

SLOVENSKI STANDARD SIST-TS CEN/TS 19103:2022

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Evrokod 5: Projektiranje lesenih konstrukcij - Projektiranje sovprežnih konstrukcij iz lesa in betona - Splošna pravila in pravila za stavbe

Eurocode 5: Design of Timber Structures - Structural design of timber-concrete composite structures - Common rules and rules for buildings

Eurocode 5: Berechnung und Konstruktion von Holzbauten - Bemessung und Berechnung von Holz-Beton-Verbundbauteilen - Allgemeine Regeln und Regeln für den Hochbau

Eurocode 5 : Conception et calcul des structures en bois - Calcul des structures mixtes bois-béton - Règles communes et règles pour les bâtiments

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Eurocode 5: Design of Timber Structures - Structural design of timber-concrete composite structures - Common rules and rules for buildings

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This Technical Specification (CEN/TS) was approved by CEN on 25 July 2021 for provisional application.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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European foreword

This document (CEN/TS 19103:2021) has been prepared by Technical Committee CEN/TC 250 "Structural Eurocodes", the secretariat of which is held by BSI. CEN/TC 250 is responsible for all Structural Eurocodes and has been assigned responsibility for structural and geotechnical design matters by CEN.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN shall not be held responsible for identifying any or all such patent rights.

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This document has been drafted to be used in conjunction with relevant execution, material, product and test standards, and to identify requirements for execution, materials, products and testing that are relied upon by this document.

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0 Introduction

0.1 Introduction to the Eurocodes

The Structural Eurocodes comprise the following standards generally consisting of a number of parts:

- EN 1990 Eurocode: Basis of structural design;
- EN 1991 Eurocode 1: Actions on structures;
- EN 1992 Eurocode 2: Design of concrete structures;
- EN 1993 Eurocode 3: Design of steel structures;
- EN 1994 Eurocode 4: Design of composite steel and concrete structures;
- EN 1995 Eurocode 5: Design of timber structures;
- EN 1996 Eurocode 6: Design of masonry structures;
- EN 1997 Eurocode 7: Geotechnical design;
- EN 1998 Eurocode 8: Design of structures for earthquake resistance;
- EN 1999 Eurocode 9: Design of aluminium structures;
- New Eurocodes under development dards.iteh.ai)

0.2 Introduction to EN 1995 (all parts)

- (1) EN 1995 (all parts) applies to the design of buildings and civil engineering works in timber (solid timber, sawn, planed or in pole form, glued laminated timber or wood-based structural products, e.g. LVL) or wood-based panels jointed together with adhesives of mechanical fasteners. It complies with the principles and requirements for the safety and serviceability of structures and the basis of design and verification given in EN 1990.
- (2) EN 1995 (all parts) is concerned only with requirements for mechanical resistance, serviceability, durability and fire resistance of timber structures. Other requirements concerning thermal or sound insulation, for example, are not considered.
- (3) EN 1995 (all parts) is subdivided into various parts:
- EN 1995-1 *General*;
- EN 1995-2 *Bridges*.
- (4) EN 1995-1 "General" in itself does not exist as a physical document, but comprises the following two separate parts:
- EN 1995-1-1 General Common rules and rules for buildings;
- EN 1995-1-2 General Structural fire design.

EN 1995-2 refers to the General rules in EN 1995-1-1.

This document supplements EN 1995.

0.3 Verb forms used in this Technical Specification

The verb "shall" expresses a requirement strictly to be followed and from which no deviation is permitted in order to comply with the Eurocodes.

The verb "should" expresses a highly recommended choice or course of action. Subject to national regulation and/or any relevant contractual provisions, alternative approaches may be used/adopted where technically justified.

The verb "may" expresses a course of action permissible within the limits of the Eurocodes.

The verb "can" expresses possibility and capability; it is used for statements of fact and clarification of concepts.

0.4 National annex for CEN/TS 19103

This document provides values within notes, indicating where national choices can be made. Therefore, a national document implementing CEN/TS 19103 can have a National Annex containing all Nationally Determined Parameters to be used for the assessment of buildings and civil engineering works in the relevant country.

National choice is allowed in CEN/TS 19103 through the following subclauses:

- 4.3.1.2(5) Average timber moisture content due to the environmental conditions
- 4.4.1.1 Partial factor for shrinkage action R K V K
- 4.4.1.2 Partial factor for temperature action ards.iteh.ai)
- 4.4.1.2 Partial factor for moisture content action

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• 4.4.2 Partial factor for connection shear strength of standards/sist/446e4a24-

National choice is allowed in CEN/TS 19103 on the application of the following informative annexes:

• Annex A Yearly variations of moisture content averaged over the timber cross-section for timber-concrete composite structures in variable environmental conditions

The National Annex can contain, directly or by reference, non-contradictory complementary information for ease of implementation, provided it does not alter any provisions of the Eurocodes.

1 Scope

1.1 Scope of CEN/TS 19103

- (1) CEN/TS 19103 gives general design rules for timber-concrete composite structures.
- (2) It provides requirements for materials, design parameters, connections, detailing and execution for timber-concrete composite structures. Recommendations for environmental parameters (temperature and moisture content), design methods and test methods are given in the Annexes.
- (3) It includes rules common to many types of timber-concrete composite, but does not include details for the design of glued timber-concrete composites, nor for bridges.
- NOTE For the design of glued timber-concrete composites or bridges alternative references are available.
- (4) It covers the design of timber-concrete composite structures in both quasi-constant and variable environmental conditions. For ease of use, it provides simple design rules for quasi-constant environmental conditions and more complex rules for variable environmental conditions.

1.2 Assumptions

- (1) The general assumptions of EN 1990 apply.
- (2) CEN/TS 19103 is intended to be used in conjunction with EN 1990, EN 1991 (all parts), EN 1992 (all parts), EN 1994 (all parts), EN 1995 (all parts), EN 1998 (all parts) when timber structures are built in seismic regions, and ENs for construction products relevant to timber structures.

2 Normative references

PREVIEW

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

NOTE See the Bibliography for a list of other documents cited that are not normative references, including those referenced as recommendations (i.e. in 'should' clauses), permissions ('may' clauses), possibilities ('can' clauses), and in notes.

EN 1990:2002¹⁾, Eurocode - Basis of structural design

EN 1991 (all parts), Eurocode 1: Actions on structures

EN 1991-1-5:2003, Eurocode 1: Actions on structures - Part 1-5: General actions - Thermal actions

EN 1992-1-1:2004²⁾, Eurocode 2: Design of concrete structures - Part 1-1: General rules and rules for buildings

EN 1993-1-8, Eurocode 3: Design of steel structures - Part 1-8: Design of joints

EN 1994-1-1:2004, Eurocode 4: Design of composite steel and concrete structures - Part 1-1: General rules and rules for buildings

2) As impacted by EN 1992-1-1:2004/A1:2014.

¹⁾ As impacted by EN 1990:2002/A1:2005.

EN 1994-2:2005, Eurocode 4 - Design of composite steel and concrete structures - Part 2: General rules and rules for bridges

EN 1995-1-1:2004³⁾, Eurocode 5: Design of timber structures - Part 1-1: General - Common rules and rules for buildings

EN 14592, Timber structures - Dowel-type fasteners - Requirements

3 Terms, definitions and symbols

3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in EN 1990, EN 1995-1-1 and the following apply.

3.1.1

continuous fastener

fastener that is continuous along the length of the timber component

3.1.2

connection

any device or system formed of connected parts and an associated fastener or fasteners as well as, where applicable, notches, which resists slip and transfers the related shear force at the interface between timber and concrete

Note 1 to entry: Examples include dowel-type fasteners of any material, notches, plates and continuous fasteners, any of which can be either mechanically fixed or bonded.

Note 2 to entry: Staples fall beyond the scope of this standard. 19103:2022

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inelastic strain

strain which is caused not by stresses but by shrinkage, swelling or thermal expansion, for example

3.1.4

moisture content

mass of water in wood, expressed as a percentage of its oven-dry mass

3.1.5

quasi-constant environmental conditions

environmental conditions where

- timber is installed close to its expected moisture content in use mc_{use} and
- for softwood timber, the variation of average moisture content in use (Δmc , see Formula (4.5)) does not exceed 6 % and
- the temperature variations of the air do not exceed 20 °C

Note 1 to entry: The indoor conditions of a heated building are a typical example of quasi-constant conditions.

³⁾ As impacted by EN 1995-1-1:2004/A1:2008 and EN 1995-1-1:2004/A2:2014.

3.1.6

shrinkage of concrete

decrease in dimension of a piece of concrete due to the hardening process

3.1.7

shrinkage of timber

decrease in dimension of a piece of timber due to reduction of moisture content

3.1.8

swelling of timber

increase in dimension of a piece of timber due to increase of moisture content

3.1.9

thermal expansion

linear thermal expansion between given temperatures

3.1.10

 $E_{\mathbf{k}}$

 $E_{q,per}$

variable environmental conditions

conditions that do not comply with quasi-constant environmental conditions

Note 1 to entry: Typical examples where variable environmental conditions can be experienced are balconies, unheated roof spaces and outdoor covered and uncovered spaces.

3.2 Symbols and abbreviations

For the purposes of this document, the symbols given in EN 1995-1-1 and the following apply.

Latin upper-case letters (standards.iteh.ai)

A_1	Area of cross-section 1 SIST-TS CEN/TS 19103:2022
A_2	Area of cross-section 2 https://standards.nen.arcatalog/standards/sist/446e4a24-
$A_{\rm b}$	d'Arealof longitudinal reinforcement in concréte flange 22
$A_{\rm conc,ef}$	Effective area of the concrete cross-section
$A_{\rm S}$	Area of longitudinal reinforcement in concrete flange
$A_{\rm sf}$	Area of transverse reinforcement in concrete flange
A_{tim}	Area of the timber cross-section
$C_{J,sls}$	Coefficient which considers the interaction between vertical load $q_{\rm d}$ and inelastic strains in terms of slip in the joint
$C_{p,sls}$	Coefficient which correlates the inelastic strains with a fictitious load
E_1	Modulus of elasticity of cross-section 1
E_2	Modulus of elasticity of cross-section 2
$E_{\rm conc}$	Modulus of elasticity of concrete
$E_{\rm conc,fin}$	Effective long-term modulus of elasticity of concrete

Characteristic combination of actions

Quasi-permanent combination of actions

 $E_{\rm u}$ Fundamental combination of actions

 $E_{\rm s}$ Design value of the modulus of elasticity of the steel reinforcement as given in

EN 1992-1-1:2004, 3.2.7

 E_{tim} Mean modulus of elasticity of timber parallel to the grain

 $E_{
m tim.fin}$ Effective long-term modulus of elasticity of timber parallel to the grain

 $(EI)_i$ Bending stiffness of the cross-section i

(EI)_{ef.EC5-AnnexB} Effective bending stiffness according to EN 1995-1-1:2004, Annex B

(EI)_{ef sls} Modified effective bending stiffness according to EN 1995-1-1:2004, Annex B,

which accounts for the interaction between vertical load and inelastic strains

 $F_{\text{ax.Rk}}$ Characteristic axial withdrawal capacity of the fastener

 $F_{\rm est}$ Estimated load-carrying capacity as defined in accordance with EN 26891 and

used in determining the mean slip modulus for ultimate limit states

 $F_{
m max}$ Characteristic load-carrying capacity in an Annex C test, as determined in

accordance with EN 26891

 $F_{\rm Rd}$ Design load-carrying capacity for a notched connection

 $F_{\rm t.Ed}$ Design tensile force between the timber and the concrete cross-section

 $F_{v,Ed}$ Design shear force per connection S

 $F_{v,Rd}$ Design load-carrying capacity per connection

 $F_{v,Rk}$ Characteristic connection shear strength 03.2022

https://standards.iteh.ai/catalog/standards/sist/446e4a24- $F_{v.R.t.c.k}$ Characteristic load-carrying capacity in shear per connection at time t_c

 I_1 Moment of inertia of cross-section 1 I_2 Moment of inertia of cross-section 2

 I_{tim} Moment of inertia of the timber cross-section

K Stiffness of the connection

 $K_{
m max}$ Maximum stiffness of the connection $K_{
m min}$ Minimum stiffness of the connection

 K_{ref} Reference stiffness of connection

 $K_{\rm ser}$ Slip modulus for serviceability limit states

 $K_{\text{ser.fin}}$ Final slip modulus

 $K_{\rm ser.t_c}$ Mean slip modulus for serviceability at time $t_{\rm c}$

 K_{u} Instantaneous slip modulus of the connection for ultimate limit states

 $K_{\text{u.fin}}$ Final slip modulus for ultimate limit states

 $K_{\mathrm{u,t_c}}$ Slip modulus for ultimate limit states at time t_{c}

L Span of the beam

 $M(q_d + 0.8p_{sls})$ Resulting bending moment due to external loads and part (80 %) of the fictitious

load equivalent to inelastic strains

 $M(q_{\rm d})$ Resulting bending moment due to external load only

 M_i Bending moment of component i

 $M_{\rm max,2}$ Maximum bending moment in cross-section 2

 M_{tim} Bending moment in the timber cross-section

 N_i Axial force in cross-section i

 $N_{\rm max,2}$ Maximum axial force in cross-section 2

 N_{tim} Axial force in the timber cross-section

 $T_{0,\mathrm{conc}}$ Initial average temperature in the concrete at time t_c

 $T_{0,\text{tim}}$ Initial average temperature in the timber at time t_c

 $T_{\text{max,conc}}$ Maximum temperature in the concrete (averaged over the cross-section)

 $T_{\text{max,tim}}$ Maximum temperature in the timber (averaged over the cross-section)

 $T_{\min, conc}$ Minimum temperature in the concrete (averaged over the cross-section)

 $T_{\text{min.tim}}$ Minimum temperature in the timber (averaged over the cross-section)

V_{max} Effective maximum shear force iteh ai

 $V(q_d)$ Resulting shear force due to external load

 $V_{
m u}$ Ultimate slip determined in an Annex C test in accordance with EN 12512

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 $X_{\rm d}$ Design value of a strength property of timber or a wood-based product

Latin lower-case letters

a Distance

 a_1 spacing of fasteners parallel to the grain

 $a_{1\leftrightarrow c}$ Distance from the centroid of cross-section 1 to the centroid of the effective

composite cross-section

 a_{3c} Distance between the fastener and the unloaded edge

 a_{3t} Distance between the fastener and the loaded edge

 a_4 spacing of fasteners perpendicular to the grain

as Cross-sectional area of the transverse reinforcement of the concrete flange when

checking in-plane shear in the concrete

 a_{h} Cross-sectional area of the longitudinal reinforcement of the concrete flange when

checking in-plane shear in the concrete

 $b_{\rm conc}$ Width of the concrete

 $b_{\rm conc.ef}$ Effective width of the concrete

*b*_n Notch width

 b_{tim} Width of the timber

 $b_{\rm w}$ Width of the timber element (in verification of concrete for in-plane shear)

 $c_{\min, dur}$ Minimum concrete cover for durability of steel reinforcement

 c_{nom} Nominal concrete cover

d Fastener diameter or rebar diameter

 d_{g} Diameter of the aggregate

 $d_{\rm r}$ Diameter of the concrete reinforcement bar diameter

 $f_{\rm cd}$ Design value of the compressive strength of concrete

 $f_{\rm ck}$ Characteristic compressive cylinder strength of the concrete at 28 days

 $f_{\rm ctd}$ Design value of the tensile strength of concrete

 $f_{c,h,2,k}$ characteristic embedment strength of the concrete member for evaluation of the

load-carrying capacity based on the Johansen models

 $f_{\rm vcd}$ Effective design shear strength for the concrete

 $f_{\rm v.t.d}$ Design shear strength of the timber member

 $f_{
m yd}$ Design value of the yield strength of steel reinforcement

 $h_{\rm s,conn}$ Nominal height of the connector

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 $h_{\rm f}$ Thickness of the concrete flange/catalog/standards/sist/446e4a24- $h_{\rm n}$ Notch deptha-4535-8018-5fa5f6e255f9/sist-ts-cen-ts-19103-2022

 k_{def} Deformation factor of timber

 k_{def} Deformation factor for connections between concrete and timber

 k_{mod} Modification factor for duration of load and moisture content for timber strength

 k_{mod} Modification factor for duration of load and moisture content for the strength of

connections between concrete and timber

 $k_{\rm s}$ Mean slip modulus for serviceability limit states, determined from Annex C tests in

accordance with EN 26891

 k_{tc} Coefficient for concrete, taking into account the effect of high sustained loads on

compressive strength

l_n Notch length

 $l_{\rm s}$ Distance between notches

 $l_{\rm v}$ Length of timber in front of the notch

mc Moisture content of timber (averaged over the timber cross-section)

 mc_0 Moisture content of timber at time t_c

Maximum moisture content of timber during annual cycles mc_{max} Minimum moisture content of timber during annual cycles mc_{\min} mc_{use} Expected moisture content of timber in use (mean over the year, averaged over the timber cross-section) Variation in moisture content over an annual cycle $mc_{\rm var}$ Fictitious vertical load which represents the effects of inelastic strains on the $p_{\rm sls}$ structure Effective spacing of the connections s_{ef} Spacing of the transverse reinforcement bars in the concrete slab when checking in- S_{f} plane actions in the concrete Longitudinal spacing of the fasteners when checking in-plane shear in the concrete S_1 Maximum spacing of the connections s_{max} Minimum spacing of the connections S_{\min} Transverse spacing of the fasteners when checking in-plane shear in the concrete S_{t} t The time when the concrete achieves the design strength or the time when the design t_0 imposed load is applied to the composite structure, whichever is the earlier Time for design for long-term condition t_{∞} Time according to EN 13670:2009, 8.5(6) when curing and protection of the concrete $t_{\rm c}$ are complete Time of removal of props at tale glatendards (significant) $t_{\rm p}$ /catalog/standards/sist/446e4a24-Age of concrete at which drying shrinkage begins according to EN 1992-1-1:2004, $t_{\rm s}$ 3.1.4(6) Design value of the external loads $q_{\rm d}$ Mean ultimate slip $u_{\rm u,tc}$ Crack width in concrete $w_{\rm k}$ Recommended maximum crack width in concrete EN 1992-1-1:2004, Table 7.1N $w_{\rm max}$ Distance between the centres of gravity of the cross-sections \boldsymbol{Z}

Greek upper-case letters

$\Delta F_{\rm d}$	Design longitudinal shear over a certain length of beam in verification of concrete for in-plane shear (including diaphragm actions)
Δmc	Total change over the annual cycle of the average timber moisture content due to environmental conditions
Δmc^{-}	Reduction in average moisture content in timber over the annual cycle with respect to the expected moisture content in use $mc_{\rm use}$
Δmc^+	Increase in average moisture content in timber over the annual cycle with respect to the expected moisture content in use mc_{use}