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## Measurement of apparent thermal conductivity of wet porous building materials by a periodic method

*Titre manque*

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## Foreword

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The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

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ISO 16957 was prepared by Technical Committee ISO/TC 163, *Thermal performance and energy use in the built environment*, Subcommittee SC 1, *Test and measurement methods*.

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## Introduction

Most building materials, with the exception of glass and metals, are porous and thus absorb moisture due to condensation, rain, and water uptake from the ground. The absorbed moisture may damage the materials through, e.g., rotting or frost damage, and thus may cause their performance to deteriorate. In particular, an increase in the moisture content of insulation material causes a reduction of its thermal resistance, which must be avoided as much as possible to preserve its performance. However, infiltration of rain water into a brick wall or joints of tiles and uptake of ground water into the foundation (footing) are very difficult to avoid. Therefore, it is important to understand the changes in the thermal properties (thermal conductivity and heat capacity) of porous materials due to changes in their moisture content.

ISO 10051 specifies a steady-state method for measuring the thermal conductivity of a moist building material. In the steady-state method, a nonuniform distribution of moisture content in the test piece is inevitable, since the imposed temperature gradient causes moisture transfer. The nonuniform moisture distribution makes it difficult to define which moisture content the measured thermal conductivity corresponds to. ISO 10051 categorizes the moisture distribution in the test piece into several types and estimates the thermal conductivity corresponding to each type.

Since theoretical and experimental research has recently been performed concerning heat and moisture transfer in porous materials [1], [2], [3], [4], [5] along with measurements and the construction of a database of hygrothermal properties [6], hygrothermal behavior can now be predicted with reasonable accuracy.

This International Standard describes a transient method for measuring the thermal conductivity of a wet porous building material and a method of evaluating the measurement uncertainty, on the basis of both theoretical developments for heat and mass transfer and the constructed database of hygrothermal properties. The evaluation of the measurement uncertainty makes possible a simple and thus practical method for measuring thermal conductivity.

**NOTE** Thermal conductivity is one of the necessary hygrothermal properties. Since heat transfer and mass transfer in porous material interact with each other, an exact value of the thermal conductivity must be given in order to examine the validity of the theoretical models. Thus, precisely speaking, the above-mentioned theoretical models have not been validated, and the construction of the model and the measurements of the hygrothermal properties must be carried out in parallel. Nonetheless, it seems reasonable to expect that measurement of the thermal conductivity with an allowable accuracy is possible using a suitable measuring method. This is the basis for the present document.

# Measurement of apparent thermal conductivity of wet porous building materials by a periodic method

## 1 Scope

The International Standard describes a method of measuring the thermal conductivity (diffusivity) of a wet porous building material and a method of evaluating the measurement uncertainty.

While ISO 10051 is the current standard, based on a steady-state method, the proposed method makes use of a non-steady-state method that uses a small temperature change with a short period as an input. Along with the measurement, an evaluation of the measurement uncertainty will be carried out, which makes possible a simple and practical measuring method.

This International Standard describes intends to measure the apparent (effective) thermal conductivity including latent heat transfer caused by vapour movement. The situation in which moisture and/or air movement occur due convection or gravity is excluded. The application of this standard to high moisture content is excluded so that the gravity effect can be neglected. This International Standard describes can be applied to a porous material heavier than about  $100 \text{ kg/m}^3$ , in which radiative heat transfer can be neglected.

The content of this International Standard describes is as follows:

- 1) a non-steady-state method of measuring thermal conductivity;
- 2) an approximation formula for the measurement uncertainty caused by moisture movement and nonuniform moisture distribution (and thus, a determination of the measuring conditions that satisfy the upper limit of measurement uncertainty), and
- 3) an estimate of the heat transfer caused by moisture (vapour) movement.

## 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 9346:2007, *Thermal insulation — Mass transfer — Physical quantities and definitions*

ISO 10456:2007, *Thermal insulation — Building materials and products — Determination of declared and design thermal values*

ISO 10051:1996, *Thermal insulation — Moisture effects on heat transfer — Determination of thermal transmissivity of a moist porous material*

## 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 9346:2007, ISO 10051:1996 and the following apply.

### 3.1

#### **apparent thermal conductivity of a wet material $\lambda^*$**

intrinsic material property dependent upon moisture content and temperature but not on testing conditions.

Note 1 to entry: Since this value includes the influence of heat transfer due to phase change (condensation and evaporation), it is called apparent thermal conductivity.

#### 4 Symbols and units

Symbol	Quantity	Units
$a$	thermal diffusivity of the material	$m^2/s$
$A, B, C, D$	defined in Equation (B.14)	-
$c$	porosity	$m^3/m^3$
$c'$	specific heat of the material	$J/(kg \cdot K)$
$c_s$	specific heat of the dry material	$J/(kg \cdot K)$
$D_T$	Moisture (vapour and liquid water) conductivity related to temperature gradient	$kg/(m \cdot s \cdot K)$
$D_\theta$	Moisture (vapour and liquid water) conductivity related to water content gradient	$m^2/s$
$D_{Tl}$	liquid water conductivity related to temperature gradient	$kg/(m \cdot s \cdot K)$
$D_{\theta l}$	liquid water conductivity related to water content gradient	$m^2/s$
$D_{Tv}$	vapour conductivity related to temperature gradient	$kg/(m \cdot s \cdot K)$
$D_{\theta v}$	vapour conductivity related to water content gradient	$m^2/s$
$E, E_1, E_2$	defined in Formula (B.12)	-
$I_0$	amplitude of the input surface temperature	K
$k_v$	vapour diffusivity	$kg/(m \cdot s \cdot (kg/kg'))$
$R$	latent heat of vaporization	J/kg
$S$	specific surface area inside the material, i.e., ratio of surface area to the pore volume	$m^2/m^3$
$t$	time	s
$T$	temperature	K
$T_0$	initial temperature	K
$T_1, T_2, \theta_1, \theta_2$	the first and second terms of the perturbation solution of the temperature and water content, respectively	K, $kg/m^3$
$x$	coordinate	m
$X$	humidity ratio of moist air in the pores of the specimen	$kg/kg'$
$X_i$	equilibrium humidity ratio with liquid or capillary water at the interface in the material	$kg/kg'$
$U_3, U_7, Q_1 - Q_6,$ $R_1 - R_6, V_{18}$	coefficients appearing solutions $\theta_2$ and $T_2$	-
$\alpha_1, \alpha_2$	defined in Formula (B.13)	-
$\alpha'$	effective vapour transfer coefficient at the interface	$kg/(m \cdot s \cdot kg)/kg'$



$\gamma$	specific weight of dry air	kg/m <sup>3</sup>
$\gamma'$	density of the material	kg/m <sup>3</sup>
$\gamma_s$	density of the dry material	kg/m <sup>3</sup>
$\eta_1, \zeta_1, \beta_1, \xi_1, \kappa_1, \gamma_1$	water content coefficients of $D_{\theta l}, D_{\theta v}, D_{Tl}, D_{Tv}, c', \gamma', \lambda$	-
$\eta_2, \zeta_2, \beta_2, \xi_2, \gamma_2$	temperature coefficients of $D_{\theta l}, D_{\theta v}, D_{Tl}, D_{Tv}, \lambda$	-
$\lambda$	thermal conductivity without moisture movement	W/(m·K)
$\lambda^*$	thermal conductivity defined as $\lambda^* = \lambda + RD_{Tv}$	W/(m·K)
$\theta$	water content of material	kg/m <sup>3</sup>
$\theta_0$	initial water content of material	kg/m <sup>3</sup>
$\theta_0$	water content by weight	%
$\omega$	angular velocity of the input surface temperature	rad/s

## 5 Determination of thermal conductivity of a wet porous material by non-steady-state method (periodic method)

When measuring the thermal conductivity of a porous material in which moisture transfer may occur, the nonuniformity of the water content distribution must be kept as low as possible under the temperature gradient. In order to minimize the nonuniformity, a periodic method is adopted as a transient method of measuring thermal conductivity in this standard. Since positive and negative temperature gradients are generated in turn in this method, the (time-averaged) water content distribution can be expected to remain uniform.

By measuring the temperatures at two points in the sample (usually one of them is at the sample surface), the thermal diffusivity (not conductivity) can be determined based on the amplitude ratio or phase difference of these two temperatures. If moisture movement does occur, a similar method can be used to determine the thermal diffusivity if the input cyclic temperature fluctuation is kept small enough that the change in transport properties is also small enough that the system can be regarded as linear (see Annex B).

## 6 Measurement by periodic method

### 6.1 Test procedure

A schematic diagram of the apparatus for the periodic method is given in Figure 1. The whole system is installed in a climate chamber whose temperature is kept at the mean temperature of the sample under measurement. The sample is preconditioned at a certain water content, and then the whole surface is made impermeable to moisture movement. A periodic temperature variation is imposed on the sample, and the temperatures at (at least) two points in the sample are measured by thermocouples.

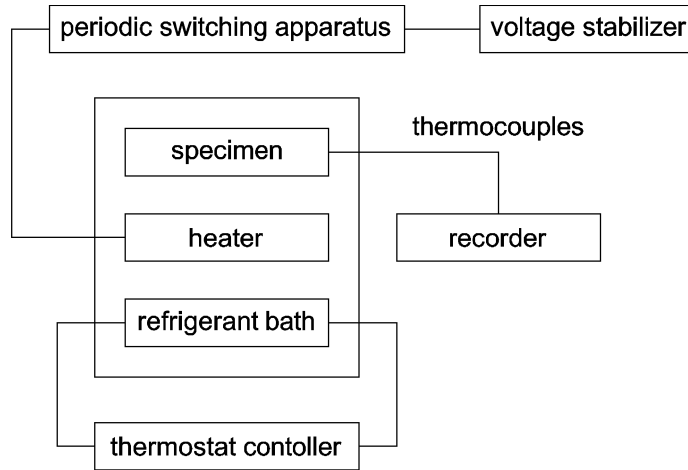


Figure 1 — Schematic diagram for measuring thermal diffusivity

## 6.2 Measuring apparatus

### 6.2.1 Overall design

A detailed schematic of the measuring apparatus is shown in Figure 2. Refrigerant kept at a low constant temperature is circulated in a metal refrigerant bath (200 mm (length) × 200 mm (wide) × 50mm (height)) in order to avoid a temperature increase due to heating by the heater. A heater, a damping layer, and a sample are placed on the refrigerant bath in order, and another damping layer is placed on the sample to reduce the influence of the temperature fluctuations of the climate chamber surrounding the measuring apparatus. Either a sinusoidal or stepwise electric current is generated in the heater. The stepwise wave becomes almost sinusoidal as it flows through the damping layers before arriving at the sample surface. Thermocouples are inserted into the sample and connected to the recorders. The output from the thermocouples is recorded by both an analog recorder and a digital recorder. The digital recorder is used for a long-term record for temperatures at multiple points, while the analog recorder is used for recording the temperature wave in a short-term measurement