

SLOVENSKI STANDARD oSIST prEN ISO 11343:2018

01-julij-2018

Lepila - Ugotavljanje dinamične odpornosti proti cepitvi lepljenih spojev z veliko trdnostjo pod udarnimi pogoji - Metoda z udarnim klinom (ISO/DIS 11343:2018)

Adhesives - Determination of dynamic resistance to cleavage of high-strength adhesive bonds under impact conditions - Wedge impact method (ISO/DIS 11343:2018)

Klebstoffe - Bestimmung des dynamischen Keil-Schlag-Widerstandes von hochfesten Klebungen unter Schlagbelastung - Keil-Schlag-Verfahren (ISO/DIS 11343:2018)

Adhésifs - Détermination de la résistance dynamique au clivage de joints collés à haute résistance soumis aux conditions d'impact - Méthode d'impact au coin (ISO/DIS 11343:2018)

Ta slovenski standard je istoveten z: prEN ISO 11343

ICS:

83.180 Lepila Adhesives

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Adhesives — Determination of dynamic resistance to cleavage of high-strength adhesive bonds under impact wedge conditions — Wedge impact method

Adhésifs — Détermination de la résistance dynamique au clivage de joints collés à haute résistance soumis aux conditions d'impact — Méthode d'impact au coin

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ii

Forewordiv		Page
1	Scope	1
2	Normative references	1
3	Terms and definitions	1
4	Principle	2
5	Apparatus	2
6	Specimens	3
7	Test procedure	6
8	Expression of results	7
9	Precision	
10	Test report	11

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Foreword

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The committee responsible for this document is ISO/TC 61 *Plastics*, Sub-Committee SC 11 *Products*.

This third edition cancels and replaces the second edition which has been technically revised.

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Adhesives — Determination of dynamic resistance to cleavage of high-strength adhesive bonds under impact wedge conditions — Wedge impact method

1 Scope

This International Standard specifies a dynamic impact wedge method for the determination of the cleavage resistance under impact loading of high-strength adhesive bonds between two adherends, when tested under specified conditions of preparation and testing. This test procedure does not provide design information.

The method allows a choice of sheet metal or fiber reinforced plastic substrates corresponding to those materials frequently used in industry, e.g. for automotive applications.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 291, Plastics — Standard atmospheres for conditioning and testing

ISO 10365, Adhesives — Designation of main failure patterns

EN 13887, Structural adhesives — Guidelines for surface preparation of metals and plastics prior to adhesive bonding $\frac{1}{1000} \frac{1}{1000} \frac{$

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

3.1

dynamic resistance to cleavage

force per unit width necessary to bring an adhesive joint to the point of failure by means of a stress applied by a wedge moving between the two substrates of the joint, and thus separating the adherends in a cleaving mode

Note 1 to entry: The dynamic resistance to cleavage is expressed in kilonewtons per metre.

3.2

cracking force

is the maximum after which the force falls to a plateau (typically it is also the highest force measured), it characterizes the beginning of cracking

Note 1 to entry: The cracking force is expressed in newtons.

3.3

dynamic cleavage energy

Is the energy necessary to bring an adhesive joint to the point of failure by means of a stress applied by a wedge moving between the two substrates of the joint, and thus separating the adherends in a peeling mode

Note 1 to entry: The dynamic cleavage energy is expressed in Joule.

4 Principle

The method allows the determination of the average cleavage resistance, expressed as force or energy, of the adhesive bond between two adherends. The cleavage is caused by a wedge, moving at high speed, separating the adherends.

5 Apparatus

5.1 Instrumented impact-testing machine, capable of applying impact energy of at least 50 J and an impact speed of at least 3 m/s. It shall be provided with a suitable grip to hold the specimen. The jaws of this grip shall firmly engage the outer part of the ends of the adherends and shall have provision for positive location of these adherends by means of a hardened-steel bolt passing through the grips and through an 8 mm hole predrilled in the specimens, to clamp the assembly together.

The machine shall be equipped with an instrument capable of registering and storing the force data during the impact event, as a function of time or displacement of the wedge. The response time shall be at least an order of magnitude shorter than the impact event. The machine shall be equipped with a microprocessor/computer in order to perform the necessary calculations for expression of the results. Figure 1 represents a pendulum-type impact machine, using a piezoelectric transducer fixed to the specimen clamp.

- NOTE 1 Falling-weight and servohydraulic-impact machines may be used for this test in addition to pendulum machines. Suitable machines are commercially available.
- NOTE 2 Data collection is controlled by the machine type. A servohydraulic machine provides both force-time and force-displacement data, while pendulum-type or falling-weight machines provide only force-time data. Pendulum-type and falling-weight machines do not necessarily allow the calculation of force-displacement data by double integration. Nevertheless all three machines are usable.
- **5.2 Test wedge**, made of hardened steel, for cleaving the specimen (see Figures 2 and 3, symmetric and asymmetric wedges).

The wedge, attached to its support frame which has a vertical degree of freedom, is pulled through the adhesive joint by the force of the impact on the frame. Because of the degree of freedom, the wedge aligns itself with the adhesive joint during the test. The included angle of the wedge, its leading-edge radius and its maximum depth will determine the progression of opening of the bonded joint ahead of the wedge tip. The wedge surface condition and state of cleanliness shall be maintained and inspected before each test, since friction unduly increases the energy consumed. A deformed, bend, scraped, roughened or otherwise compromised wedge shall be replaced and the respective test shall be discarded.

The three-dimensional diagram in Figure 4 shows the interrelation of the path of the impact head and the positions of the wedge and the test specimen.

- **5.3 Device for measuring thickness**, with an accuracy of \pm 0,01 mm.
- **5.4 Wedge support frame**, consisting of two parallel steel bars with the wedge fixed between them (at one of their ends) and a steel crosshead, for receiving the impact, positioned parallel to the wedge and connected perpendicular to the two bars at their other ends. The bar cross-section shall be 6,0 mm to 6,5 mm wide by 4,5 mm to 5,0 mm high. The total mass of the assembly shall be 820 g \pm 5 g.

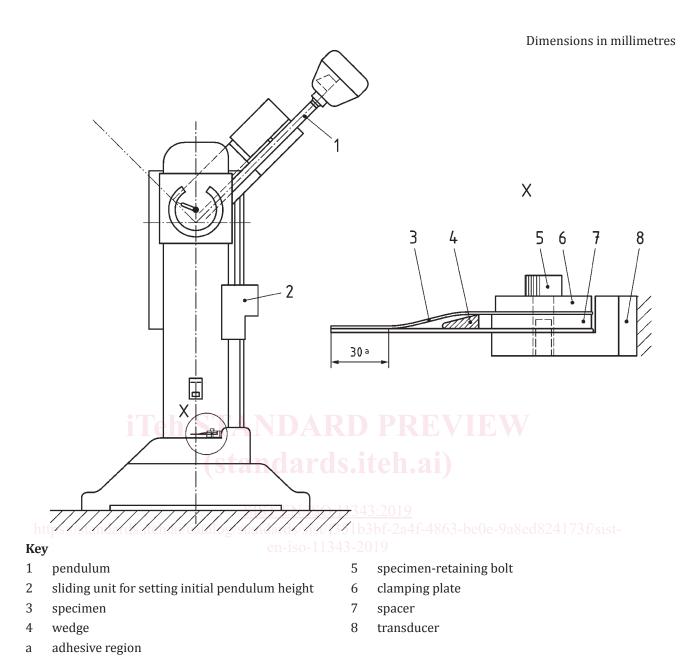


Figure 1 — Example of pendulum-type impact machine

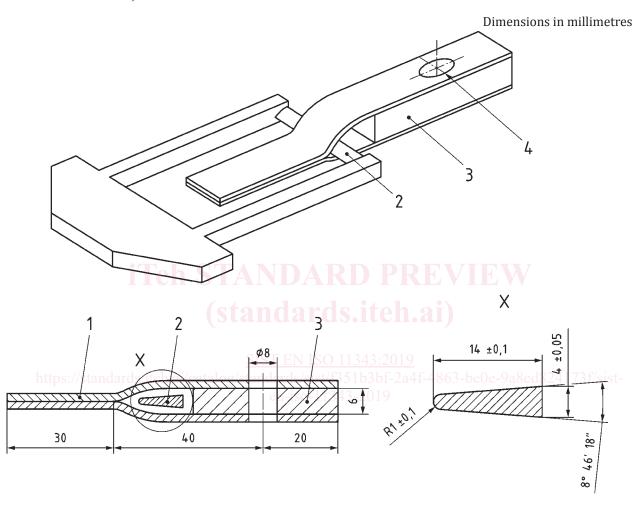
6 Specimens

- **6.1** Specimens of the dimensions shown in Figures 2 and 3 shall be prepared individually, and shall consist of two adherends properly prepared and bonded together.
- **6.2** Surface treatment shall be such as to obtain consistent results in the bonded assembly. Thus the preparation of the surfaces shall be in accordance with either the adhesive manufacturer's instructions

or EN 13887. When a surface contaminant, e.g. oil, is required for the purpose of the test, then it shall be applied in a manner that ensures uniformity between specimens.

The adhesive shall be applied in accordance with the manufacturer's instructions to obtain an optimum bond with minimum variation.

NOTE Direct comparison of different adhesives can be made only when specimen construction, adherend materials and dimensions, and test conditions are identical.



Key

- 1 specimen
- 2 wedge
- 3 spacer
- 4 bolt hole

Figure 2 — Symmetric wedge

6.3 The thickness of the adherends shall be chosen from sheet materials representative of industrial manufacturing and shall fall into the range 0,6 mm to 1,7 mm.

Where two adherends of different thicknesses, materials or yield point are to be tested or if the adherends are of different modulus, the asymmetric wedge shall be employed with the adherent with lower influence on the measurement on the bottom (flat side of the wedge). Usually this is the adherent with either higher modulus or higher yield point or higher thickness. If the adherends are identical, the symmetric wedge shall be employed. The symmetric wedge is not always suitable for high strength