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# Standard Test Method for Contamination Outgassing Characteristics of Spacecraft Materials<sup>1</sup>

This standard is issued under the fixed designation E 1559; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\varepsilon$ ) indicates an editorial change since the last revision or reapproval.

# 1. Scope

1.1 This test method covers a technique for generating data to characterize the kinetics of the release of outgassing products from materials. This technique will determine both the total mass flux evolved by a material when exposed to a vacuum environment and the deposition of this flux on surfaces held at various specified temperatures.

1.2 This test method describes the test apparatus and related operating procedures for evaluating the total mass flux that is evolved from a material being subjected to temperatures that are between 298 and 398 K. Pressures external to the sample effusion cell are less than  $7 \times 10^{-3}$  Pa ( $5 \times 10^{-5}$  torr). Deposition rates are measured during material outgassing tests. A test procedure for collecting data and a test method for processing and presenting the collected data are included.

1.3 This test method can be used to produce the data necessary to support mathematical models used for the prediction of molecular contaminant generation, migration, and deposition.

1.4 All types of organic, polymeric, and inorganic materials can be tested. These include polymer potting compounds, foams, elastomers, films, tapes, insulations, shrink tubing, adhesives, coatings, fabrics, tie cords, and lubricants.

1.5 There are two test methods in this standard. Test Method A uses standardized specimen and collector temperatures. Test Method B allows the flexibility of user-specified specimen and collector temperatures, material and test geometry, and user-specified QCMs.

1.6The values stated in SI units are to be regarded as the standard.

1.6 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.7 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

#### 2. Referenced Documents

2.1 ASTM Standards:

#### <u>ASTM E1559-09</u>

E177Practice for Use of the Terms Precision and Bias in ASTM Test Methods<sup>-2</sup> E 595 Test Method for Total Mass Loss and Collected Volatile Condensable Materials from Outgassing in a Vacuum Environment

<u>IEEE/ASTM SI 10American National Standard for Use of the International System of Units (SI): The Modern Metric System<sup>2</sup></u> <u>Test Method for Total Mass Loss and Collected Volatile Condensable Materials from Outgassing in a Vacuum Environment</u> 2.2 *Military Standard:* 

<u>MIL-P-27401C MIL-P-27401D</u> Propellant Pressurizing Agent, Nitrogen<sup>3</sup> 2.3 *Other Standard:* 

SMC-TR-95-28 Non-Volatile Residue Solvent Replacement, Report No. TR95 (5448)-14

#### 3. Terminology

3.1 Definitions:

Vol 14.02-volume information, refer to the standard's Document Summary page on the ASTM website.

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Current edition approved May 10, 2003. Published June 2003. Originally approved in 1993. Last previous edition approved in 2000 as E1559–00. Current edition approved April 1, 2009. Published May 2009. Originally approved in 1993. Last previous edition approved in 2003 as E 1559–03. <sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For\_Annual Book of ASTM Standards

<sup>&</sup>lt;sup>3</sup> Available from Standardization Documents Order Desk, Bldg. 4 Section D, 700 Robbins Ave., Philadelphia, PA 19111-5094, Attn: NPODS.

<sup>&</sup>lt;sup>4</sup> Available from Standardization Documents Order Desk, Bldg. 4 Section D, 700 Robbins Ave., Philadelphia, PA 19111-5094, Attn: NPODS.

<sup>&</sup>lt;sup>4</sup> Available from The Aerospace Corporation, P.O. Box 92957, Los Angeles, CA 90009–2957, http://www.aero.org.

3.1.1 AT cut crystal, n—a quartz crystal orientation that minimizes the temperature coefficient (frequency change versus temperature) over a wide range of temperature.

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<u>3.1.2</u> *azeotropic mixture*, *n*—a solution of two or more liquids, the composition of which does not change upon distillation. Also known as azeotrope.

3.1.23.1.3 collected volatile condensable material, CVCM, n—(from Test Method E 595). The quantity of outgassed matter from a test specimen that condenses on a collector maintained at a specific constant temperature for a specified time and measured before and after the test outside the chamber.

## 3.1.2.1

<u>3.1.3.1</u> *Discussion*—CVCM is specific to Test Method E 595 and is calculated from the condensate mass determined from the difference in mass of the collector plate before and after the test in a controlled laboratory environment. CVCM is expressed as a percentage of the initial specimen mass. The view factor is not considered; so all the VCM outgassing from the sample may not be collected. Care should be used in comparing the CVCM from Test Method E 595 with VCM from this test method.

# 3.1.3

<u>3.1.4</u> *differential scanning calorimetry, DSC, n*—a technique in which the difference in energy inputs into a substance and a reference material is measured as a function of temperature while the substance and reference material are subjected to a controlled-temperature program.

### <del>3.1.4</del>

<u>3.1.5</u> *effusion cell*, *n*—a container, placed in a vacuum, in which a sample of material can be placed and heated to some specified temperature.

<del>3.1.4.1</del>

<u>3.1.5.1</u> *Discussion*—The container has a cylindrical orifice at one end so that evolving gases exit the cell in a controlled manner. The effusion cell dimensions and orifice size are specified such that there is free molecular flow of the evolving gases and a predictable molecular flux from the orifice.

<del>3.1.5</del>

3.1.6 mass flux, n—the mass of molecular flux.

3.1.6 ITCH Sta

<u>3.1.7</u> molecular flux (molecules  $cm^{-2} \cdot s^{-1}$ ), *n*—the number of gas molecules crossing a specified plane in unit time per unit area. 3.1.7

<u>3.1.8</u> nonvolatile residue, NVR, n—the quantity of residual molecular and particulate matter remaining following the filtration of a solvent containing contaminants and evaporation of the solvent at a specified temperature.

#### <del>3.1.8</del>

<u>3.1.9</u> outgassing, *n*—the evolution of gas from a material, usually in a vacuum. Outgassing also occurs in a higher pressure environment.

#### <del>3.1.9</del>

<u>3.1.10</u> *quartz crystal microbalance, QCM, n*— a device for measuring small quantities of mass using the properties of a quartz crystal oscillator.

# <del>3.1.9.1</del>

<u>3.1.10.1</u> *Discussion*—The resonant frequency of a quartz crystal oscillator is inversely proportional to the thickness of the crystal. When the mass of a uniform deposit is small relative to the mass of the crystal, the change in frequency is proportional to the mass of the deposit.

# 3.1.10

<u>3.1.11</u> QCM thermogravimetric analysis, QTGA, n—a technique in which a QCM is heated at a constant rate to remove a collected deposit.

3.1.10.1

<u>3.1.11.1</u> *Discussion*—This is performed to determine the evaporation characteristics of the species in the deposit. The mass of the deposit on the QCM is recorded as a function of time or temperature.

# <del>3.1.11</del>

3.1.12 residual gas analyzer, RGA, n-a mass spectrometer mounted inside or attached to a vacuum chamber.

3.1.11.1

3.1.12.1 Discussion-RGA can be used for identifying gases in the vacuum chamber.

<del>3.1.12</del>

<u>3.1.13</u> total mass flux  $(g \cdot cm^{-2} \cdot s^{-1})$ , *n*—the summation of the mass from all molecular species crossing a specified plane in unit time per unit area.

3.1.133.1.14 total mass loss, TML, n—total mass of material outgassed from a test specimen that is maintained at a specified constant temperature and operating pressure for a specified time and measured within the test chamber. TML is expressed as a percentage of the initial specimen mass. In addition, TML can be normalized with respect to the sample surface area and be expressed as  $\mu g/cm^2$ .

<del>3.1.13.1</del>



3.1.14.1 in-situ TML, n—calculated from the mass deposited on a cryogenically cooled QCM and the view factor from the effusion cell orifice to the QCM.

## 3.1.13.2

<u>3.1.14.2</u> *Discussion*—In-situ TML is a function of the outgassing test time and is expressed as a percentage of the initial specimen mass. This is not necessarily the same as the TML determined by Test Method E 595.

# 3.1.13.3

3.1.14.3 ex-situ TML, n—total mass of material outgassed from a test specimen that is maintained at a specified constant temperature and operating pressure for a specified time and measured outside the test chamber.

# <del>3.1.13.4</del>

<u>3.1.14.4</u> *Discussion*—Ex-situ TML is calculated from the mass of the specimen as measured before and after the test in a controlled laboratory environment and is expressed as a percentage of the initial specimen mass. (From Test Method E 595.)  $\frac{3.1.14}{2.1.14}$ 

<u>3.1.15</u> total outgassing rate, *n*—the net rate of mass loss from a material sample as a result of outgassing. Total outgassing rate can be normalized per unit sample surface area and expressed as  $g \cdot cm^{-2} \cdot s^{-1}$  or it can be normalized per unit initial sample mass and expressed as  $g \cdot g^{-1} \cdot s^{-1}$ .

# 3.1.15

<u>3.1.16</u> volatile condensable material, VCM, n— the matter that outgasses from a material and condenses on a collector surface that is at a specified temperature.

#### 3.1.15.1

<u>3.1.16.1</u> *Discussion*—For this test method, this is the quantity of outgassed matter from a test specimen that condenses on surfaces maintained at QT2 or QT3. The VCM is calculated from the mass deposited on QCM2 or QCM3 and the view factor from the effusion cell orifice to the QCMs. VCM is a function of the outgassing test time and is expressed as a percentage of the initial specimen mass. In addition, VCM can be normalized with respect to the sample surface area and be expressed as  $\mu g/cm^2$ . This is not the same as CVCM as determined by Test Method E 595 (see <u>3.1.23.1.3</u>).

3.2 Acronyms:Acronyms:

3.2.1 GN<sub>2</sub>, *n*—gaseous nitrogen.

3.2.2  $LN_2$ , *n*—liquid nitrogen.

3.2.3 *MAPTIS*, *n*—Materials and Process Technical Information Service.

3.3 Definitions of Terms Specific to This Standard:

3.3.1 QCM1—the QCM that is operating at the temperature TQ1 (cryogenic) for measuring the total outgassing rate.

3.3.2 *QCM2 and QCM3*—the QCMs that are operating at temperatures TQ2 and TQ3 for the measurement of the deposition of outgassing matter.

#### 4. Summary of Test Method

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4.1 The test apparatus described in this test method is designed to measure outgassing rate data that can be used to develop kinetic expressions for use in models that predict the evolution of molecular contaminants and the migration and deposition of these contaminants on spacecraft surfaces. Materials that contain volatile species that will be outgassed under the temperature and vacuum conditions of this test method can be characterized. The quartz crystal microbalances used in this test method provide a sensitive technique for measuring very small quantities of deposited mass. In addition to providing data for kinetic expressions, the reduced data can be used to compare the outgassing behavior of different materials for material selection purposes.

4.2 There are two test methods in this standard. Test Method A is the standard procedure using prescribed configurations and temperatures. Test Method B allows for the use of spacecraft system specific temperatures, configurations, and QCM collector surface finishes.

4.3 The measurements are made by placing the material sample in an effusion cell so that the outgassing flux leaving the cell orifice will impinge on three QCMs which are arranged to view the orifice. A fourth QCM is optional. The effusion cell is held at a constant temperature in the high vacuum chamber and has a small orifice directed at the QCMs. The QCMs are controlled to selected temperatures. The total outgassing rate is determined from the collection rate on a cryocooled QCM. At the end of the isothermal test, the QCMs are heated in a controlled manner to determine the evaporation characteristics of the deposits.

4.4 The effusion cell is loaded from the vacuum interlock chamber to the main test chamber and is positioned at a fixed distance and angle with respect to the QCM surfaces. The effusion cell is temperature controlled to provide constant and uniform heating of the sample. The vacuum interlock chamber is a device that enables the expedient introduction of the test sample into the high vacuum of the main test chamber. Use of the interlock chamber to load and unload samples prevents loss of vacuum in the main chamber and diminishes the need to pump it down before each test.

4.5 The QCM collection method for measuring the total outgassing rate from a sample is an indirect technique. Rather than directly measuring sample mass loss, the basic measurement is the fraction of the flux that condenses on the cryogenically cooled QCM collector at a point in the outgassing flow field. That point in the flow field is defined as the geometric location of the QCM relative to the effusion cell orifice, which is at a fixed location. To determine the rate of sample mass loss from the rate of QCM collection, the view factor from the QCM to the effusion cell orifice and the angular distribution of flux leaving the orifice must be determined. This relationship can be calculated from the apparatus geometry and the effusion cell orifice dimensions.

4.6 A QCM thermogravimetric analysis (QTGA) test is also included in the procedure. This technique heats the QCMs at a constant rate to measure evaporation characteristics of the deposits collected on the QCMs. The QTGA also provides an effective means to clean the QCM surfaces before subsequent tests.

4.7 It is critical to the posttest analysis that the material sample be completely described and specified, so that the outgassing characteristics can be applied to the material when used on a spacecraft. It is also necessary so that any material sample can be properly compared with that of other samples. The outgassing rate of the material will, in general, be determined by its composition, processing history, and environmental conditioning before the test. All test sample processing should be representative of normal material processing and usage. All materials are environmentally conditioned to specified conditions. However, samples may be subjected to environmental conditions that are expected during actual use. Test sample processing and conditioning history shall be included in the test report.

4.8 Because outgassing of all materials is, to some extent, diffusion rate controlled, the outgassing rate of a test sample depends on the distance from the sample interior to a free surface. Hence, the geometry of a test sample must be controlled in a specified manner to permit meaningful interpretation of the data. When possible, the sample geometry should be in the specified configuration to simplify modeling. However, the material sample can be made with the same geometry as it would have in an actual application.

# 5. Test Apparatus

5.1 *Description*—The test apparatus consists of four main subsystems: a vacuum chamber, a temperature control system, internal configuration, and a data acquisition system. Fig. 1 is a schematic of the systems, and Fig. 2 shows the vacuum chamber and internal configuration.

5.2 Vacuum Chamber—The principal components of the vacuum chamber are the main test chamber, the vacuum interlock chamber, and cryogenic shrouds (for example,  $LN_2$ ). A high-vacuum gate valve is used to isolate the main test chamber from the interlock chamber. This allows the effusion cell to be withdrawn or inserted into the main chamber without the loss of high vacuum in the main chamber. High-vacuum electrical and mechanical feedthroughs are used to access the interior of the chamber.

5.3 Internal Configuration—Three quartz crystal microbalances (QCMs) (a fourth QCM is optional), an effusion cell, and cryogenic heat sinks in the chamber are the principal components. The cryogenic heat sinks are used to ground the QCMs thermally and to cool shrouds which surround the effusion cell and QCMs. The cold shrouds limit molecular contaminant fluxes to the line-of-sight outgassing flux from the effusion cell orifice to the collector QCMs. The cryogenic heat sink system ( $LN_2$  reservoirs) and shrouds, effusion cell, and QCMs are shown in Fig. 2.



FIG. 1 Data System and Control Schematic



5.3.1 The QCMs are thermally shielded from each other so that the temperatures of each can be controlled independently. Each QCM has its own temperature sensing and control system.

5.3.2 Each QCM contains two crystals (one for mass collection and one for reference), the oscillator electronics, and a temperature sensor. The QCM crystals shall have optically polished surfaces (60/40 cerium polish). Uncoated, aluminum electrodes shall be used for the sensing and reference crystals.

NOTE 1—The quantitative effect of the surface finish on the deposition rates is not known at this time. A diffuse surface has more surface area than a polished surface resulting in more conservative (higher) values of contaminant accumulation, especially with monolayer thicknesses. However, diffuse surfaces are difficult to reproduce and clean uniformly, resulting in unwanted test variability. Future round-robin tests will be used to evaluate the effects of surface finish on the results.

NOTE 2—Aluminum electrodes are easy to apply and to clean. If it is desirable to measure deposition on a simulated optical surface, a QCM that simulates the surface roughness and composition of the optical surfaces may be used in Test Method B. Future round-robin tests will be used to evaluate the effects of surface composition on the results.

5.3.3 The QCMs are thermally connected to a cryogenic heat sink (that is,  $LN_2$ ), and heaters provide the temperature control above the base temperature ( $\leq 90$  K). The QCMs shall be controllable from the set points specified in 9.3 or 9.4 to 398 K and maintained to within  $\pm 0.5$  K of the desired temperature.

5.3.4 The required sensitivity of the QCM to mass deposits depends upon the required precision of the mass measurements. Sensitivity is a function of the crystal cut, temperature, and natural frequency of the quartz crystals. QCMs used for this test method shall have a sensitivity of at least  $1 \times 10^{-8}$  g·cm<sup>-2</sup>·Hz<sup>-1</sup> at 298 K. Table 1 shows the theoretical sensitivities of quartz crystals. Shows the theoretical sensitivities of quartz crystals (1).<sup>5</sup> The sensitivity of the QCMs shall be sufficient to measure the incident mass fluxes required to perform the test.

NOTE 3—QCMs with 10- or 15-MHz crystals are typically used. The sensitivities in Table 1 assume that the areas of the electrodes on both sides of a crystal are the same.

5.3.5 The QCMs are arranged symmetrically so that each QCM has the same view factor to the effusion cell orifice. The QCMs are angled  $10 \pm 0.5^{\circ}$  off the normal to the plane of the effusion cell orifice so that the axes of the QCMs intersect at a common point that coincides with the location of the effusion cell orifice when the cell is placed in its standard position. The distance from the effusion cell orifice to each QCM collector surface is  $150 \pm 1$  mm.

NOTE 4—This QCM to collector surface geometry is mandated for Test Method A. See 9.1 for Test Method B, allowing nonstandard geometries and test conditions.

NOTE 5-The QCMs shall be placed so that the active surface of any QCM cannot "see" the active surface of any other QCM.

5.3.6 The effusion cell is cylindrical and the recommended dimensions are  $\frac{65-65}{5} \pm 5$ -mm inside diameter by 50  $\pm 5$  mm in depth. Effusion cell dimensions shall accommodate the standard sample geometries described in Section 8. The flux distribution

<sup>&</sup>lt;sup>5</sup> Wrought aluminum alloys such as the 2000 and 6000 series can be used.

<sup>&</sup>lt;sup>5</sup> The boldface numbers in parentheses refer to a list of references at the end of this standard.

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TABLE 1 AT or Rotated Cut Crystal with Identical Electrode Areas on Each Side of the Crystal

Natural Frequency (f), MHz	Sensitivity at 298 K ( $K_s$ ), g·cm <sup>-2</sup> ·Hz <sup>-1</sup>
10	$4.42 imes10^{-9}$
15	$1.96 imes10^{-9}$
20	$1.10  imes 10^{-9}$

of the outgassing products leaving the effusion cell is controlled by the cylindrical orifice in the top of the effusion cell. The orifice  $\mathbf{I}$  size shall be  $3.0-3.0 \pm 0.1$ -mm diameter by  $3.0-3.0 \pm 0.1$ -mm long.

NOTE 6-This orifice size is mandated for conformance to this test method.

5.3.7The cell shall be machined from aluminum<sup>5</sup> or copper for high thermal conductivity. The cell shall have an integral heater and temperature sensor. The integral heater shall be capable of uniformly heating the effusion cell to 398K within 20 min after inserting the cell into the main vacuum chamber.

5.3.7 The cell shall be machined from aluminum (Note 7) or copper (Note 8) for high thermal conductivity. The cell shall have an integral heater and temperature sensor. The integral heater shall be capable of uniformly heating the effusion cell to 398 K within 20 min after inserting the cell into the main vacuum chamber.

Note 7—Wrought aluminum alloys such as the 2000 and 6000 series can be used.

NOTE 8-OFHC (oxygen free, high conductivity) copper has been found to be satisfactory.

5.3.8 Effusion cell temperatures shall be controlled to within  $\pm 0.5$  K.

5.3.9 The positioning mechanism shall place the exit plane of the effusion cell orifice at a distance of  $150 \pm 1$  mm from the surface of the sensing crystal in each QCM.

5.3.10 A shroud, cooled with a cryogenic heat sink, shall surround the effusion cell to minimize the reflection of molecular flux from the chamber wall to the QCMs. A shutter may be used over the orifice to isolate the QCMs from the molecular flux.

5.4 *Temperature Control System*—All temperatures of the effusion cell and the QCMs are maintained by independently controlled heaters to a precision of  $\pm 0.5$  K or better. In addition to maintaining temperatures at selected specific values, the controller for the QCMs shall be capable of performing ramp functions, in which temperatures are increased at a constant rate of 1 K per minute.

NOTE<del>7—Users</del> <u>9—Users</u> should be aware that the QTGA heating rate can affect the test data. A heating rate of 1 K per minute was selected for practicality. 1 K per minute was found to provide good agreement with the predicted evaporation rates of water using vapor pressure data. Higher rates showed significant errors. This is covered in Footnote 7:Ref (2). Lower rates have also shown differences but will result in long, impractical test times.

5.5 *Data Acquisition System*—Data acquisition, storage, and manipulation can be accomplished by any method that is capable of measuring the frequencies of the QCMs, the temperatures of the QCMs and the effusion cell, and the times of data collection at specified intervals. Experimental or processed data shall be stored for later retrieval for further analysis. An automated, computer operated data collection system is recommended.

#### 6. Support Equipment/Materials

6.1 Analytical Microbalance, with a 30 g or greater tare, a readability of 10  $\mu$ g or better, and a precision of  $\pm$ 10  $\mu$ g is required for recording mass changes of the samples.

6.2 Oil-Free Aluminum Foil, is recommended as a nonoutgassing substrate.

6.3 *High Purity, Low NVR Solvents* are required for cleaning the effusion cell and other hardware before insertion into the vacuum chamber. Suitable reagent grade solvents include acetone, methanol, ethanol, 1,1,1 trichloroethane (methyl chloroform), and 75/25% mixture of methyl chloroform and ethanol. are required for cleaning the effusion cell and other hardware before insertion into the vacuum chamber. Suitable reagent grade solvents include acetone, methanol, ethanol, ethanol, and an azeotropic mixture of ethyl acetate (47 % volume) and cyclohexane (53 % volume).

NOTE 10—Methyl chloroform, used in these practices, is toxic, and is being phased out for many applications. Methyl chloroform has been replaced in this edition of these practices. The replacement solvents were selected based on tests and analyses performed by The Aerospace Corporation and described in SMC-TR-95–28.

6.3.1 Low NVR hexane or toluene is required to clean QCM surfaces.

NOTE8—Some QCMs may use materials on the electrodes that are not compatible with some solvents. Cleaning instructions from the QCM manufacturer should be followed.

6.3.2Swabs shall be extracted to have a low NVR. <u>11</u>—Some QCMs may use materials on the electrodes that are not compatible with some solvents. Cleaning instructions from the QCM manufacturer should be followed. 6.3.2 Swabs shall be extracted to have a low NVR.

NOTE 12-Commercial swabs may be acceptable but should be tested before use for NVR and suitability for this application.