

Designation: D409/D409M - 09

Standard Test Method for Grindability of Coal by the Hardgrove-Machine Method¹

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This standard has been approved for use by agencies of the Department of Defense.

INTRODUCTION

This test method is structured into the following parts:

The body of the test method discusses the scope, referenced documents, significance and use, apparatus, gross samples, preparation of test samples, procedure, calculation and report, precision and bias, and keywords.

Annex A1 through Annex A5 contain the methods used to prepare, homogenize, and assign HGI values to the international HGI reference materials (primary HGI RMs) and to calibrate an individual laboratory's HGI machine using these HGI RMs.

Annex A1 contains the method to obtain and prepare international HGI standard reference coal sample feedstock for potential use as international (primary) HGI RMs (reference materials).

Annex A2 contains the method to divide and containerize the candidate international HGI standard reference coal samples (candidate RMs) prepared from the feedstock prepared in Annex A1.

Annex A3 contains the method for homogeneity testing of the candidate international HGI standard reference coal samples (candidate RMs) containerized in Annex A2.

Annex A4 contains the method for determining the Hardgrove grindability index (HGI) to be assigned to each lot of the candidate international HGI standard reference coal samples (RMs).

Annex A5 contains the method used to calibrate the individual laboratory's Hardgrove grindability machine using the international HGI RMs.

Annex A6 through Annex A10 contain the methods used to prepare, homogenize, and assign HGI values to the national HGI reference materials (secondary HGI RMs) and to calibrate a national HGI machine using the international (primary) HGI RMs.

Annex A6 contains the method to obtain and prepare national HGI standard reference coal sample feedstock for potential use as national (secondary) HGI RMs (reference materials).

Annex A7 contains the method to divide and containerize candidate national HGI standard reference coal samples (candidate national RMs) prepared from the feedstock prepared in Annex A6.

Annex A8 contains the method for homogeneity testing of candidate national HGI standard reference coal samples (candidate national RMs) containerized in Annex A7.

Annex A9 contains the method for determining the Hardgrove grindability index to be assigned to each lot of the candidate national HGI standard reference coal samples (national RMs).

Annex A10 contains the method to calibrate a national Hardgrove machine using the international (primary) HGI RMs.

Annex A11 contains the method for determining the moisture content of the 1.18×0.60 mm (No. 16×30) test sample.



1. Scope

1.1 This test method² covers the determination of the relative grindability or ease of pulverization of coals in comparison with coals chosen as standards. A prepared and sized sample receives a definite amount of grinding energy in a miniature pulverizer, and the size consist of the pulverized product is determined by sieving. The resultant size consist is used to produce an index relative to the ease of grinding (Hardgrove Grindability Index (HGI)).

1.1.1 Some coals, such as some high-volatile bituminous, subbituminous, and lignite coals, can undergo physical change as the natural or seam moisture is released during handling and preparation. This change is often sufficient to alter the grindability characteristics that will be reported when tested in the laboratory and could produce different indices dependent on the conditions of drying and the moisture level of the 1.18-mm by 600-µm (No. $16 \times$ No. 30) (see Test Method D4749D4916) materials used for the test. Therefore, the repeatability and reproducibility cited in this test method may not apply for these high-volatile bituminous, subbituminous, and lignite coals.

1.2 The values stated in either SI units or inch-pound units are to be regarded separately as standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in non-conformance with the standard.

1.3 It is recognized that the term *weight* is considered equivalent to *mass* as used in this test method.

1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

2.1 ASTM Standards:³

D2013 Practice for Preparing Coal Samples for Analysis

D4749 Test Method for Performing the Sieve Analysis of

Coal and Designating Coal Size

D4916 Practice for Mechanical Auger Sampling⁴

D6609 Guide for Part-Stream Sampling of Coal

D6883 Practice for Manual Sampling of Stationary Coal from Railroad Cars, Barges, Trucks, or Stockpiles ⁵

D7256/D7256M Practice for Mechanical Collection and Within-System Preparation of a Gross Sample of Coal

from Moving Streams⁴

E11 Specification for Woven Wire Test Sieve Cloth and Test Sieves ⁵

E826 Practice for Testing Homogeneity of a Metal Lot or Batch in Solid Form by Spark Atomic Emission Spectrometry

Note 1—Part stream samples should be used for this test only if all parties find part stream sampling acceptable.

Note 2—If the topsize of the final sample product produced from a mechanical sampling system (whether auger, cross-stream, or cross-belt) is smaller than 4.75 mm (No. 4), the sample is unsuitable for this test procedure.

3. Significance and Use

3.1 This test method develops a measurement of grinding or pulverizing characteristics that can be used to evaluate the yield, or energy input, or both, required in a grinding or pulverizing process.

4. Apparatus

4.1 Air-Drying Oven [for air-drying the 1000 g, 4.75 mm (No. 4) sample]—A device for passing slightly heated air over the sample. The oven shall be capable of maintaining a temperature of 10 to 15°C [18 to 27°F] above room temperature with a maximum oven temperature of 40°C [104°F] unless ambient temperature is above 40°C, in which case ambient temperature shall be used. In the case of easily oxidized coals, the temperature shall not be over 10°C [18°F] above room temperature unless ambient temperature is above 37°C [100°F] in which case ambient temperature shall be used. Air changes shall be at the rate of 1 to 4 air volumes of oven capacity per minute.

4.2 Drying Pans [for air-drying the 1000 g, 4.75 mm (No. 4) sample]—Drying pans of sufficient size so that the sample may be spread to a depth of not more than 25 mm [1.0 in.] with sides not more than 38 mm [1.5 in.] high. The pans shall be nonreactive with coal and unaffected by the method of air drying selected.

4.3 Balance [for weighing the 1000-g sample before and after air-drying and the sieve fractions formed during stage-crushing]—With a sensitivity of 0.5 g in 1000 g and sufficient capacity to weigh a \geq 1000-g sample along with the drying pan.

4.4 Balance [for weighing the 50-g test sample and the sieve fractions formed during milling]—With a sensitivity of 10 mg and a minimum capacity of 800 g.

Note 3—A single balance meeting the specifications of 4.3 and 4.4 is permitted.

- 4.5 *Calibration Weights*—These calibration weights shall be used to monitor the response of each balance over the range of normal use each time HGIs are determined.
- 4.6 Sample Divider— An enclosed riffle divider with feed chute as described in Practice D2013 is required and shall be used. Alternatively, a rotary sample divider, which has been proven to be free of significant bias, may be used.
- 4.7 Standard Sieves—A working set of circular, standard testing sieves, which are 203 mm [8 in.] in diameter and conform to Specification E11, are required in the following sizes, together with cover and catch pan (receiver):

² For information concerning the experimental work on which this test method is based, see paper by Hardgrove, R. M., "Grindability of Coal," *Transactions*, American Society of Mechanical Engineers, Vol 54, F.S.P., p. 37, 1932.

D05.07.02 on Grindability is conducting ongoing investigations in regard to quality control during preparation, distribution, and use of standard reference materials and during preparation and testing of actual samples.

³ For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

⁴ Withdrawn. The last approved version of this historical standard is referenced on www.astm.org.

⁵ Withdrawn. The last approved version of this historical standard is referenced on www.astm.org.

TABLE 1 Standard Sieves for HGI Testing

E11 Specification	U.S.A. Standard Sieve Series Designation
16.0 mm	5⁄8 in.
4.75 mm	No. 4
2.36 mm	No. 8
1.18 mm	No. 16
600 μm	No. 30
75 μm	No. 200

4.7.1 These working sieves must be periodically inspected for wear or damage. Any excessively worn or damaged sieves (for example, sieves with holes, tears, cracks; see Note 4) must be replaced immediately, and the HGI calibration procedure must be repeated after the damaged sieves are replaced (see Annex A5). Since the HGI depends upon the sieve analysis and since the 75-µm (No. 200) sieve is fragile, it is recommended that at least one set of working sieves be obtained, identified, and used exclusively for HGI determinations and that only this exclusive set of sieves be used.

Note 4—Excessive wear may be indicated by poor repeatability or by failure of quality control checks (A5.4.1.1) to agree reasonably with the initial calibration data.

4.7.2 Normal wear on sieves is compensated by the use of international HGI standard reference samples (HGI RMs) and proper calibration of equipment; excessive wear (such as holes or tears in the sieve cloth, and so forth) is not compensated by HGI RMs. Because excessive wear is unacceptable, inspect sieves carefully before each test to ensure the absence of excessive wear. For the 75- and 600-μm (No. 200 and 30) sieves, use only a soft-bristled brush (such as short-bristled camel hair) for brushing and cleaning.

Note 5—It is good practice to keep a separate primary 75-µm (No. 200) check sieve to be used only to check the 75-µm (No. 200) working sieve described in 4.7.1 when the working sieve becomes suspect. This check is done by running a comparative HGI test between the two 75-µm (No. 200) sieves. Use of the working sieve for HGIs should be discontinued if HGI difference between the sieves is greater than 1 HGI unit.

4.8 *Crusher*—A laboratory plate mill capable of reducing 4.75-mm (No. 4) sieve size coal particles with the production of a minimum of minus 600-μm (minus No. 30) sieve size material (Note 6). The crusher plates shall be serrated and about 100 mm [4 in.] in diameter (Note 7). The distance between the plates shall be adjustable, and the relative speed of rotation of the plates shall not exceed 200 r/min.

Note 6—Evidence from HGI standard reference sample user-response forms (A5.4.4) indicates that the median value of % Yield (8.3) of the 4.75-mm (No. 4) material as 1.18-mm by 600-µm (Nos. 16 by 30) material, regardless of the HGI level, is about 55 %. Use this median value to gage the effectiveness/efficiency of the stage-crusher and of the stage-crushing process.

Note 7—The most frequently used plate mill can be equipped with "fine" or "coarse" plates. One independent study⁶ has found evidence of differences in percent recovery resulting from use of different types of plate. Only the coarse plate should be used in preparation of both HGI calibration standards and unknown samples.

4.9 Mechanical Sieving Machine—The mechanical sieving machine shall accept an assembly of vertically nested circular sieves of 203 mm [8 in.] in diameter, together with cover and

receiver. The machine shall simulate the motions given testing sieves during hand sieving by imparting a horizontal oscillatory motion of approximately 28-mm [1.1-in.] amplitude at a rate of approximately 300 oscillations or cycles per minute (cpm). Simultaneously, the top of the oscillating assembly is struck at a rate of approximately 150 blows per minute by a weight of 1.9 kg [4.2 lb] moving through a vertical distance of approximately 28 mm [1.1 in.] under the influence of gravity.

4.10 Grindability Machine—The Hardgrove Grindability Machine such as is shown in Fig. 1 is required for this test. Essential tolerances and specifications are shown in Fig. 2. The grindability machine includes a stationary grinding bowl of polished cast iron, with a circular horizontal track that holds eight polished steel balls, each 25.40 \pm 0.13 mm [1.000 \pm 0.005 in.] in diameter. The balls are driven by an upper grinding ring which is rotated at 20 ± 1 r/min by means of the upper spindle and which, in turn, is driven by an electric motor through reduction gears and, in newer models, belts. Weights are added to the driving spindle so that the total vertical force on the balls as a result of the weights, shaft, top grinding ring, and gear is equal to 29.0 ± 0.2 kg [64 ± 0.5 lb]. The machine is equipped with a counter and automatic device which can be properly adjusted for stopping the machine after 60 ± 0.25 revolutions.

Note 8—It is good laboratory practice to have the dimensions and the tolerances of the grinding balls verified by a qualified machine shop (or equivalent) on an annual basis.

4.10.1 The position of the counter trip mechanism before and after the test must be used to determine the number of revolutions completed. Sometimes, it may be necessary to position strategically the counter trip mechanism at the beginning of the test to accomplish the desired number of revolutions (that is, watch where the trip mechanism is initially, count the number of revolutions from the point of origin, determine where the trip mechanism is at the end of the test, and determine if the specified 60 ± 0.25 revolutions are obtained. If not, adjust the position of the trip mechanism at the beginning of the test until the specified number of revolutions are obtained).

5. Gross Samples

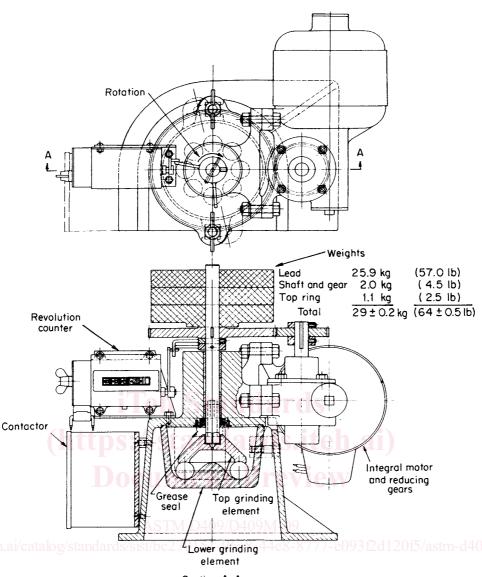
5.1 Collect a gross sample of coal, representative of the material from which it is taken, in accordance with Practice D4916 (Note 2), D6883, or D7256/D7256M (Note 2) or Guide D6609 (Note 1), and prepare the sample in accordance with Practice D2013 except that the sample topsize shall not be reduced beyond the 4.75-mm (No. 4) sieve and the sample shall weigh at least 1000 g.

6. Preparation of Test Samples

- 6.1 Prepare a 1.18-mm \times 600- μ m (No. 16 \times No. 30) test sample for establishing the HGI of HGI RMs (Annex A4 and Annex A9), for calibration (Annex A5 and Annex A10), or for routine determination of HGI.
- 6.2 When necessary, divide the quantity of 4.75-mm (No. 4) sieve size coal to not less than 1000-g lots using an enclosed riffle or rotary sample divider, and air dry each sample in

⁶ D05.07 Minutes, J. Gardner, Georgia Power and G. Linton, October 1990.





Section A-A
FIG. 1 Hardgrove Grindability Machine

conformance with Practice D2013. To calculate the % Yield (8.3), record the mass of the air-dried sample (W₁).

6.3 Sieve the entire amount (1000 g) of air-dried 4.75-mm (No. 4) sieve size sample in lots of no greater than 250 g for 2 min \pm 10 s in the mechanical sieving machine. Use a set of nested sieves consisting of a 1.18-mm (No. 16) sieve on top of a 600- μ m (No. 30) sieve. Weigh and record the mass of each sieve size.

Note 9—Include a 4.75-mm (No. 4) and a 2.36-mm (No. 8) sieve in this nest of sieves to record the particle size distribution and to verify that the topsize of the sample is appropriate for this test.

6.4 Stage crush the material retained on the 1.18-mm (No. 16) sieve with the crusher adjusted so that only the largest particles are crushed. Sieve the crushed material in portions of no greater than 250 g for 2 min \pm 10 s in the mechanical sieving machine. Return the oversize to the crusher, after setting the crusher so that only the largest particles are crushed. Continue the stage crushing and sieving procedure until all the

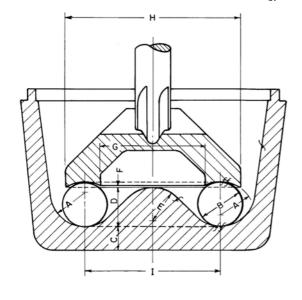
material passes the 1.18-mm sieve. Retain the 1.18-mm \times 600- μ m (No. 16 \times No. 30) material. After all stage-crushing is completed, to calculate the % Yield (8.3), record the mass of the 1.18-mm \times 600- μ m (No. 16 \times No. 30) fraction (W.)

6.5 Mix well all the 1.18-mm \times 600- μ m (No. 16 \times No. 30) material accumulated from the stage crushing and sieving and divide the quantity using an enclosed riffle or rotary sample divider to obtain approximately 120 \pm 10 g.

6.6 As the final step in preparation of the test sample, dedust the 120- \pm 10-g sample from 6.5 by sieving on a 600- μ m (No. 30) sieve for 5 min \pm 10 s using the mechanical sieving machine.

7. Procedure

7.1 Clean the grindability machine thoroughly, place the machine on a level surface, and space the balls as evenly as possible around the grinding bowl. Set the automatic stopping



f Smooth machined surface
ff Fine machined surface and polished

SECTIONAL VIEW

 $A = 19.05 \pm 0.13 \text{ mm} [0.750 \pm 0.0005 \text{ in.}] \text{ radius}$ $B = 25.40 \pm 0.13 \text{ mm} [1.000 \pm 0.0005 \text{ in.}] \text{ diameter}$ C = 12.70 mm [0.50 in.] D = 22.23 mm [0.875 in.] E = 19.05 mm [0.750 in.] F = 1.42 mm [0.078 in.] G = 60.33 mm [2.375 in.] G = 60.34 mm [3.875 in.] G = 60.35 mm [3.875 in.]

FIG. 2 Grinding Elements of Hardgrove Machine

device so that the motion of the grindability machine will stop after 60 ± 0.25 revolutions of the upper grinding ring.

7.1.1 If the grindability machine makes a different number of revolutions other than the specified 60 ± 0.25 revolutions, the machine must be adjusted to within the tolerance specified. (This is normally done by strategically placing the counter tripper arm at the start of the test.)

7.2 Weigh 50 \pm 0.01 g of the 1.18-mm \times 600- μ m (No. 16 \times No. 30) sieve size dedusted material from 6.6 and distribute it evenly in the grinding bowl, brushing any material that falls on the elevated section of the lower grinding element into the lower grinding element, which contains the balls. Fasten the bowl in position and make sure the load is fully applied to the driving spindle.

7.3 Operate the machine for the specified 60.00 ± 0.25 revolutions.

7.4 Remove the bowl from the machine, lift out the upper grinding ring, and carefully brush adhering coal dust from the

bowl and grinding ring onto a 16-mm [5/8-in.] sieve nested on a 75-µm (No. 200) sieve and a closely fitting receiving pan. Carefully empty the contents of the bowl onto the 16-mm [5/8-in.] sieve (Note 10). Brush off material adhering to the balls and remove them from the 16-mm [5/8-in.] sieve. Brush material adhering to the 16-mm [5/8-in.] sieve, including the underside of the sieve, onto the 75-µm (No. 200) sieve. Replace the 16-mm [5/8-in.] sieve with a close-fitting cover and shake the nested 75-µm (No. 200) sieve; cover and pan for 10 $\min \pm 10$ s in a mechanical sieving machine. After the 10-min ± 10-s period, carefully brush coal dust from the underside of the 75-µm (No. 200) sieve into the receiving pan using a soft-bristled brush to avoid damaging the sieve. Repeat the shaking of the ball-milled material and the cleaning of the underside of the 75-µm (No. 200) sieve for two more periods each of 5-min \pm 10-s duration.

Note 10—Before emptying the contents of the lower grinding bowl onto the 16-mm [5%-in.] sieve, the tops of the grinding balls may be brushed and then removed from the lower grinding bowl by use of a magnetic extraction tool. Each grinding ball is brushed off and set aside; then, the pulverized coal is emptied from the bowl onto the 16-mm [5%-in.] sieve

7.5 Weigh separately to the nearest 0.01 g the coal retained on the 75- μ m (No. 200) sieve (W_o) and the coal passing the 75- μ m (No. 200) sieve [W_u].

7.5.1 Alternatively, predetermine the tare weights of the 75-µm (No. 200) sieve ($W_{\rm sieve}$) and the catch pan ($W_{\rm pan}$). After the sieving of 7.4, weigh the 75-µm (No. 200) sieve and its contents ($W_{\rm sieve+}$). Subtract the tare mass to obtain the mass of the +75-µm (+No. 200) material = $W_{\rm o} = W_{\rm sieve+} - W_{\rm sieve}$. Weigh the catch pan and its contents ($W_{\rm pan+}$). Subtract the tare mass to obtain the mass of the -75-µm (-No. 200) material = $W_{\rm u} = W_{\rm pan+} - W_{\rm pan}$.

7.6 If the sum of the +75- μ m (+No. 200) (W_o) and the -75- μ m (-No. 200) (W_u) sieve fraction masses differs by more than 0.50 g from the initial weight of 50 \pm 0.01 g (W_i), reject the test and repeat. Use the calculated weight of the coal passing the 75- μ m (No. 200) sieve (W_c), determined by subtracting the weight retained on the 75- μ m (No. 200) sieve (W_o) from the test specimen weight (W_i), in determining the sum-of-least-squares fit (A5.4.3), in preparation of the calibration chart (A5.4.3.2) or in calculation of the grindability index of the sample (8.1) W_c = W_i - W_o.

8. Calculation and Report

8.1 Calculate the grindability index corresponding to the calculated weight of test specimen passing the 75- μ m (No. 200) sieve (7.5) directly from the equation of the line prepared in A5.4.3 and report to the nearest whole number.

8.2 For ease of comparison between or among laboratories, calculate and report the percent residual moisture in the 1.18-mm by 600-μm (No. 16 by No. 30) sample (Annex A11).

8.3 Calculate the % Yield of 1.18-mm by 600-µm (No. 16 by No. 30) material generated from the initial 1000 g of 4.75-mm (No. 4) top-size sample and compare the actual value to a typical median value (4.8, Note 6) to gage the effectiveness/efficiency of the stage-crusher and of the stage-crushing process.

Sample I.D.:	Date:	Analyst:	
Sample Description:			
2000 / 500 W 19440 - 60 W 1 44 CO			
	AIR-DRYING		
Air-dry pan mass, (a) :	g	Ambient Temp :	°C [°F]
Initial sample and air-dry pan wt, (b) :	g	Time into oven :	
Final sample and air-dry pan mass, (c):	g	Time out of oven :	
Air-dried sample mass, c - a, (d) :	g	Temperature :	°C [°F
Mass loss on drying, b - c, (e):	g	Heat on at :	
Initial sample mass, b - a, (f) :	g	Heat off at :	
% Mass loss on drying, e/f x 100%, (g):	%	Fan on at:	
		Fan off at :	
INIT	TAL SIEVED WEIGHT	TS	
+4.75mm (+No.4), (h) :	g	1.18x0.600mm (No.16x30), (k) :	
4.75x2.36mm (No.4x8), (i):	g	-0.600mm (-No.30), (I):	
2.36x1.18mm (No.8x16), (j) :	g	Topsize:	
Total recovered mass after sieving, $(h+l+j+k+l)$, (m) :	g		-
Mass loss on sieving, d - m, (n):	g		
% Mass loss on sieving, (n/d) x 100%, (o):	%		
REDUCT	TON OF +1.18mm [+	No. 161	
	+1.18mm (+No. 16)		.18mm (+No. 16)
Initially, h + i + j, (p):	g	>6th crushing of oversize, (v):	g
>1st crushing of oversize, (q):	g	>7th crushing of oversize, (w) :	g
>2nd crushing of oversize, (r) :	100750	>8th crushing of oversize, (x):	g
>3rd crushing of oversize, (s):		>9th crushing of oversize, (y):	g
>4th crushing of oversize, (t):		>10th crushing of oversize, (z):	
>5th crushing of oversize, (u):	765.50	,,,,,,,,	
Final total wt of 1.18x0.600mm (No.16x30), (A) :			
	g		
Final total wt of -0.600mm (-No.30), (B) :	g		
Final total recovered wt, (A+B), (C):			
Loss on crushing, (m-C), D:			
% loss on crushing, (D/d) x 100%, (E):	%		
% Yield of 1.18x0.600mm (No.16x30), A/d x 100%, (F):	- %		
DEDUSTING 120g OF 1.	18 x 0.600 mm [No.1	6 x No.30] and Milling	
Mass of 1.18x0.600mm (No.16x30) dedusted sample placed into HGI bowl, (G) :	g	Number of revolutions, (I):	
No. of increments collected, (H):	PRAVI	Seconds to mill, (J):	sec
Start position:		RPM, [I/(J/60)]:	RPM
Stop position :	-		
Start time :			
A STM Stop time:	40014.09		
tenderde itali evlastela a/standerde/sixt/ha 7/1115 li eve	10 05 151 150 55 05	000347d17045/astm_d/00	d/100m 1
Tare mass of catch pan, (L):	IG OF MILLED PROD	Mass of -75µm (-No.200), (N -L), (P) :	-u-tuziii-l
Tare mass of Catch pan, (L): Tare mass of 75µm (No.200) sieve, (M):	g	Mass of +75μm (+No.200), (N -L), (P) : Mass of +75μm (+No.200), (O - M), (Q) :	9
Mass of catch pan and -75μm (-No.200), (N) :	g		9
	g	Total recover, (P + Q), (R):	
Mass of 75µm (No.200) sieve and +75µm (+No.200), (O) : Calculated mass of -75µm (-No.200), (G - Q), (T) :	g	Loss (≤0.50g), (G - R), (S):	
Calculated mass of -7 Spirit (-10.200), (6 - 4), (1) :	g		
	ALYTICAL RESULT	S	
HGI Formula (from Least Squares Regression):			
HGI (U) :			
% moisture on 1.18x0.600mm (No.16x30) material :	%	See the ANNEX, Method for Determining the Moistu	
(a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c		Content of the 1.18x0.600mm (No.16x30) Test Samp	ole

FIG. 3 HGI Log Sheet is for Example Only and is Non-Mandatory

$$Y = \frac{W_2}{W_1} \times 100 \tag{1}$$

where:

Y = % Yield,

 W_1 = mass of air dried sample (6.2), and

 $W_2 = \text{mass of } 1.18\text{-mm by } 600\text{-}\mu\text{m} \text{ (No. } 16 \text{ by No. } 30)$

material (6.4).

8.4 If other than primary HGI RMs are used for calibration of the test apparatus and method, report the source of the calibration standards used.

8.5 An example of a typical HGI preparation log sheet that has found application for record keeping during preparation of samples to be used for HGI determination is shown in Fig. 3.

9. Precision and Bias

9.1 Precision:

9.1.1 The precision of this test method for the determination of Hardgrove Grindability Index of Coal, whenever international (primary) HGI reference materials are used for calibration, is shown in Table 2.