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Železniške naprave - Akustika - Merjenje zvočnih opozoril pri vratih

Railway applications - Acoustics - Measuring of door audible warnings

Bahnanwendung - Akustik - Messung akustischer Türsignale von Eisenbahnfahrzeugen

Application ferroviaires - Acoustique - Mesurage des signaux audibles d'avertissement des portes

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ICS:

17.140.30 Emisija hrupa transportnih Noise emitted by means of

sredstev transport

45.060.20 Železniški vagoni Trailing stock

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Railway applications - Acoustics - Measuring of door audible warnings

Application ferroviaires - Acoustique - Mesurage des signaux audibles d'avertissement des portes

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European foreword

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1 Scope

This document describes the type test assessment method for acoustic signals at passenger external doors applying to rolling stock. The following applies to this standard:

- this document refers to acoustical passenger information indicating the release, opening and closing of passenger doors;
- this document is applicable to tonal signals with defined frequency components;
- this document is not applicable to spoken information.
- NOTE 1 Acoustic door signals in terms of TSI compliance are defined in EN 16584-2 "Design for PRM use".
- NOTE 2 Acoustic doors signals in terms of door system function are described in EN 14752.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60942, Electroacoustics — Sound calibrators

IEC 61260, Electroacoustics — Octave-band and fractional-octave-band filters

IEC 61672-1:2002, Electroacoustics — Sound level meters — Part 1: Specifications

IEC 61672-2:2003, Electroacoustics — Sound level meters — Part 2: Pattern evaluation tests

ISO 1996-2:2007, Acoustics — Description, measurement and assessment of environmental noise — Part 2: Determination of sound pressure levels

ISO 266, Acoustics — Preferred frequencies

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

3.1

sound pressure

p

root mean square (RMS) value of a fluctuating pressure superimposed on the static atmospheric pressure measured over a certain time-period, expressed in Pa

3.2

sound pressure level

 $L_{\mathbf{p}}$

level given by the equation:

$$L_{\rm p} = 10 \, \lg (p / p_0)^2 \, dB$$
 (1)

where

 $L_{\rm p}$ is the sound pressure level in dB;

p is the RMS sound pressure in Pa;

 p_0 is the reference sound pressure; $p_0 = 20 \mu Pa$

3.3

A-weighted sound pressure level

L_{pA}

sound pressure level obtained by using the frequency weighting A, given by the following formula:

$$L_{\rm pA} = 10 \lg \left(p_{\rm A} / p_0 \right)^2 dB \qquad (2)$$

where

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 L_{pA} is the A-weighted sound pressure level in dB;

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 p_0 is the reference sound pressure; p_0 = 20 μPa

Note 1 to entry: (see EN 61672-1 and EN 61672-2)

3.4

AF-weighted sound pressure level history

$L_{pAF}(t)$

A-weighted sound pressure level as a function of time with time weighting F (fast)

3.5

AF-weighted maximum sound pressure level

*L*_{pAF}max

maximum value of the A-weighted sound pressure level determined during the measurement time interval T by using time weighting F (fast)

[SOURCE: EN 61672-1]

3.6

A-weighted equivalent continuous sound pressure level

$L_{\mathsf{pAeq},T}$

A-weighted sound pressure level given by the following equation:

$$L_{\text{pAeq,T}} = 10 \lg \left(\frac{1}{T} \int_{0}^{T} \frac{p_{\text{A}}^{2}(t)}{p_{0}^{2}} dt \right) dB L_{\text{pAeq,T}} = 10 \lg \left(\frac{1}{T} \int_{0}^{T} \frac{p_{\text{A}}^{2}(t)}{p_{0}^{2}} \right)$$
(3)

where

 L_{pAeq} , T is the A-weighted equivalent continuous sound pressure level in dB;

T is the measurement time interval in s;

 $p_{A}(t)$ is the A-weighted instantaneous sound pressure in Pa;

 p_0 is the reference sound pressure; p_0 = 20 μPa

[SOURCE: ISO 1996-1]

3.7

RMS sum

The sum of the root mean squares of sound pressures

$$RMS \ sum = 10 \lg \left(10^{\frac{L_{p1}}{10}} + 10^{\frac{L_{p2}}{10}} + \dots + 10^{\frac{L_{pi}}{10}} \right) dB$$
 (4)

where

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Lp1, Lp2 ... Lpi are a set of sound pressure levels

3.8

RMS average

average of the root mean square of sound pressures

RMS average =
$$10 \lg \left(\frac{\frac{L_{p1}}{10} + \frac{L_{p2}}{10} + \dots + \frac{L_{pN}}{10}}{N} \right) dB$$
 (5)

where

 $L_{\rm n1}, L_{\rm n2}$... $L_{\rm nN}$ are a set of sound pressure levels

4 Symbols and abbreviations

dB decibel

Hz Hertz, the SI unit of frequency

5 Instrumentation and calibration

5.1 Instrumentation

Each component of the instrumentation system shall meet the requirements for a class 1 instrument specified in IEC 61672-1.

The sound calibrator shall meet the requirements of class 1 according to IEC 60942.

Microphones with free-field characteristics shall be used.

NOTE A suitable microphone windscreen should be used.

Where one-third octave frequency band analysis is required, the filters shall meet the requirements of class 1, according to IEC 61260.

The compliance of the calibrator with the requirements of IEC 60942 shall be verified at least once a year. The compliance of the instrumentation system with the requirements of IEC 61672-1 and IEC 61672-2 shall be verified at least every 2 years. The date of the last verification of the compliance with the relevant European Standards shall be recorded.

5.2 Calibration

Before and after each series of measurements a sound calibrator meeting the requirements of class 1 according to IEC 60942 shall be applied to the microphone(s) for verifying the calibration of the entire measuring system at one or more frequencies over the frequency range of interest. If the difference between the two calibrations is more than 0,5 dB all the measurement results in between shall be rejected.

6 Interior tests

6.1 General

All the vestibules of a vehicle shall be classified into finite number of vestibule types. The list of vestibule types is to be determined before measurements. Vestibule types are to be differentiated on basis of the following distinctions:

- a) whether the vestibule has single or double exterior doors;
- b) whether there is a change in the number and type of partitions to the side of the vestibule area. That is, a vertical wall, partition or door between vestibule and another area of the vehicle. Such a partition may be partial or complete. A vestibule can have only 0, 1 or 2 such partitions, each of which can be full or partial (e.g. panels either side of an open aisle but not, when a gangway door is closed, forming a full partition of the vestibule from other parts of the train). No other property of the partition than 'full' or 'partial' shall be considered;
- c) whether there is a change in the mounting of the sounder to the vehicle structure. If there is a difference in the mechanical impedance of the structure at the location of the mounting that would lead to a change of the sound power emitted, this also differentiates a vestibule type;

- d) if there are differences in the sounder location such as:
 - the height above the floor changes by more than 30 cm,
 - the edge of the sounder is located within a distance of 4 cm from the junction of two or three approximately normal surfaces compared to an installation at the door panel.

No other criteria shall be used as they affect the sound pressure level less significantly.

A difference between vestibules in any of these features shall cause a new vestibule type to be added to the list of types.

6.2 Environmental conditions

The door opening of the vehicle shall be at least 5 m away from reflecting walls or roof of any building. There are no requirements on the external ground conditions or ground height.

Care shall be taken to ensure that noise from other sources, e.g. other vehicles or industrial plants and due to external wind, does not influence the measurements significantly.

For fixed sounders, the background noise level $L_{pAeq,T}$ measured over T = 20 s of each measurement position shall be at least 10 dB below the final result (L_{pAF} , L_{pAFmax} and, possibly, $L_{pAeq,T}$, see 6.4).

For adaptive sounders, the effective background noise is controlled by the method itself – see Annex B.

6.3 Vehicle conditions

The unit shall be stationary.

Surfaces shall present their normal operational acoustic properties.

As long as the background noise level requirement in 6.2 is fulfilled, any operational condition of auxiliary equipment shall be accepted.

6.4 Measured quantities

The measured acoustic quantities are $L_{\rm pAF}$, $L_{\rm pAFmax}$ and, possibly, $L_{\rm pAeq,\it{T}}$, with \it{T} as time of the sounder event duration. For the assessment of spectral content narrow band frequency analysis shall be applied.

6.5 Measurement procedure

6.5.1 General

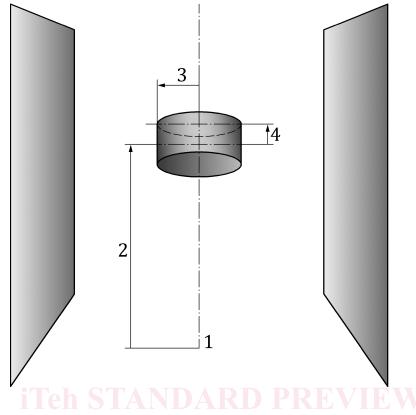
Separate procedures are defined below for estimating the sound pressure level of the signal in the vehicle, for the duration of the signal, for determining the pulse rate and for determining the frequency content. The first of these procedures, described in 6.5.3, shall be carried out *in situ* in the vehicle. The pulse rate (6.5.4) and frequency content (6.5.5) may alternatively be determined from measurements made of the door sounder component separately – see Annex C.

If an adaptive sounder system is present in the train, the background noise within the vestibule has to be controlled using a sound source (see Annex B).

6.5.2 Microphone positions for measurements in the vehicle

For the interior tests two alternative microphone arrangements are allowed.

Arrangement 1: A single microphone is located between 1,4 and 1,6 m height above the vehicle floor and anywhere within a lateral distance of 0,25 m from a point on the mid-plane of the vestibule normal to the centre-line of the door opening. That is, within the cylindrical volume indicated in Figure 1.



Key

- 1 mid way between the doors
- 2 height: 1,5 m
- 3 lateral distance: 0,25 m
- 4 range: ± 0,1 m

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Figure 1 — Arrangement 1 with one microphone

Arrangement 2: Eight microphones equally distributed in a circle of radius 0,25 m about a point 1,5 m in height above the vehicle floor and in the mid-plane of the vestibule normal to the centre-line of the door opening shall be measured twice; (1) for the circle in the horizontal orientation and (2) for the circle in a vertical orientation.

6.5.3 Sound pressure level estimation and duration of the signal

In a case of an adaptive level device an alternative measurement shall be carried out to ensure that the sounder level is adapted to the ambient noise level. The measuring procedure for adaptive door sound devices is described in Annex B.

For non-adaptive systems, the following procedure shall be followed.

For at least one microphone position the following shall be produced:

1) The time history of L_{pAF} shall be produced for the whole door opening signal and for the whole door closing signal. This shall be used to determine the timing and duration of the signal in relation to the operation of the door.

For all microphone positions the following shall be produced while the door is stationary (fully open, fully closed). The noise of the operation of the door itself is thereby omitted from the following results:

2) L_{pAF} for the door opening signal taken from the part of the signal with the door closed;

- 3) L_{pAFmax} for the door closing signal taken from the part of the signal with the door open;
- 4) If required, the $L_{pAeq,T}$ shall also be evaluated, where T is several cycles of the sound modulation.

For arrangement 2, the results of 2, 3 and 4 at the microphone positions shall be the RMS average.

NOTE The requirements can involve testing the door for each of the cases in which the door is actuated and not actuated.

6.5.4 Pulse rate estimation

This test may be performed on sound pressure measurements made on the door sounder component in a suitable environment other than the vehicle (see Annex C).

To count the number of pulses per second a visual representation of the pulsing of the sounder noise shall be produced.

NOTE It has been found that a plot of $L_{pAeq,T}$ where T is 10 ms will present a clear pulse up to 10 pulses per second. A plot of L_{AF} will not. Alternatively, a spectrogram with a sufficient time resolution can be produced by many software packages. This has been found to provide a clear representation of pulse count.

6.5.5 Frequency analysis

This test may be performed on sound pressure measurements made on the door sounder component in a suitable environment other than the vehicle (see Annex C).

To determine the frequency of tones within the signal a narrow band power spectrum shall be produced that has a resolution no worse than 20 Hz.

NOTE The frequency can also be found in a spectrogram produced for the purpose of pulse rate estimation in 6.5.4.

6.5.6 Tonal prominence assessment

If required, an assessment of the relative audibility of different tones shall be carried out as described in Annex A.

7 Exterior tests

7.1 General

The test shall be carried out on one entrance door of the unit.

7.2 Environmental conditions

The door opening of the vehicle shall be at least 5 m away from reflecting walls or roof of any building. There are no requirements on the external ground conditions or ground height (with or without platform).

Care shall be taken to ensure that the noise from other sources, e.g. other vehicles or industrial plants and due to external wind, does not influence the measurements significantly.

For fixed sounders, the background noise level $L_{pAeq,T}$ measured over T = 20 s of each measurement position shall be at least 10 dB below the final result (L_{pAF} , L_{pAFmax} and, possibly, $L_{pAeq,T}$, see 7.4).

For adaptive sounders, the effective background noise is controlled by the method itself.