method should be circulated as an informative Technical Report CEN/TR 14585-3, which is limited to the pressure resistance of the combined structure of hose and braid. This approach will enable manufacturers and Notified Bodies to use and gain experience of the calculation method and any feedback can be taken into account in the revision of EN 14585, harmonized to the Pressure Equipment Directive 2014/68/EU. Teh STANDARD PREVIEW

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#### 1 Scope

This Technical Report provides guidance on the design of corrugated metal hose assemblies for pressure applications, i.e. maximum allowable pressure PS greater than 0,5 bar. Allowable stresses are consistent with the requirements of the Pressure Equipment Directive 2014/68/EU.

#### 2 Normative references

Not applicable.

#### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in EN ISO 7369 and the following apply.

#### 3.1

#### metal hose assembly

assembly of a corrugated metal hose with its end fittings

Note 1 to entry: In the context of Pressure Equipment Directive [1], a metal hose assembly is a component of piping and not a PED assembly.

#### 3.2

## maximum allowable pressure PSh STANDARD PREVIEW

maximum pressure for which the metal hose assembly is designed

#### 3.3

#### maximum/minimum allowable temperature TSEN/IR 14585-3:2018

maximum and minimum temperature for which the metal hose assembly is designed bad863e5ed73/sist-tp-cen-tr-14585-3-2018

#### 3.4

#### nominal pressure PN

dimensionless alphanumerical designation which is a convenient rounded number commonly used for reference purposes of piping components and stock parts; for this Technical Report PN represents the maximum allowable pressure at 20  $^{\circ}$ C as specified by the metal hose assembly manufacturer

#### 3.5

#### test pressure PT

pressure at which the pressure metal hose assembly is pressure tested (normally at ambient temperature)

#### 3.6

#### main pressure bearing parts

parts, such as corrugated metal hose, braid, pipe ends, the failure of which may result in a sudden discharge of pressure energy

#### 3.7

#### pressure bearing parts

parts, such as swivel nuts, flanges, threaded fittings, that are not main pressure bearing parts defined in 3.6 and the failure of which may not lead to a sudden discharge of pressure energy

#### 3.8

## attachments to pressure parts

parts, such as ferrules, that are directly welded to parts defined in 3.6 or 3.7

#### 3.9

#### other parts

parts, such as external protection, anti-kink device, braid protecting spiral, which are not parts according to  $3.6\ \text{to}\ 3.8$ 

#### 3.10

#### equipment manufacturer

natural or legal person responsible for the values of the parameters PS and TS

Note 1 to entry: This may be the manufacturer or planner of the piping for which the metal hose assembly is designed.

#### 3.11

#### hose manufacturer

natural or legal person responsible for the design and the manufacturing of the corrugated metal hose and/or the metal hose assembly

#### 3.12

#### hydraulic forming (longitudinal welded)

corrugating a tube by pressurizing the inside against external tooling which allows this corrugated tube to be axially shortened during the process

#### 3.13

## roll forming (longitudinal welded) AND ARD PREVIEW

corrugating a tube by rolling from the outside to the inside and allowing or forcing this corrugated tube to be axially shortened during the process ards.iteh.ai

#### 3.14 <u>SIST-TP CEN/TR 14585-3:2018</u>

### helical crest welded (resistance welded)/standards/sist/0d33972c-f35f-4b40-97d6-

profiling a strip, rolling it over helically and finally welding the overlaps

#### 3.15

#### strand

group of parallel wires used for plain braid or wires woven together to form a braided strand

#### 3.16

#### braided braid

braid that is manufactured from previously braided strands

### 4 Symbols and abbreviations

For the purposes of this document, the symbols listed in Table 1 apply.

#### Table 1 — Symbols

Symbol	Description	Unit
Α	elongation at rupture according to EN ISO 6892-1	%
$A_{\rm c}$	cross sectional metal area of one corrugation; see Formula (3a) and 3b)	mm²
$A_{\mathrm{e}}$	hose effective area; see Formula (5)	mm²
$a_w$	Braid wire cross section; see Formula (29)	mm²
$b_{\rm c}$	width of corrugation crest; see Figures 2 a) and 2 b)	mm

Symbol	ymbol Description		
$b_{\rm n}$	nominal width of material (strip) according to EN ISO 9445-1	mm	
$b_{\rm r}$	width of corrugation root; see Figures 2 a) and 2 b)	mm	
$b_{\rm s}$	width of a strand; see Figure 4	mm	
$C_1$ , $C_2$	factors used to determine the calculation coefficients $C_p$ , $C_f$ , $C_d$ ; see Formulae (6) and (7)	_	
$C_{\mathrm{B}}$	braid coverage; see Formula (38)	_	
$C_{\rm p}$ , $C_{\rm f}$ , $C_{\rm d}$	calculation coefficients (see Annex A)	_	
$c_{\rm st}$	stacking factor for crossing braid wires and strands; see Formula (26)	_	
$D_{\mathrm{i}}$	inside diameter of the corrugated metal hose; see Figures 2 a) and 2 b)	mm	
$D_{\mathrm{m}}$	mean diameter of the corrugated metal hose; see Formula (8)	mm	
Do	outside diameter of the corrugated metal hose; see Formulae (9a) and (9b)	mm	
$d_{\mathrm{w}}$	diameter of the braid wire; see Figure 4	mm	
$d_{\mathrm{B}}$	mean diameter of a braid layer; see Formula (30)	mm	
Е	modulus of elasticity of hose material at room temperature/	N/mm² (MPa)	
$E_{t}$	modulus of elasticity of hose material at design temperature	N/mm <sup>2</sup> (MPa)	
е	nominal thickness of hose material; see Figures 2 a) and 2 b)	mm	
$e_{ m p}$	nominal thickness of one ply SIST-TP CEN/TR 14585-3:2018 https://standards.iteh.ai/catalog/standards/sist/0d33972c_f35f_4b40_97d6	mm	
e*	equivalent wall thickness corrected for thinning during forming; see Formula (11)	mm	
$e_{\mathrm{p}}^{*}$	equivalent thickness of one ply with thinning correction; see Formulae (10a) and (10b)	mm	
$F_{\mathrm{p}}$	force due to pressure effect (pressure thrust); see Formula (12)	N	
f	allowable general membrane stress at design temperature; see Table 7	N/mm <sup>2</sup> (MPa)	
$f_{ m T}$	allowable general membrane stress at test conditions; see Table 7	N/mm² (MPa)	
$G_{\sigma}$	degree of load; see 5.5 and Formula (1)	_	
h <sub>s</sub>	thickness of a strand; see Formula (27)	mm	
$K_{ax(1)}$	axial spring rate of one corrugation; see Formula (21)	N/mm	
$K_{\mathrm{f}}$	forming factor; see Formulae (18) and (19)	_	
$k_{\Theta}$	reduction factor for circumferential stress due to braid; see Formula (32)	_	
$k_{ m p,t}$	derating factor for the pressure at operating temperature $t$ ; see 6.3	_	
$l_{\mathrm{B}}$	axial pitch of the braid; see Figure 4 and Formula (24)	mm	
l <sub>c</sub>	active corrugated length of a metal hose	mm	
$n_{ m p}$	number of plies of a corrugated metal hose	_	
$n_{\rm s}$	number of braid strands	_	

Symbol	Description		Unit
$n_{ m w}$	number of wires in one braid strand		_
$P_{1,0}$	pressure resulting in an initial remaining (plastic) elongation of 1 %; see Formula (22)		N/mm² (MPa)
$P_{ m m,b}$	primary meridional bending stress		N/mm² (MPa)
$P_{ m m,m}$	primary meridional membrane stress		N/mm² (MPa)
$P_{\Theta}$	primary circumferential stress		N/mm² (MPa)
<sub>PS</sub> a	maximum allowable pressure		N/mm <sup>2</sup> (MPa)
PT	test pressure		bar
P <sub>t, max</sub>	maximum allowable pressure at of Formula (2)	operating temperature <i>t</i> ; see	bar
q	corrugation length; see Figures 2 a) and	2 b)	mm
$R_1$ to $R_4$	bend radii of hose assemblies; see Table	5	mm
R <sub>eH, t</sub>	minimum specified value of upper yield	strength at design temperature	N/mm² (MPa)
R <sub>m, t</sub>	minimum specified value of tensile stren	ngth at design temperature	N/mm <sup>2</sup> (MPa)
R <sub>m, 20</sub>	minimum specified value of tensile stren	gth at room temperature	N/mm² (MPa)
R <sub>p 0,2, t</sub>	minimum specified value of 0,2 % proof	strength at design temperature	N/mm <sup>2</sup> (MPa)
R <sub>p 1,0, t</sub>	minimum specified value of 1 % proof st	rength at design temperature	N/mm <sup>2</sup> (MPa)
$r_{ m m}$	mean radius of torus at crest and root of U-shaped corrugations; see Figures 2 a) and 2 b) and Formulae (4a) and (4b) - 135f-4b40-97d6-		mm
t	operating temperature	<del>(* 19383-3-2018</del>	°C
t <sub>n</sub>	nominal thickness of the material (strip)		mm
w	corrugation height, see Figures 2 a) and	2 b) and Formula (13)	mm
α	initial braid angle; see Figure 4 and Forn	nula (25)	degree or radian
$oldsymbol{eta}_0$	initial side wall angle of the corrugation;	see Figure 3 and Formula (14)	degree
$\Delta l_{ m el}$	elastic hose elongation due to pressure; see Formula (20)		mm
$\Delta l_{ m pl}$	plastic hose elongation due to pressure; see Formula (46)		mm
η	load carrying efficiency of braid layer; see 7.3.2.4		-
λ	relative plastic elongation; see Formula (46)		-
ν	value of Poisson's ratio for stainless steel of 0,3		-
σ (P)	stress depending on P		N/mm <sup>2</sup> (MPa)
$\sigma_{ m w}$	longitudinal stress in the braid wire; see Formula (39)		N/mm <sup>2</sup> (MPa)
Subscripts		o outside	
0 initial p ply B braid pl plastic			
H hose pr plastic r root			
111000			

Symbol	Descrip	Unit		
t test cond	ition	t temperature		
b bending or burst condition		w wire		
c corrugation or crest		Δ difference		
el elastic		λ relative elongation		
i inside or	running index	Θ circumferential		
m membra	ne, meridional or mean	Σ sum		
n number of or upper summation index				
All pressures for calculation purpose are in N/mm² (MPa).				

#### 5 Materials

#### 5.1 General requirements

Materials for the manufacture of hose assemblies including filler metal should be selected on the basis of their suitability for fabrication, e.g. forming, joining, and for the conditions under which they will be used.

When combining different materials, special care should be taken regarding compatibility with each other.

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#### 5.2 Suitable materials

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Materials suitable for hoses assemblies are given as follows:

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- a) materials suitable for corrugated metal hoses and their temperature limits are given in Table 2;
- bad863e5ed73/sist-tp-cen-tr-14585-3-2018 b) materials suitable for braid, fittings, and additional parts are given in Table 3.

Table 2 — Materials for corrugated metal hoses and their temperature limits

Material		Temperature °C		Dogument		
Type	Number	Steel name	Minimum	Maximum	Document	
	1.4306	X2CrNi19-11	– 273 a	550		
	1.4401	X5CrNiMo17-12-2	- 196 <sup>a</sup>	550		
	1.4404	X2CrNiMo17-12-2	– 273 a	550		
stainless	1.4435	X2CrNiMo18-14-3	– 273 a	550	EN 10000 F	
austenitic steels	1.4539	X1NiCrMoCu25-20-5	- 196 <sup>a</sup>	550	EN 10028-7	
	1.4541	X6CrNiTi18-10	– 273 a	550		
	1.4547	X1CrNiMoCuN20-18-7	- 196 <sup>a</sup>	500		
	1.4571	X6CrNiMoTi17-12-2	– 273 a	550		
heat resistant austenitic steels	1.4876	X10NiCrAlTi32-21 X10NiCrAlTi32-21 (H)	- 196	600 900 b	EN 14917, B (2.1) EN 14917, B (2.2)	

Material		Temperature °C		Desument	
Туре	Number	Steel name	Minimum	Maximum	Document
	2.4360	NICu30Fe	- 196	425	EN 14917, B (3)
	2.4610	NiMo16Cr16Ti	- 196	400	EAM-0526-28
	2.4816	.4816 NiCr15Fe	- 10	450	EAM-0526-43-1, EAM-0526-43-2
Nickel alloys	2.4010		(- 273)	(900) b	EN 14917:2009+A1: 2012, Annex J
alloys	2.4819	NiMo16Cr15W	- 196	400	EAM-0526-18
		NiCr22Mo9Nb	- 196	450	EAM-0526-40
	2.4856		(- 273)	(900) b	EN 14917:2009+A1: 2012, Annex J
	2.4858	NiCr21Mo	- 10	540	EN 14917, B (4)
Copper	CW024A	Cu-DHP (R200)	- 180	250	
	CW452K	CuSn6 (R350)	- 250	500	EN 1652 C
Copper alloy	CW503L	S CuZn20 (R270)	P 200	300	EN 1652 <sup>c</sup>
	CW508L	CuZn37 (R300)	- 200 - 200	500	

a Minimum temperature in accordance with EN 13445-2 / Annex B or EN 13480-2 / Annex B.

Table 3 — Materials for braid, fittings, ferrules, and additional parts

Component	Material No	Document				
Pressure parts	Pressure parts					
	1.4301, 1.4306, 1.4401, 1.4404, 1.4541, 1.4571		EN 10088-3			
Braid	1.4876, 2.4360, 2.4816, 2.4819, 2.4856, 2.4858		Table 2			
	Cu-based material: CW450K, CW452K, CW508L		EN 12166 <sup>a</sup>			
	Carbon steel	forged	EN 10222-2 and -3			
Fixed flance		flat products	EN 10028-2			
Fixed flange, Weld collar,	1.4301, 1.4306, 1.4401, 1.4404, 1.4541, 1.4571		EN 10222-5,			
Floating flange b			EN 10028-7			
i loading hange	1.4876, 2.4360, 2.4816, 2.4819, 2.4856, 2.4858		Table 2			
	Cu-based material:	CW024A	EN 1653+A1			

b Special care should be exercised due to the risk of embrittlement when using the materials at elevated temperatures above 550 scandards iteh avcatalog standards/sist/0d33972c-i351-4640-97d6-

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Copper and copper alloys for general purpose (not harmonized to PED); Particular Material Appraisals (PMA) are necessary for applications within the scope of the PED.