INTERNATIONAL STANDARD

ISO 11274

Second edition 2019-09

Soil quality — Determination of the water-retention characteristic — Laboratory methods

Qualité du sol — Détermination de la caractéristique de la rétention en eau — Méthodes de laboratoire

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Published in Switzerland

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Foreword

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The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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This document was prepared by Technical Committee ISO/TC 190, *Soil quality,* Subcommittee SC 3, *Chemical methods and soil characteristics*. ISO 11274:2019

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This second edition cancels and replaces the first edition (ISO 11274:1998), which has been technically revised. It also incorporates the Technical Corrigendum ISO 11274:1998/Cor. 1:2009.

Introduction

Soil water content and matric pressure are related to each other and determine the water-retention characteristics of a soil. Soil water which is in equilibrium with free water is at zero matric pressure (or suction) and the soil is saturated. As the soil dries, matric pressure decreases (i.e. becomes more negative), and the largest pores empty of water. Progressive decreases in matric pressure will continue to empty finer pores until eventually water is held in only the finest pores. Not only is water removed from soil pores, but the films of water held around soil particles are reduced in thickness. Therefore a decreasing matric pressure is associated with a decreasing soil water content [9][10]. Laboratory or field measurements of these two parameters can be made and the relationship plotted as a curve, called the soil water-retention characteristic. The relationship extends from saturated soil (approximately 0 kPa) to oven-dry soil (about -10^6 kPa).

The soil water-retention characteristic is different for each soil type. The shape and position of the curve relative to the axes depend on soil properties such as texture, density and hysteresis associated with the wetting and drying history. Individual points on the water-retention characteristic may be determined for specific purposes.

The results obtained using these methods can be used, for example:

- to provide an assessment of the equivalent pore size distribution (e.g. identification of macro- and micropores);
- to determine indices of plant-available water in the soil and to classify soil accordingly (e.g. for irrigation purposes);
- to determine the drainable pore space (e.g. for drainage design, pollution risk assessments);
- to monitor changes in the structure of a soil (caused by e.g. tillage, compaction or addition of organic matter or synthetic soil conditioners);

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- to ascertain the relationship between the negative matric pressure and other soil physical properties (e.g. hydraulic conductivity, thermal conductivity);
- to determine water content at specific negative matric pressures (e.g. for microbiological degradation studies);
- to estimate other soil physical properties (e.g. hydraulic conductivity).

Soil quality — Determination of the water-retention characteristic — Laboratory methods

1 Scope

This document specifies laboratory methods for determination of the soil water-retention characteristic.

This document applies only to measurements of the drying or desorption curve.

Four methods are described to cover the complete range of soil water pressures as follows:

- a) method using sand, kaolin or ceramic suction tables for determination of matric pressures from 0 kPa to -50 kPa;
- b) method using a porous plate and burette apparatus for determination of matric pressures from 0 kPa to -20 kPa;
- c) method using a pressurized gas and a pressure plate extractor for determination of matric pressures from -5~kPa to -1~500~kPa;

Guidelines are given to select the most suitable method in a particular case.

2 Normative references ISO 112742019

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There are no normative references in this document. 74-2019

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at https://www.iso.org/obp
- IEC Electropedia: available at http://www.electropedia.org/

3.1

soil water-retention characteristic

relation between soil water content and soil matric head of a given soil (sample)

3.2

pressure

pressure equivalent of soil water potential

3.3

matric pressure

amount of work done in order to transport, reversibly and isothermally, an infinitesimal quantity of water, identical in composition to the soil water, from a pool at the elevation and the external gas pressure of the point under consideration, to the soil water at the point under consideration, divided by the volume of water transported

3.4

water content mass ratio

 $m_{\rm w}$

mass of water evaporating from the soil when dried to constant mass at 105 °C, divided by the dry mass of the soil (i.e. the ratio between the masses of water and solid particles within a soil sample)

3.5

water content volume fraction

 φ_{x}

volume of water evaporating from the soil when dried to constant mass at 105 °C, divided by the original bulk volume of the soil (i.e. the ratio between the volume of liquid water within a soil sample and the total volume including all pore space of that sample)

Note 1 to entry: The soil water-retention characteristic is identified in the scientific literature by various names including soil water release curve, soil water-retention curve, pF curve and the capillary pressure-saturation curve. Use of these terms is deprecated.

Note 2 to entry: The Pascal is the standard unit of pressure but many other units are still in use. <u>Table A.1</u> provides conversions for most units.

Note 3 to entry: Sometimes suction is used instead of pressure to avoid the use of negative signs (see Introduction). However, this term can cause confusion and is deprecated as an expression of the matric pressure.

Note 4 to entry: For swelling and shrinking soils, seek the advice of a specialist laboratory since interpretation of water-retention data will be affected by these properties.

iTeh STANDARD PREVIEW 4 Guidelines for choice of method (standards.iteh.ai)

4.1 General

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Guidelines are given belowhto help selecting/the most suitable method in a particular case.

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4.2 Sand, kaolin or ceramic suction tables for determination of pressures from 0 kPa to $-50~\mathrm{kPa}$

The sand, kaolin and ceramic suction table methods are suitable for large numbers of determinations at high pressures on cores or aggregates of different shapes and sizes. Analyses on samples of a wide range of textures and organic matter contents can be carried out simultaneously since equilibration is determined separately for each core. The suction table methods are suitable for a laboratory carrying out analyses on a routine basis and where regular equipment maintenance procedures are implemented.

4.3 Porous plate and burette apparatus for determination of pressures from 0 kPa to -20 kPa

The porous plate and burette apparatus allow analysis of only one sample at a time, and several sets of equipment are therefore necessary to enable replication and full soil profile characterization. The method is particularly suited to soils with weak structures and sands which are susceptible to slumping or slaking, since minimal sample disturbance occurs. Capillary contact is not broken during the procedure and all samples, particularly soils with higher organic matter content or sandy textures, will equilibrate more rapidly using this technique. This is a simple technique suitable for small laboratories.

4.4 Pressure plate extractor for determination of pressures from -5 kPa to -1 500 kPa

The pressure plate method can be used for determinations of all pressures to $-1\,500$ kPa. However, different specifications of pressure chambers and ceramic plates are required for the range of pressures, e.g. 0 kPa to -20 kPa, -20 kPa to -100 kPa and -100 kPa to $-1\,500$ kPa. The method is, however, best suited to pressures of -33 kPa or lower, since air entrapment at high negative pressures can occur. It is preferable that soils with similar water-release properties are analysed together to ensure equilibration

times are approximately the same, though in practice it may be difficult. Sample size is usually smaller than for the previous two methods and therefore the technique is less suitable for heterogeneous soil horizons, or for those with a strong structural composition. Analysis of disturbed soils is traditionally carried out using this method.

4.5 Pressure membrane cells for determination of pressures from -33 kPa to -1 500 kPa

The pressure membrane cell should only be used for pressures below -33 kPa. Capillary contact at higher pressures is not satisfactory for this method. The method is appropriate for all soil types though the use of double membranes is recommended for coarse (sandy) textured soils. Sample size can be selected (according to the size of the pressure cell) to take into account soil structure. Different textures can be equilibrated separately using a suite of cells linked to one pressure source.

5 Sampling

5.1 General requirements

It is essential that undisturbed soil samples are used for measurement at the high matric pressure range 0 kPa to -100 kPa, since soil structure has a strong influence on water-retention characteristics. Use either undisturbed cores or, if appropriate, individual peds for low matric pressure methods (<-100 kPa).

Soil cores shall be taken in a metal or plastic sleeve of a height and diameter such that they are representative of the natural soil variability and structure. The dimensions of samples taken in the field are dependent on the texture and structure of the soil and the test method to be used. Table 1 provides guidance on suitable sample sizes for the different methods and soil structure.

Take soil cores carefully to ensure minimal compaction and disturbance to structure, either by hand pressure in suitable material or by using a suitable soil corer. Take a minimum of three representative replicates for each freshly exposed soil horizon or layer; more replicates are required in stony soils. Record the sampling date, sample grid reference, horizon and sampling depths. Dig out the sleeve carefully with a trowel, trim roughly the two faces of the cylinder with a knife and if necessary, adjust the sample within the sleeve before fitting lids to each end, and label the top clearly with the sample grid reference, the direction of the sampling (horizontal or vertical), horizon number and sample depth.

Wrap the samples (e.g. in plastic bags) to prevent drying. Wrap aggregates (e.g.in aluminium foil or plastic film) to retain structure and prevent drying. Alternatively, excavate blocks measuring approximately 30 cm cube of undisturbed soil in the field, wrap in metal foil, wax (to retain structure and prevent drying) and take to the laboratory for subdivision. Store the samples at 1 $^{\circ}$ C to 2 $^{\circ}$ C to reduce water loss and suppress biological activity until they are required for analyses. Treat samples having obvious macrofaunal activity with a suitable biocide, e.g. 0,05 % copper sulfate solution.

Other relevant site information should be noted, e.g. soil water status, topsoil/surface conditions, etc. (see <u>5.2</u>).

Table 1 — Recommended sample sizes (height × diameter) for the different test methods

Dimensions in millimetres

Test method	Structure			
rest method	Coarse	Medium	Fine	
Suction table	50 × 100	40 × 76	24 × 50	
Porous plate	50 × 76	40 × 76	20 × 36	
Pressure plate	_	10 × 76	10 × 50	

Table 1 (continued)

Test method	Structure			
rest method	Coarse	Medium	Fine	
Pressure membrane	_	20 × 76	10 × 50	

NOTE 1 The points mentioned here are specific to water-retention analyses. Reference is made to ISO 18400-101 in which general advice on sampling and problems encountered is given.

NOTE 2 In moist conditions, soil is easier to sample and in shrink/swell soils the bulk density under natural conditions is lowest. It is therefore preferable to take samples in the wet season when soil matric pressures are at or near –5 kPa. Especially clayey soils, are difficult to core when dry and they shrink and swell with varying water content. Samples of swelling and shrinking soils can be taken in cores only under completely saturated conditions, i.e. under the water table and in the full capillary zone. In all other circumstances peds can be taken.

5.2 Sample preparation

To prepare samples for water-retention measurements at pressures greater than -50 kPa (see Clause 3), trim undisturbed cores flush with the ends of the container and replace one lid with a circle of polyamide (nylon) mesh, similar close-weave material or paper if the water-retention characteristic is known, secured with an elastic band. The mesh will retain the soil sample in the sleeve and enable direct contact with the soil and the porous contact medium. Avoid smearing the surface of clayey soils. Remove any small projecting stones to ensure maximum contact and correct the soil volume if necessary. Replace the other lid to prevent drying of the sample by evaporation. Prepare soil aggregates for high matric pressure measurements by levelling one face and wrapping other faces in aluminium foil to minimize water loss. Disturbed soils should be packed into a sleeve with a mesh attached. Firm the soil by tapping and gentle pressure to obtain a specified bulk density.

Weigh the prepared samples. Ensure that the samples are brought to a pressure of less than the first equilibration point by wetting them, if necessary by capillary rise, mesh side or levelled face down on a sheet of foam rubber saturated with 0,005 mgl/h calcium sulfate solution or tap water. Weigh the wet sample when a thin film of water is seen on the surface. This water content represents the total or maximum water-holding capacity and is calculated according to 6.5.

The water-retention characteristic of swelling and shrinking soils should be determined under the same load as that occurring in the field. Otherwise the laboratory data can deviate from the water-retention characteristic of the soil under natural field conditions.

The time required for wetting varies with initial soil water content and texture, being a day or two for sands and two weeks or more for clayey soils. Except for sands, wetting needs to be slow to prevent air entrapment in samples. Care should be taken not to leave sandy soils wetting for too long because their structure may collapse. Low-density subsoil sands without the stabilizing influence of organic matter or roots are the most susceptible. The burette method is most suitable for this type of soil and samples can be wetted using the procedure in <u>6.3</u>. Soils should, ideally, be field-moist when the wetting is commenced; dried soils may cause differences in the water-retention characteristic due to hydrophobia or hysteresis.

General guidelines for wetting times are:

- Sand 1 d to 5 d
- Loam 5 d to 10 d
- Clayd to 14 d or longer
- Peat 5 d to 20 d

Increasing temperature causes a decrease in water content at a given pressure. It is recommended that all water-retention measurements be made at a constant temperature of (20 ± 2) °C. Report the temperature at which the water-retention measurements are made.

- NOTE 1 It can be necessary to discard samples with large projecting stones.
- NOTE 2 Very coarse pores are not water-filled when the soil sample is saturated by capillary rise.

6 Determination of the soil water characteristic using sand, kaolin and ceramic suction tables

6.1 Principle

A negative matric pressure is applied to coarse silt or very fine sand held in a rigid watertight nonrusting container (a ceramic sink is particularly suitable). Soil samples placed in contact with the surface of the table lose pore water until their matric pressure is equivalent to that of the suction table. Equilibrium status is determined by weighing samples on a regular basis and soil water content by weighing, oven drying and reweighing. The maximum negative pressure which can be applied before air entry occurs is related to the pore size distribution of the packed fine sand or coarse silt which is determined by the particle size distribution, the shape of the particles and their consolidation.

6.2 Apparatus

- **6.2.1 Large ceramic sink** or other watertight, rigid, non-rusting container with outlet in base [dimensions about $(50 \times 70 \times 25)$ cm] and with close-fitting cover.
- **6.2.2 Tubing** and connecting pieces to construct the draining system for the suction table. ISO 11274:2019
- 6.2.3 Sand, silt or kaolin, as packing material for the suction table.

Commercially available graded and washed industrial sands with a narrow particle size distribution are most suitable. The particle size distributions of some suitable sand grades and the approximate suctions they can attain are given in <u>Table 2</u>. It is permissible to use other packing materials, such as fine glass beads or aluminium oxide powder, if they can achieve the required air entry values.

- **6.2.4 Levelling bottle**, stopcock and 5 l aspirator bottle.
- **6.2.5** Tensiometer system (optional).
- **6.2.6 Drying oven,** capable of maintaining a temperature of (105 ± 2) °C.
- **6.2.7 Balance,** capable of weighing with an accuracy of 0.1 % of the measured value.

NOTE Examples of a drainage system, sand and kaolin suction tables and details of their construction are described in Annex A.

Туре	Coarse sand	Medium sand	Fine sand	Silica flour
Use	Base of suction tables	Surface of suction tables (-5 kPa matric pressure)		Surface of suction ta- bles (-21 kPa matric pressure)
Typical particle size distribution Per			content	
>600 μm	1	1	1	0

Table 2 — Examples of sands and silica flour suitable for suction tables

Table 2 (continued)

Type	Coarse sand	Medium sand	Fine sand	Silica flour
200 μm to 600 μm	61	8	1	0
100 μm to 200 μm	36	68	11	1
63 μm to 100 μm	1	20	30	9
20 μm to 63 μm	1	3	52	43
<20 μm	0	0	5	47

6.3 Preparation of suction tables

Prepare suction tables using packing material that can attain the required air entry values (see <u>Table 2</u>). In <u>Annex A</u> the detailed procedure for one specific type of suction table is given as an example.

6.4 Procedure

Prepare soil cores as described in <u>5.2</u>. Weigh the cores and then place them on a suction table at the desired matric pressure. Leave the cores for 7 d. The sample is then weighed, and thereafter weighed as frequently as needed to verify that the daily change in mass of the core is less than 0,02 %. The sample is then regarded as equilibrated and is moved to a suction table of a lower pressure or oven dried. Samples which have not attained equilibrium should be replaced firmly onto the suction table and the table cover replaced to minimize evaporation from the table.

The time for reaching equilibrium is proportional to the square of the height of the sample but, as a guide, cores normally require at least 7 d to equilibrate at each potential and sometimes 20 days or more. A minimum of 7 d is recommended so that samples establish good capillary connectivity, enabling an equilibrium status to be more rapidly attained.

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6.5.1 Procedure for soils containing less than 20 % stones (diameter greater than 2 mm)

6.5.1.1 Calculate the water content mass ratio at a matric pressure $p_{\rm m}$ using Formula (1):

$$m_{\rm w}\left(p_{\rm m}\right) = \frac{m(p_{\rm m}) - m_{\rm d}}{m_{\rm d}} \tag{1}$$

where

 $m_{\rm w}(p_{\rm m})$ is the water content mass ratio at a matric pressure $p_{\rm m}$, in grams;

 $m(p_{\rm m})$ is the mass of the soil sample at a matric pressure $p_{\rm m}$, in grams;

 $m_{\rm d}$ is the mass of the oven-dried soil sample, in grams;

6.5.1.2 Calculate the water content on volume basis at matric pressure $p_{\rm m}$ using Formula (2):

$$\varphi_{\rm w}(p_{\rm m}) = \frac{m(p_{\rm m}) - m_{\rm d}}{V \cdot \rho_{\rm w}} \tag{2}$$

where