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# Standard Test Method for Measuring Reaction Rates by Radioactivation of Uranium-238<sup>1</sup>

This standard is issued under the fixed designation E704; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

### 1. Scope

1.1 This test method covers procedures for measuring reaction rates by assaying a fission product (F.P.) from the fission reaction  $^{238}$ U(n,f)F.P.

1.2 The reaction is useful for measuring neutrons with energies from approximately 1.5 to 7 MeV and for irradiation times up to 30 to 40 years.

1.3 Equivalent fission neutron fluence rates as defined in Practice E 261E261 can be determined.

1.4Detailed 1.4 Detailed procedures for other fast-neutron detectors are referenced in Practice E 261E261.

<del>1.5</del>

1.5 The values stated in SI units are to be regarded as standard. No other unites of measurement are included in this standard.

<u>1.6</u> This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

#### 2. Referenced Documents

2.1 ASTM Standards:<sup>2</sup>

E170 Terminology Relating to Radiation Measurements and Dosimetry

E181 Test Methods for Detector Calibration and Analysis of Radionuclides

- E261 Practice for Determining Neutron Fluence, Fluence Rate, Fluence, and Spectra by Radioactivation Techniques
- E262 Test Method for Determining Thermal Neutron Reaction Rates and Thermal Neutron Fluence Rates by Radioactivation Techniques

E320 Test <u>Methods</u> Method for Cesium-137 in Nuclear Fuel Solutions by Radiochemical Analysis

E393 Test Method for Measuring Reaction Rates by Analysis of Barium-140 from Fission Dosimeters<sup>2</sup>

E482Guide for Application of Neutron Transport Methods for Reactor Vessel Surveillance, E706 (IID)<sup>2</sup> Test Method for Macauring Practice Provide the Analysis of Parises 140 From Eissian Designation

Measuring Reaction Rates by Analysis of Barium-140 From Fission Dosimeters 18-7659(2)6689d/astm-e704-08 E705 Test Method for Measuring Reaction Rates by Radioactivation of Neptunium-237

E844 Guide for Sensor Set Design and Irradiation for Reactor Surveillance, E 706 (IIC)

E944 Guide for Application of Neutron Spectrum Adjustment Methods in Reactor Surveillance, E 706 (IIA)

E1005 Test Method for Application and Analysis of Radiometric Monitors for Reactor Vessel Surveillance, E 706 (IIIA)

E1018 Guide for Application of ASTM Evaluated Cross Section Data File, Matrix E706 (IIB)

# 3. Terminology

3.1 Definitions:3.1.1Refer to Terminology E 170E 1703.1.1 Refer to Terminology E170.

## 4. Summary of Test Method

4.1 High-purity  $^{238}$ U (<40 ppm  $^{235}$ U) is irradiated in a fast-neutron field, thereby producing radioactive fission products from the reaction  $^{238}$ U(n,f)F.P.

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<sup>&</sup>lt;sup>1</sup> This test method is under the jurisdiction of ASTM Committee <u>E-10 E10</u> on Nuclear Technology and Applications and is the direct responsibility of Subcommittee E10.05 on Nuclear Radiation Metrology.

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<sup>&</sup>lt;sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards , Vol 12:02.volume information, refer to the standard's Document Summary page on the ASTM website.

4.2 Various fission products such as <sup>137</sup>Cs-<sup>137m</sup>137mBa, <sup>140</sup>Ba-<sup>140</sup>La, <sup>95</sup>Zr, and <sup>144</sup>Ce can be assayed depending on the length of irradiation, purpose of the experiment, etc.

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4.3 The gamma rays emitted through radioactive decay are counted, and the reaction rate, as defined in Practice E = 261E261, is calculated from the decay rate and the irradiation conditions.

4.4 The neutron fluence rate for neutrons with energies from approximately 1.5 to 7 MeV can then be calculated from the spectral-weighted neutron activation cross section as defined in Practice E 261E261.

4.5 A parallel procedure that uses  $^{237}$ Np instead of  $^{238}$ U is given in Test Method <del>E 705</del>E705.

#### 5. Significance and Use

5.1Refer to Practice E 261E 261

5.1 Refer to Practice E261 for a general discussion of the determination of fast-neutron fluence rate with fission detectors.

5.2  $^{238}$ U is available as metal foil, wire, or oxide powder (see Guide E 844E844). It is usually encapsulated in a suitable container to prevent loss of, and contamination by, the <sup>238</sup>U and its fission products.

5.3 One or more fission products can be assayed. Pertinent data for relevant fission products are given in Table 1 and Table 2. 5.3.1 <sup>137</sup>Cs-<sup>137</sup>m<u>137</u>mBa is chosen frequently for long irradiations. Radioactive products <sup>134</sup>Cs and <sup>136</sup>Cs may be present, which can interfere with the counting of the 0.662 MeV  $^{137}$ Cs- $^{137}$ -m, Ba gamma rays (see Test Methods E 320E320).

5.3.2  $^{140}$ Ba- $^{140}$ La is chosen frequently for short irradiations (see Test Method E 393E393).

5.3.3 <sup>95</sup>Zr can be counted directly, following chemical separation, or with its daughter <sup>95</sup>Nb using a high-resolution gamma detector system.

5.3.4 <sup>144</sup>Ce is a high-yield fission product applicable to 2- to 3-year irradiations.

5.4 It is necessary to surround the  $^{238}$ U monitor with a thermal neutron absorber to minimize fission product production from a quantity of  $^{235}$ U in the  $^{238}$ U target and from  $^{239}$ Pu from (n, $\gamma$ ) reactions in the  $^{238}$ U material. Assay of the  $^{239}$ Pu concentration when a significant contribution is expected.

5.4.1 Fission product production in a light-water reactor by neutron activation product <sup>239</sup>Pu has been calculated to be insignificant (<2 %), compared to that from <sup>238</sup>U(n,f), for an irradiation period of 12 years at a fast-neutron (E > 1 MeV) fluence rate of  $1 \times 10^{11}$  cm<sup>-2</sup>· s<sup>-1</sup> provided the <sup>238</sup>U is shielded from thermal neutrons (see Fig. 2 of Guide <del>E 844</del>E844).

5.4.2 Fission product production from photonuclear reactions, that is,  $(\gamma, f)$  reactions, while negligible near-power and research-reactor cores, can be large for deep-water penetrations (1).<sup>3</sup>

5.5 Good agreement between neutron fluence measured by <sup>238</sup>U fission and the <sup>54</sup>Fe(n,p)<sup>54</sup>Mn reaction has been demonstrated (2). The reaction  $^{238}$ U(n,f) F.P. is useful since it is responsive to a broader range of neutron energies than most threshold detectors.

<sup>3</sup> Vanadium-encapsulated monitors of high purity are available from the Oak Ridge National Laboratory, Isotope Sales Div., Oak Ridge, TN 37830.

<sup>3</sup> The boldface numbers in parentheses refer to the list of references appended to this test method.

TABLE 1 Recommended Nuclear Parameters for Certain Fission

Products						
Fission Product	Parent Half-Life <sup>A</sup> (6)	Primary Radiation <sup>A</sup> – <b>(7)</b> (keV)	γ Probability of Decay <sup>A</sup> (7)	Maximum Useful Irradiation Duration		
<sup>95</sup> Zr	<del>64.04 (4) d</del>	<del>724.199 (5)</del>	<del>0.4417 (19)</del>	6 months		
<sup>95</sup> Zr	64.032 (6) d	724.192 (4)	0.4427 (22)	6 months		
		756.729 (12)	0.5446			
		756.725 (12)	0.5438			
<sup>99</sup> Mo	<del>65.94 (1) h</del>	0.1213	739.5	300 hours		
<sup>99</sup> Mo	2.7489 (6) d	739.500 (17)	0.1213 (22)	300 hours		
		<del>0.0435</del>	<del>777.921</del>			
		777.921 (20)	0.0426 (8)			
<sup>103</sup> Ru	<del>39.254 (8) d</del>	<del>497.084 (10)</del>	<del>0.910 (23)</del>	4 months		
<sup>103</sup> Ru	39.26 (2) d	497.084 (6)	<u>0.910 (12)</u>	4 months		
137Cs	<del>30.0 (2) yr</del>	<del>661.660 (3)<sup>B</sup></del>	0.8510 <sup>B</sup>	<del>30–40 years</del>		
<sup>137</sup> Cs	30.03 (5) yr	<u>661.657 (3)<sup>B</sup></u>	0.8510 <sup>B</sup>	30-40 years		
$\frac{140}{140}Ba - \frac{140}{140}La$	<del>12.746 (10) d</del>	<del>537.31 (4)</del>	<del>0.2439</del>	1-1.5 months		
<sup>140</sup> Ba – <sup>140</sup> La	<u>12.752 (3) d</u>	537.261 (4)	<u>0.2439 (23)</u>	1-1.5 months		
		<del>1596.54 (14)</del>	0.9540 <sup>C</sup>			
		1596.21 (4)	0.954 (14) <sup>C</sup>			
144.0			1.1515 <sup>D</sup>			
144 <b>Ce</b>	<del>284.9 (2) d</del>	<del>133.515 (8)</del>	<del>0.1109 (4)</del>	2-3 years		
<sup>144</sup> Ce	289.91 (5) d	133.515 (2)	0.1109 (10)	2–3 years		

<sup>A</sup> The lightface numbers in parentheses are the magnitude of plus or minus uncertainties in the last digit(s) listed.

<sup>B</sup> With <sup>137m</sup>Ba (2.552 min) in equilibrium. <sup>C</sup> Probability of daughter <sup>140</sup>La decay.

<sup>D</sup> With <sup>140</sup>La (1.67801 d) in transient equilibrium.



#### TABLE 2 Recommended Fission Yields for Certain Fission Products<sup>A</sup>

FIGUEIS						
Fissile Isotope	Neutron Energy	Reaction Product	Type Yield	ENDF/B-VII <sup>_BA,AB_</sup> Fission Yield <u>%</u>		
<sup>238</sup> U(n,f) <sup>238</sup> U(n,f)	0.5 MeV 0.5 MeV	95 Zr 95 Zr 99 99 00 103 Ru 103 Ru 103 Ru 137 Cs 137 Cs 137 Ba 137 Ba 137 Ba 140 Ba 140 La 140 La 144 Ce	유 오 육 오 육 오 육 도 육 오 국 코 숙 오	$\begin{array}{c} \hline 5.15126 \pm 1 \ \% \\ \hline 6.01736 \pm 4 \ \% \\ \hline 6.18839 \pm 1.4 \ \% \\ \hline 6.16825 \pm 1.4 \ \% \\ \hline 6.26113 \pm 1 \ \% \\ \hline 6.27532 \pm 1.4 \ \% \\ \hline 6.02075 \pm 1 \ \% \\ \hline 6.02075 \pm 1 \ \% \\ \hline 6.05254 \pm 1 \ \% \\ \hline 4.100116 \ 8 \pm 64 \ \% \\ \hline 5.8004e \ 6 \pm 64 \ \% \\ \hline 5.81523 \pm 0.7 \ \% \\ \hline 1.38004e \ 5 \pm 64 \ \% \\ \hline 4.55034 \pm 1.4 \ \% \\ \hline 4.55034 \pm 1.4 \ \% \\ \hline 4.54797 \pm 1.4 \ \% \end{array}$		

<sup>A</sup>E <u>"Special Issue ong Evaluanted, T. R., and Rid Nuclear, B. Data</u> F., <u>ile</u> ENDF/<u>B-349 EvalVII.0</u>," <u>Nuclear Dationand Compila</u> <u>Sheetion of Fission Prod</u>, <u>J.</u> K. Tuet Yli, elds-itor, <u>L. Vos Ala</u> 107, <u>Decemes Nber</u> 2006. <u>Dational L aborvatory</u>, Los Ailamos, NM, rblep orn t-LA-UR-94-3106;he ENDF/<u>B-349VII</u>, <u>Oenline</u>, <u>htetp://</u> www.nndc.bnl.gov/exfor/endf00.htm, July 1994, 2008.

<sup>B</sup> All yield data given as a %; RC represents a cumulative yield; RI represents an independent yield.

5.6 The <sup>238</sup>U fission neutron spectrum-averaged cross section in several benchmark neutron fields is given in Table 3 of Practice E 261E261. Sources for the latest recommended cross sections are given in Guide E 1018E1018. In the case of the <sup>238</sup>U(n,f)F.P. reaction, the recommended cross section source is the ENDF/B-VI release 8 cross section (MAT=9237), revision 1(MAT = 9237) (3). Fig. 1 shows a plot of the recommended cross section versus neutron energy for the fast-neutron reaction <sup>238</sup>U(n,f)F.P.

NOTE 1—The data is taken from the Evaluated Nuclear Data File, ENDF/B-VI, rather than the later ENDF/B-VII. This is in accordance with Guide E1018, Section 6.1, since the later ENDF/B-VII data files do not include covariance information. Some covariance information exists for <sup>238</sup>U in the standard sublibrary, but this is only for energies greater than 1 MeV. For more details, see Section H of Ref 4.

#### 6. Apparatus

6.1 *Gamma-Ray Detection Equipment* that can be used to accurately measure the decay rate of fission product activity are the following two types (4(5): ASTM E704-08)

https://standards.jteh.ai/catalog/standards/sist/6899d4d4-a9c0-4875-9df8-7b59f2fb689d/astm-e704-08

