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**Disc springs —**

**Part 1:  
Calculation**

*Ressorts à disques —*

*Partie 1: Calcul*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: [www.iso.org/iso/foreword.html](http://www.iso.org/iso/foreword.html). (standards.iteh.ai)

This document was prepared by Technical Committee ISO/TC 227, *Springs*.

A list of all the parts in the ISO 19690 series can be found on the ISO website.  
ISO 19690-1:2017  
d15/19690-1 series/ can be found on the ISO website. 165103-wb881d2e-895d-069bda04a043/iso-19690-1-2017

# Disc springs —

## Part 1: Calculation

### 1 Scope

This document specifies design criteria and features of disc springs, whether as single disc springs or as stacks of disc springs. It includes the definition of relevant concepts, as well as design formulae, and covers the fatigue life of such springs.

### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 16249, *Springs — Symbols*

ISO 26909, *Springs — Vocabulary*

### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 26909 apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at [www.iso.org/obp](http://www.iso.org/obp)
- IEC Electropedia: available at [www.electropedia.org](http://www.electropedia.org)

### 4 Symbols and units

For the purposes of this document, the symbols and units given in ISO 16249 and [Table 1](#) apply.

**Table 1 — Symbols and units for design calculation**

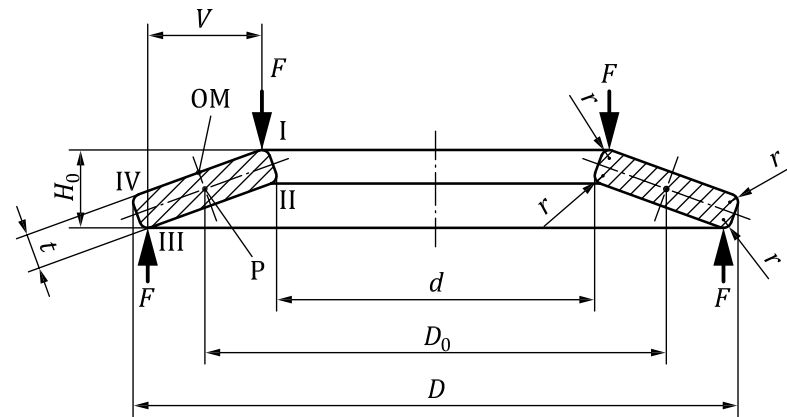
Symbol	Unit	Parameter
$C_1, C_2, C_3, C_4$	—	coefficients
$D$	mm	external diameter of spring
$D_0$	mm	diameter of centre of rotation
$d$	mm	internal diameter of spring
$E$	N/mm <sup>2</sup>	modulus of elasticity of material (carbon steel and carbon alloy steel: 206 000 N/mm <sup>2</sup> ) (other materials: respective modulus of elasticity of material )
$F$	N	spring load
$F_c$	N	design spring load when spring is in the flattened position
$F_G$	N	spring load at the time of combining springs
$F_t$	N	spring test load at $H_t$
$H_t$	mm	height of spring when measuring spring load, $H_t = H_0 - 0,75 h_0$
$H_0$	mm	free height of spring
$h_0$	mm	initial cone height of springs without flat bearings, $h_0 = H_0 - t$
$h_{0,f}$	mm	initial cone height of springs with flat bearings, $h_{0,f} = H_0 - t_f$
$i$	—	number of springs combined in series
$k_1, k_2$	—	coefficients
$L_0$	mm	free height at the time of combining springs
$N$	—	number of cycles for fatigue life
$n$	—	number of springs piled in parallel
OM	—	point at upper surface of the spring perpendicular to the centre line at point P
P	—	theoretical centre of rotation of disc cross section
$R$	N/mm	spring rate
$r$	mm	chamfer radius at edge
$s$	mm	deflection of spring
$s_G$	mm	deflection of stack
$t$	mm	thickness of spring
$t_f$	mm	reduced thickness of single disc spring with flat bearings
$V$	mm	length of lever arms
$V_f$	mm	length of lever arms with flat bearings
$W$	N·mm	energy capacity of springs
$\alpha$	—	ratio of external diameter to internal diameter
$\nu$	—	Poisson's ratio of material
$\sigma_{OM}$	N/mm <sup>2</sup>	stress at position OM
$\sigma_I$	N/mm <sup>2</sup>	stress at position I
$\sigma_{II}$	N/mm <sup>2</sup>	stress at position II
$\sigma_{III}$	N/mm <sup>2</sup>	stress at position III
$\sigma_{IV}$	N/mm <sup>2</sup>	stress at position IV

NOTE N/mm<sup>2</sup> = MPa

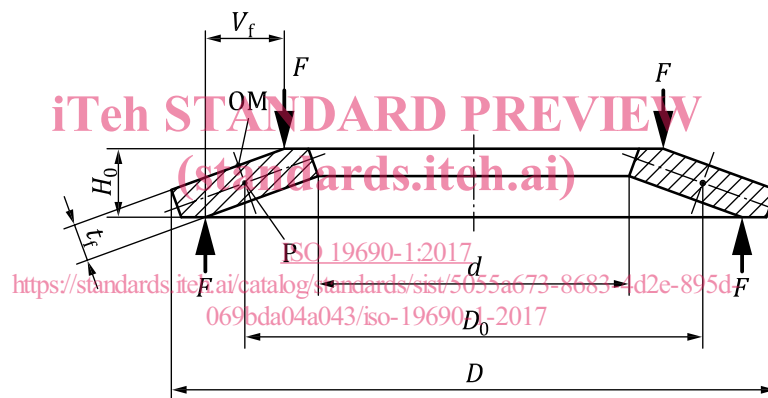
## 5 Dimensions and designation

### 5.1 General

Figure 1 illustrates a single disc spring, including the relevant positions of loading.



a) Without flat bearings: group 1 and group 2



b) With flat bearings: group 3

#### Key

$D$	external diameter of spring	$t$	thickness of spring
$D_0$	diameter of centre of rotation	$V$	length of lever arms
$d$	internal diameter of spring	$V_f$	length of lever arms with flat bearings
$F$	spring load	I	position I
$H_0$	free height of spring	II	position II
OM	point at upper surface of the spring perpendicular to the centre line at point P	III	position III
P	theoretical centre of rotation of disc cross section	IV	position IV
$r$	chamfer radius at edge		
$t_f$	reduced thickness of single disc spring with flat bearings		

Figure 1 — Single disc spring (sectional view), including the relevant positions of loading

### 5.2 Disc spring groups

Table 2 shows disc spring groups.

**Table 2 — Disc spring groups**

Group	$t$ (mm)	With flat bearings and reduced thickness
1	$0,2 \leq t < 1,25$	No
2	$1,25 \leq t \leq 6,0$	No
3	$6,0 < t \leq 14,0$	Yes

**5.3 Dimensional series**

Table 3 shows the dimensional series.

**Table 3 — Dimensional series**

Dimensional series	$h_0/t$	$t_f/t$	$D/t$
A	approximately 0,40	approximately 0,94	approximately 18
B	approximately 0,75	approximately 0,94	approximately 28
C	approximately 1,30	approximately 0,96	approximately 40

**6 Design formulae for springs**

**6.1 General**

The following formulae apply to single disc springs with or without flat bearings, where  $16 < D/t < 40$  and  $1,8 < D/d < 2,5$ . In the case of other designs or materials, it is recommended that the spring manufacturer should be consulted.

**6.2 Test load**

The test load of single disc springs,  $F_t$ , is designed for a deflection  $s = 0,75 h_0$ . Single disc springs with flat bearings shall have the same test load for a test height,  $H_t$ , as ones without, where the principal dimensions  $D$ ,  $d$  and  $H_0$  are the same. Flat bearings have the effect of reducing the length of the lever arm. The increased load which results can be compensated by reducing the thickness of the disc spring. The load/deflection curve of such springs deviates from those without flat bearings, with the exception of the point at which the curves intersect.

**6.3 Coefficients used in calculation**

Coefficients can be given by Formula (1) to Formula (7):

$$\alpha = \frac{D}{d} \tag{1}$$

$$C_1 = \frac{1}{\pi} \times \frac{\left(\frac{\alpha - 1}{\alpha}\right)^2}{\frac{\alpha + 1}{\alpha - 1} - \frac{2}{\ln \alpha}} \tag{2}$$

$$C_2 = \frac{1}{\pi} \times \frac{6}{\ln \alpha} \times \left(\frac{\alpha - 1}{\ln \alpha} - 1\right) \tag{3}$$

$$C_3 = \frac{3}{\pi} \times \frac{\alpha - 1}{\ln \alpha} \tag{4}$$



$$C_4 = \sqrt{-\frac{k_1}{2} + \sqrt{\left(\frac{k_1}{2}\right)^2 + k_2}} \quad (5)$$

where

$$k_1 = \frac{\left(\frac{t_f}{t}\right)^2}{\left(\frac{1}{4} \times \frac{H_0}{t} - \frac{t_f}{t} + \frac{3}{4}\right) \left(\frac{5}{8} \times \frac{H_0}{t} - \frac{t_f}{t} + \frac{3}{8}\right)} \quad (6)$$

$$k_2 = \frac{k_1}{\left(\frac{t_f}{t}\right)^3} \left[ \frac{5}{32} \left(\frac{H_0}{t} - 1\right)^2 + 1 \right] \quad (7)$$

In the case of springs without flat bearings,  $C_4 = 1$ .

In the case of springs with flat bearings,  $C_4$  shall be calculated using [Formula \(5\)](#) and, in all subsequent formulae,  $t_f$  shall be substituted for  $t$  and  $h_{0,f}$  (i.e.  $H_0 - t_f$ ) for  $h_0$ .

Guideline values for the reduction in disc spring thickness as a function of the dimensional series are given in [Table 3](#).

## 6.4 Spring load

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The load can be calculated using [Formula \(8\)](#). In the case of springs without flat bearings,  $C_4 = 1$ .

$$F = \frac{4E}{1-\nu^2} \times \frac{t^4}{C_1 \times D^2} \times C_4^2 \times \frac{s}{t} \times \left[ C_4^2 \times \left(\frac{h_0}{t} - \frac{s}{t}\right) \times \left(\frac{h_0}{t} - \frac{s}{2t}\right) + 1 \right] \quad (8)$$

In the case of springs where there is consideration of chamfer radius at edge, and without flat bearings, the load can be calculated using [Formula \(9\)](#):

$$F = \frac{D-d}{(D-d)-3r} \times \frac{4E}{1-\nu^2} \times \frac{t^3}{C_1 \times D^2} \times s \times \left[ \left(\frac{h_0}{t} - \frac{s}{t}\right) \times \left(\frac{h_0}{t} - \frac{s}{2t}\right) + 1 \right] \quad (9)$$

## 6.5 Design stresses

The design stresses can be calculated using [Formula \(10\)](#) to [Formula \(14\)](#). Positive stresses are tensile stresses and negative stresses are compressive stresses.

$$\sigma_{OM} = -\frac{4E}{1-\nu^2} \times \frac{t}{C_1 \times D^2} \times C_4 \times s \times \frac{3}{\pi} \quad (10)$$

$$\sigma_I = \frac{4E}{1-\nu^2} \times \frac{t}{C_1 \times D^2} \times C_4 \times s \times \left[ -C_4 \times C_2 \times \left(\frac{h_0}{t} - \frac{s}{2t}\right) - C_3 \right] \quad (11)$$

$$\sigma_{II} = \frac{4E}{1-\nu^2} \times \frac{t}{C_1 \times D^2} \times C_4 \times s \times \left[ -C_4 \times C_2 \times \left(\frac{h_0}{t} - \frac{s}{2t}\right) + C_3 \right] \quad (12)$$