

# SLOVENSKI STANDARD oSIST prEN 15776:2019

01-januar-2019

Neogrevane tlačne posode - Zahteve za konstruiranje in izdelavo tlačnih posod in njihovih delov iz litega železa z raztezkom ob porušitvi, enakim ali manjšim kot 15 %

Unfired pressure vessels - Requirements for the design and fabrication of pressure vessels and pressure parts constructed from cast iron with an elongation after fracture equal or less than 15 %

Unbefeuerte Druckbehälter - Anforderungen an die Konstruktion und Herstellung von Druckbehältern und Druckbehälterteilen aus Güsselsen mit einer Bruchdehnung von 15 % oder weniger

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Récipients sous pression non soumis à la flamme : Exigences pour la conception et la fabrication des récipients et parties sous pression moulés en fonte à allongement, après rupture, inférieur ou égal à 15 %

Ta slovenski standard je istoveten z: prEN 15776

ICS:

23.020.32 Tlačne posode Pressure vessels

77.140.80 Železni in jekleni ulitki Iron and steel castings

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# EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

# DRAFT prEN 15776

January 2019

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Will supersede EN 15776:2011+A1:2015

### **English Version**

Unfired pressure vessels - Requirements for the design and fabrication of pressure vessels and pressure vessel parts constructed from cast iron with an elongation after fracture equal or less than 15 %

Récipients sous pression non soumis à la flamme -Exigences pour la conception et la fabrication des récipients et parties sous pression moulés en fonte à allongement, après rupture, inférieur ou égal à 15 % Unbefeuerte Druckbehälter - Anforderungen an die Konstruktion und Herstellung von Druckbehältern und Druckbehälterteilen aus Gusseisen mit einer Bruchdehnung von 15 % oder weniger

This draft European Standard is submitted to CEN members for enquiry. It has been drawn up by the Technical Committee CEN/TC 54.

If this draft becomes a European Standard, CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration.

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Recipients of this draft are invited to submit, with their comments, notification of any relevant patent rights of which they are aware and to provide supporting documentation.

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# **European foreword**

This document (prEN 15776:2019) has been prepared by Technical Committee CEN/TC 54 "Unfired pressure vessels", the secretariat of which is held by BSI.

This document is currently submitted to the CEN Enquiry.

This document will supersede EN 15776:2011+A1:2015.

This document has been prepared under a mandate given to CEN by the European Commission and the European Free Trade Association, and supports essential requirements of EU Directive 2014/68/EU.

For relationship with EU Directive 2014/68/EU, see informative Annex ZA, which is an integral part of this document.

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# Introduction

This standard is a stand-alone document and may be used for pressure equipment with certain restrictions and limitations.

NOTE For the design and fabrication of cast iron pressure equipment standards with higher elongations and ductility, see EN 13445-6:2014.

Attention is drawn to the references to EN 13445-6:2014 for design and fabrication according to specific grades of material standards EN 1563:2018 and EN 13835:2012 which are found in some clauses of this document, prEN 15776. Requirements for the design, material, manufacturing and testing of pressure vessels and pressure vessel parts made from ferritic or austenitic spheroidal graphite cast iron grades with an elongation after fracture higher than 15% are given in EN 13445-6:2014.

Cast iron with elongation after fracture equal or less than 15 % may only be used for pressure equipment when operational and technical advantages are dictating its use instead of the cast iron grades given in EN 13445-6:2014 with elongation after fracture higher than 15 %.

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# 1 Scope

This document specifies requirements for the design, material, manufacturing and testing of pressure vessels and pressure vessel parts made from materials for which details are specified from the following material standards for specific grades which meet the criterion of an elongation after fracture less than or equal to  $15\,\%$ :

- EN 1561:2011, Founding Grey cast irons;
- EN 1563:2018, Founding Spheroidal graphite cast irons;
- EN 13835:2012, Founding Austenitic cast irons.

NOTE The content of the vessel or pressure part is a fluid of group 2 only, according to Directive 2014/68/EU.

#### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN 764-5:2014, Pressure equipment – Part 5: Inspection documentation of metallic materials and compliance with the material specification and an analysis of the material specification and an analysis of the material specific at the material speci

EN 1370:2011, Founding - Examination of surface condition iteh.ai)

EN 1371-1:2011, Founding - Liquid penetrant testing- Part 1: Sand, gravity die and low pressure die kSIST Fpri-N 15776:2019
https://standards.iteh.ai/catalog/standards/sist/3b8b8b6f-e0af-4081-beaa-

EN 1559-1:2011, Founding - Technical conditions of delivery - Part 1: General

EN 1559-3:2011, Founding – Technical conditions of delivery – Part 3: Additional requirements for iron castings

EN 1561:2011, Founding - Grey cast irons

EN 1563:2018, Founding - Spheroidal graphite cast irons

EN 12680-3:2011, Founding - Ultrasonic testing - Part 3: Spheroidal graphite cast iron castings

EN 13445-3:2014, Unfired pressure vessels – Part 3: Design

EN 13445-5:2014, Unfired pressure vessels – Part 5: Inspection and testing

EN 13445-6:2014, Unfired pressure vessels – Part 6: Requirements for the design and fabrication of pressure vessels and pressure parts constructed from spheroidal graphite cast iron

EN 13835:2012, Founding – Austenitic cast irons

EN ISO 8062-3:2007, Geometrical Product Specifications (GPS) – Dimensional and geometrical tolerances for moulded parts – Part 3: General dimensional and geometrical tolerances and machining allowances for castings (ISO 8062-3:2007)

# 3 Terms, definitions, units and symbols

#### 3.1 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at <a href="http://www.electropedia.org/">http://www.electropedia.org/</a>
- ISO Online browsing platform: available at http://www.iso.org/obp

#### 3.1.1

#### grey cast iron

cast material, mainly iron and carbon based, carbon being present mainly in the form of flake (lamellar) graphite particles

Grey cast iron is also known as flake graphite cast iron, and less commonly as lamellar graphite Note 1 to entry: cast iron.

Note 2 to entry: Grey cast irons contain 2,0 % - 4,5 % carbon and 1 % - 3 % silicon. The structure consists of branched and interconnected graphite flakes in a matrix which is pearlite, ferrite or a mixture.

[SOURCE: EN 1561:2011, 3.1, modified — The content of Note 2 to entry was changed.]

#### iTeh STANDARD PREVIEW 3.1.2

spheroidal graphite cast iron (standards.iteh.ai) cast material, mainly iron and carbon-based, the carbon being present mainly in the form of spheroidal graphite particles kSIST FprEN 15776:2019

https://standards.itch.ai/catalog/standards/sist/3b8b8b6f-e0af-4081-beaa-Spheroidal graphite cast iron is also known as ductile iron, and less commonly as nodular iron. Note 1 to entry:

The mechanical properties of grey irons can be greatly improved if the graphite shape is modified if molten iron, having a composition in the range 3,2 % - 4,5 % carbon and 1,8 % - 2,8 % silicon, is treated with magnesium. This produces castings with graphite in spheroidal form instead of flakes, known as nodular, spheroidal graphite or ductile iron. Nodular irons are available with pearlite, ferrite or pearlite-ferrite matrices which offer a combination of greater ductility and higher tensile strength than grey cast irons.

[SOURCE: EN 1563:2018, 3.1, modified — The start of the definition was altered and Note 2 to entry was added.]

#### 3.1.3

#### austenitic cast iron

cast material with an austenitic matrix which is iron and carbon and silicon based and alloyed with nickel and manganese, copper and/or chromium in order to stabilize the austenitic structure at room temperature

Note 1 to entry: The graphite can be present in flake or spheroidal form.

[SOURCE: EN 13835:2012, 3.1, modified — The start of the definition was altered and the final sentence to the definition is now comprised in Note 1 to entry.]

#### 3.1.4

#### relevant wall thickness

wall thickness representative of the casting defined for the determination of the size of the cast samples to which the guaranteed mechanical properties apply

#### 3.1.5

#### critical zone

highly stressed area where a fracture is expected to occur in a burst test

Note 1 to entry: It can be caused, for example, by any of the following:

- sudden change in cross section;
- sharp edges;
- sharp radii;
- peak stresses;
- bending stresses;
- stresses due to other than membrane stress;
- changes in curvature.

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Note 2 to entry: A critical zone is analysed by any appropriate method, e.g. holographic, interferometric method, strain gauge methods, burst test, fatigue testing, FEM analysis, etc. 101.21

Note 3 to entry: Additionally, thermal gradients and thermal stresses due to different operating wall temperatures are to be considered in defining critical zones dards/sist/3b8b8b6f-e0af-4081-beaa-

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#### 3.1.6

#### purchaser

individual or organization that buys pressure equipment, including assemblies or parts, for its own use or on behalf of the user and/or operator

#### 3.1.7

#### manufacturer

individual or organization responsible for the design, fabrication, testing, inspection, installation of pressure equipment and assemblies where relevant

Note 1 to entry: The manufacturer may subcontract one or more of the above mentioned tasks under its responsibility.

#### 3.1.8

#### casting manufacturer

subcontractor that produces the castings used in the manufacture of pressure equipment

#### 3.1.9

#### temperature factor

reduction factor applied to the 0,2 % proof strength to take account of temperature influence

#### 3.1.10

#### wall thickness factor

reduction factor applied to the nominal design stress to take account of reduced mechanical properties

# 3.1.11

# stress factor

ratio of peak stress to total stress

# 3.1.12

# total stress

total stress in a design model which includes all stress concentration effects, non-local and local

# 3.2 Symbols

For the purposes of this document, symbols used in EN 13445-6:2014 are listed in Table 1.

Table 1 — Symbols

| Symbol                           | Quantity   | Unit |
|----------------------------------|--|------|
| С                                | corrosion allowance  | mm   |
| e                                | required thickness   | mm   |
| $e_{\rm a}$                      | analysis thickness   | mm   |
| $e_{ m act}$                     | actual thickness   | mm   |
| $e_{ m max}$                     | maximum local thickness at the location of a possible fatigue crack initiation | mm   |
| $e_{\mathrm{min}}$               | minimum thickness as specified on drawing                                      | mm   |
| f                                | nominal design strestandards.iteh.ai)  | МРа  |
| $f_{ m e}$                       | thickness correction factor  |      |
| $f_{ m m}$                       | mean stress cornection factory/standards/sist/3b8b8b6f-e0af-4081-beaa-         |      |
| $f_{ m test}$                    | nominal design stress for testing condition                                    | МРа  |
| $f_{\mathrm{T}}$                 | temperature correction factor  |      |
| $f_{ m s}$                       | surface finish correction factor   |      |
| $m_{\mathrm{C}}$                 | exponent in equation of fatigue design curve                                   |      |
| n                                | shell shape factor   |      |
| $n_{ m eq}$                      | number of equivalent full pressure cycles                                      |      |
| <i>T</i> , <i>T</i> <sub>c</sub> | calculation temperature  | °C   |
| $A, A_5$                         | minimum elongation after fracture  | %    |
| Cc                               | coefficient in equation of fatigue design curve                                |      |
| C <sub>e</sub>                   | wall thickness reduction factor  |      |
| $C_{\mathrm{T}}$                 | temperature reduction factor   |      |
| E                                | modulus of elasticity  | МРа  |
| F                                | test factor used in experimental fatigue assessment                            |      |
| $K_{ m eff}$                     | effective stress concentration factor  |      |
| Kt                               | theoretical elastic stress concentration factor                                |      |
| М                                | mean stress sensitivity factor   | МРа  |

| Symbol                            | Quantity   | Unit             |
|-----------------------------------|--|------------------|
| $m_{\rm c}$                       | value from appropriate Tables 10, 11, 13, 14 in the appropriate number of cycle number range used in fatigue calculations    |                  |
| N                                 | total number of envisaged types of pressure cycles with different amplitude  |                  |
| $N_{ m all}$                      | allowable number of cycles obtained from the fatigue design curve  |                  |
| $N_{min}$                         | minimum number of cycles obtained in experimental fatigue assessment   |                  |
| $n_{\rm i}$                       | number of cycles with amplitude ΔPi  |                  |
| РС,рс                             | calculation pressure   | MPa <sup>a</sup> |
| $P_{\mathrm{b}}$                  | burst test pressure  | MPa <sup>a</sup> |
| P <sub>b,act</sub>                | actual burst test pressure   | MPa <sup>a</sup> |
| PD,pd                             | design pressure  | MPa <sup>a</sup> |
| $P_{\max}$                        | maximum permissible pressure b   | MPa <sup>a</sup> |
| PS,ps                             | maximum allowable pressure b   | bar a            |
| <i>PT</i> , <i>p</i> <sub>t</sub> | test pressure b iTeh STANDARD PREVIE   | MPa              |
| R <sub>m</sub>                    | minimum tensile strength (standards iteh ai)   | МРа              |
| $R_{\rm p0,2}$                    | minimum 0,2 % - proof strength   | МРа              |
| Rp <sub>0,2/T</sub>               | minimum 0,2 % - proof strength at temperature T in degrees https://standards.iteh.a/catalog/standards/sist/3b8b8b6f-e0af-408 | 1MPa             |
| $R_{\rm z}$                       | surface roughness parameter – peak – to - valley height  | μm               |
| $R_{M}$                           | material strength parameter  | МРа              |
| RM3                               | average strength from 3 tensile test samples   | МРа              |
| S                                 | safety factor  |                  |
| $TS_{\max}$ , $TS_{\min}$         | maximum / minimum allowable temperature  | °C               |
| V                                 | volume   | L                |
| ΔΡ                                | pressure range   | MPa <sup>a</sup> |
| $\Delta P_{ m i}$                 | pressure cycle amplitude   |                  |
| Δσ                                | allowable stress range   | MPa              |
| $\Delta\sigma^*$                  | pseudo elastic stress range  | MPa              |
| $\Delta\sigma_{\text{Cut}}$       | cut-off limit  | MPa              |
| $\Delta\sigma_{ m D}$             | endurance limit  | МРа              |
| $\Delta\sigma_{eq,struc}$         | structural stress range  | МРа              |
| $\Delta\sigma_{R}$                | stress range in fatigue design curve   | MPa              |
| δ                                 | casting tolerance  | mm               |
| ε                                 | extra thickness due to casting process   | mm               |
|                                   | I .  |                  |

| Symbol           | Quantity   | Unit |  |
|------------------|--|------|--|
| $\gamma_{ m R}$  | partial safety factor  |      |  |
| η                | Stress factor  |      |  |
| ν                | Poisson's ratio  |      |  |
| $\sigma_{\rm e}$ | nominal design stress for external pressure  | МРа  |  |
| a MPa for        | MPa for calculation purposes only, otherwise the unit shall be bar (1 MPa = 10 bar). |      |  |
| b See also       | See also EN 13445-3:2014, Table 4-1.   |      |  |

# 3.3 Inter relation of thicknesses definitions (EN 13445-6:2014)



#### Key

- required thickness e
- analysis thickness  $e_{a}$
- minimum thickness including corrosion allowance as indicated on drawings  $e_{\mathrm{min}}$
- actual thickness  $e_{
  m act}$
- corrosion allowance С
- extra thickness due to casting process ε
- δ casting tolerance

Figure 1 — Inter-relation of thicknesses definitions

# Materials, limitations and service conditions

# 4.1 Materials and limitations on temperature, maximum allowable pressure and energy content

All material grades subject to internal or external pressure shall comply with EN 1561:2011 for grey cast iron, EN 1563:2018 for spheroidal graphite cast iron and EN 13835:2012 for austenitic cast iron. The material grades and corresponding limitations are given in Table 2 and Table 3.