

Designation: D4485 - 09

# Standard Specification for Performance of Engine Oils<sup>1</sup>

This standard is issued under the fixed designation D4485; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon  $(\varepsilon)$  indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense.

#### INTRODUCTION

This specification covers all the currently active American Petroleum Institute (API) engine oil performance categories that have been defined in accordance with the ASTM consensus process. There are organizations with specifications not subject to the ASTM consensus process, such as the International Lubricant Standardization and Approval Committee (ILSAC), American Petroleum Institute (API – SM Specification), and the Association des Constructeurs Europeans d'Automobiles (ACEA). Certain of these specifications, which have been defined primarily by the use of current ASTM test methods, have also been included in the Appendix of this document for information.

In the ASTM system, a specific API designation is assigned to each category. The system is open-ended, that is, new designations are assigned for use with new categories as each new set of oil performance characteristics are defined. Oil categories may be referenced by engine builders in making lubricant recommendations, and used by lubricant suppliers and customers in identifying products for specific applications. Where applicable, candidate oil programs are conducted in accordance with the American Chemistry Council (ACC) Petroleum Additives Product Approval Code of Practice.

Other service categories not shown in this document have historically been used to describe engine oil performance (SA, SB, SC, SD, SE, SF, SG and CA, CB, CC, CD, CD-II, CE) (see 3.1.2). SA is not included because it does not have specified engine performance requirements. SG is not included because it was a category that could not be licensed for use in the API Service Symbol after Dec. 31, 1995. The others are not included because they are based on test methods for which engine parts, test fuel, or reference oils, or a combination thereof, are no longer available. Also, the ASTM 5-Car and Sequence VI Procedures are obsolete and have been deleted from the category Energy Conserving and Energy Conserving II (defined by Sequence VI). Information on excluded older categories and obsolete test requirements can be found in SAE J183.

#### 1. Scope

- 1.1 This specification covers engine oils for light-duty and heavy-duty internal combustion engines used under a variety of operating conditions in automobiles, trucks, vans, buses, and off-highway farm, industrial, and construction equipment.
- 1.2 This specification is not intended to cover engine oil applications such as outboard motors, snowmobiles, lawn mowers, motorcycles, railroad locomotives, or oceangoing vessels.

- 1.3 This specification is based on engine test results that generally have been correlated with results obtained on reference oils in actual service engines operating with gasoline or diesel fuel. As it pertains to the API SL engine oil category, it is based on engine test results that generally have been correlated with results obtained on reference oils run in gasoline engine Sequence Tests that defined engine oil categories prior to 2000. It should be recognized that not all aspects of engine oil performance are evaluated by the engine tests in this specification. In addition, when assessing oil performance, it is desirable that the oil be evaluated under actual operating conditions.
- 1.4 This specification includes bench and chemical tests that help evaluate some aspects of engine oil performance not covered by the engine tests in this specification.

<sup>&</sup>lt;sup>1</sup> This specification is under the jurisdiction of ASTM Committee D02 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.B0 on Automotive Lubricants.

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**TABLE 1 Test Procedures** 

Test Procedure	ASTM Publications <sup>A</sup>
T-6	D02-1219 <sup>B</sup>
T-7	D02-1220 <sup>C</sup>
ISM	under development <sup>D</sup>
ISB	under development <sup>E</sup>
C13	under development <sup>F</sup>

 $<sup>^{\</sup>it A}$  Research Reports are available from ASTM International Headquarters. Request by Research Report No.

- 1.5 The test procedures referred to in this specification that are not yet standards are listed in Table 1.
- 1.6 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.
- 1.6.1 *Exceptions*—The roller follower shaft wear in Test Method D5966 is in mils. Appendix X2 descriptions are verbatim API language, which contains a few non-SI units.

#### 2. Referenced Documents

- 2.1 ASTM Standards:<sup>2</sup>
- D92 Test Method for Flash and Fire Points by Cleveland Open Cup Tester
- D93 Test Methods for Flash Point by Pensky-Martens Closed Cup Tester
- D130 Test Method for Corrosiveness to Copper from Petroleum Products by Copper Strip Test
- D874 Test Method for Sulfated Ash from Lubricating Oils and Additives
- D892 Test Method for Foaming Characteristics of Lubricating Oils
- D2622 Test Method for Sulfur in Petroleum Products by Wavelength Dispersive X-ray Fluorescence Spectrometry
- D2887 Test Method for Boiling Range Distribution of Petroleum Fractions by Gas Chromatography
- D3244 Practice for Utilization of Test Data to Determine Conformance with Specifications
- D4171 Specification for Fuel System Icing Inhibitors
- D4683 Test Method for Measuring Viscosity of New and Used Engine Oils at High Shear Rate and High Temperature by Tapered Bearing Simulator Viscometer at 150 °C
- D4684 Test Method for Determination of Yield Stress and Apparent Viscosity of Engine Oils at Low Temperature
- D4951 Test Method for Determination of Additive Elements in Lubricating Oils by Inductively Coupled Plasma Atomic Emission Spectrometry

- D5119 Test Method for Evaluation of Automotive Engine
  Oils in the CRC L-38 Spark-Ignition Engine<sup>3</sup>
- D5133 Test Method for Low Temperature, Low Shear Rate, Viscosity/Temperature Dependence of Lubricating Oils Using a Temperature-Scanning Technique
- D5185 Test Method for Determination of Additive Elements, Wear Metals, and Contaminants in Used Lubricating Oils and Determination of Selected Elements in Base Oils by Inductively Coupled Plasma Atomic Emission Spectrometry (ICP-AES)
- D5290 Test Method for Measurement of Oil Consumption, Piston Deposits, and Wear in a Heavy-Duty High-Speed Diesel Engine—NTC-400 Procedure<sup>3</sup>
- D5293 Test Method for Apparent Viscosity of Engine Oils and Base Stocks Between -5 and -35°C Using Cold-Cranking Simulator
- D5302 Test Method for Evaluation of Automotive Engine
  Oils for Inhibition of Deposit Formation and Wear in a
  Spark-Ignition Internal Combustion Engine Fueled with
  Gasoline and Operated Under Low-Temperature, LightDuty Conditions<sup>3</sup>
- D5480 Test Method for Engine Oil Volatility by Gas Chromatography<sup>3</sup>
- D5481 Test Method for Measuring Apparent Viscosity at High-Temperature and High-Shear Rate by Multicell Capillary Viscometer
- D5533 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIE, Spark-Ignition Engine<sup>3</sup>
- D5800 Test Method for Evaporation Loss of Lubricating Oils by the Noack Method
- D5844 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Rusting (Sequence IID)<sup>3</sup>
- D5862 Test Method for Evaluation of Engine Oils in Two-Stroke Cycle Turbo-Supercharged 6V92TA Diesel Engine<sup>3</sup>
- D5966 Test Method for Evaluation of Engine Oils for Roller Follower Wear in Light-Duty Diesel Engine
- D5967 Test Method for Evaluation of Diesel Engine Oils in T-8 Diesel Engine
- D5968 Test Method for Evaluation of Corrosiveness of Diesel Engine Oil at 121°C
- D6082 Test Method for High Temperature Foaming Characteristics of Lubricating Oils
- D6202 Test Method for Automotive Engine Oils on the Fuel Economy of Passenger Cars and Light-Duty Trucks in the Sequence VIA Spark Ignition Engine<sup>3</sup>
- D6278 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus
- D6335 Test Method for Determination of High Temperature Deposits by Thermo-Oxidation Engine Oil Simulation Test
- D6417 Test Method for Estimation of Engine Oil Volatility by Capillary Gas Chromatography
- D6483 Test Method for Evaluation of Diesel Engine Oils in T-9 Diesel Engine<sup>3</sup>
- D6557 Test Method for Evaluation of Rust Preventive

Multicylinder Engine Test Procedure for the Evaluation of Lubricants-Mack T-6.
 Multicylinder Engine Test Procedure for the Evaluation of Lubricants-Mack

 $<sup>^{</sup>D}$  Multicylinder Engine Test Procedure for the Evaluation of Lubricants-Cummins ISM.

 $<sup>^{\</sup>it E}$  Multicylinder Engine Test Procedure for the Evaluation of Lubricants-Cummins ISB.

 $<sup>^{\</sup>it F}$  Multicylinder Engine Test Procedure for the Evaluation of Lubricants-Caterpillar C13.

<sup>&</sup>lt;sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>&</sup>lt;sup>3</sup> Withdrawn. The last approved version of this historical standard is referenced on www.astm.org.

Characteristics of Automotive Engine Oils

D6593 Test Method for Evaluation of Automotive Engine
Oils for Inhibition of Deposit Formation in a SparkIgnition Internal Combustion Engine Fueled with Gasoline
and Operated Under Low-Temperature, Light-Duty Conditions

D6594 Test Method for Evaluation of Corrosiveness of Diesel Engine Oil at 135°C

D6618 Test Method for Evaluation of Engine Oils in Diesel Four-Stroke Cycle Supercharged 1M-PC Single Cylinder Oil Test Engine

D6681 Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel Engine—Caterpillar 1P Test Procedure

D6709 Test Method for Evaluation of Automotive Engine Oils in the Sequence VIII Spark-Ignition Engine (CLR Oil Test Engine)

D6750 Test Methods for Evaluation of Engine Oils in a High-Speed, Single-Cylinder Diesel Engine—1K Procedure (0.4 % Fuel Sulfur) and 1N Procedure (0.04 % Fuel Sulfur)

D6794 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Various Amounts of Water and a Long (6-h) Heating Time

D6795 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Water and Dry Ice and a Short (30-min) Heating Time

D6837 Test Method for Measurement of Effects of Automotive Engine Oils on Fuel Economy of Passenger Cars and Light-Duty Trucks in Sequence VIB Spark Ignition Engine

D6838 Test Method for Cummins M11 High Soot Test

D6891 Test Method for Evaluation of Automotive Engine
Oils in the Sequence IVA Spark-Ignition Engine

D6894 Test Method for Evaluation of Aeration Resistance of Engine Oils in Direct-Injected Turbocharged Automotive Diesel Engine

D6896 Test Method for Determination of Yield Stress and Apparent Viscosity of Used Engine Oils at Low Temperature

D6922 Test Method for Determination of Homogeneity and Miscibility in Automotive Engine Oils

D6923 Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel Engine—Caterpillar 1R Test Procedure

D6975 Test Method for Cummins M11 EGR Test

D6984 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIF, Spark-Ignition Engine

D6987/D6987M Test Method for Evaluation of Diesel Engine Oils in T-10 Exhaust Gas Recirculation Diesel Engine

D7097 Test Method for Determination of Moderately High Temperature Piston Deposits by Thermo-Oxidation Engine Oil Simulation Test—TEOST MHT

D7109 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus at 30 and 90 Cycles

D7156 Test Method for Evaluation of Diesel Engine Oils in the T-11 Exhaust Gas Recirculation Diesel Engine

D7216 Test Method for Determining Automotive Engine
Oil Compatibility with Typical Seal Elastomers

D7320 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIG, Spark-Ignition Engine

D7422 Test Method for Evaluation of Diesel Engine Oils in T-12 Exhaust Gas Recirculation Diesel Engine

E29 Practice for Using Significant Digits in Test Data to Determine Conformance with Specifications

E178 Practice for Dealing With Outlying Observations

2.2 Society of Automotive Engineers Standards:<sup>4</sup>

SAE J183 Engine Oil Performance and Engine Service Classification

SAE J300 Engine Oil Classification

SAE J1423 Passenger Car and Light-Duty Truck Energy-Conserving Engine Oil Classification

SAE J2643 Standard Reference Elastomers (SRE) for Characterizing the Effects on Vulcanized Rubber

2.3 American Petroleum Institute Publication:<sup>5</sup>

API 1509 Engine Oil Licensing and Certification System (EOLCS)

2.4 Government Standard:<sup>6</sup>

DOD CID A-A-52039A (SAE 5W-30, 10W-30, and 15W-40)

2.5 American Chemical Council Code:<sup>7</sup>

ACC Petroleum Additives Product Approval Code of Practice

#### 3. Terminology

- 3.1 Definitions:
- 3.1.1 *automotive*, *adj*—descriptive of equipment associated with self-propelled machinery, usually vehicles driven by internal combustion engines.
- 3.1.2 category, n—in engine oils, a designation such as SH, SJ, SL, SM, CF-4, CF, CF-2, CG-4, CH-4, CI-4, CJ-4, Energy Conserving, and so forth, for a given level of performance in specified engine and bench tests.
- 3.1.3 classification, n—in engine oils, the systematic arrangement into categories in accordance with different levels of performance in specified engine and bench tests.
- 3.1.4 *engine oil*, *n*—a liquid that reduces friction and wear between the moving parts within an engine, and also serves as a coolant.
- 3.1.4.1 *Discussion*—It can contain additives to enhance certain properties. Inhibition of engine rusting, deposit formation, valve train wear, oil oxidation, and foaming are examples.
- 3.1.5 heavy duty, adj—in internal combustion engine operation, characterized by average speeds, power output, and internal temperatures that are generally close to the potential maximums.

<sup>&</sup>lt;sup>4</sup> Available from Society of Automotive Engineers (SAE), 400 Commonwealth Dr., Warrendale, PA 15096–0001.

<sup>&</sup>lt;sup>5</sup> Available from American Petroleum Institute (API), 1220 L. St., NW, Washington, DC 20005-4070, http://www.api.org.

<sup>&</sup>lt;sup>6</sup> Available from U.S. Government Printing Office Superintendent of Documents, 732 N. Capitol St., NW, Mail Stop: SDE, Washington, DC 20401.

<sup>&</sup>lt;sup>7</sup> Available from American Chemical Council, 1300 Wilson Blvd., Arlington, VA 22209.

- 3.1.6 *heavy-duty engine*, *n*—*in internal combustion engine types*, one that is designed to allow operation continuous at or close to its peak output.
- 3.1.6.1 *Discussion*—This type of engine is typically installed in large trucks and buses as well as farm, industrial, and construction equipment.
- 3.1.7 *light-duty*, *adj—in internal combustion engine operation*, characterized by average speeds, power output, and internal temperatures that are generally much lower than the potential maximums.
- 3.1.8 *light-duty engine*, *n*—*in internal combustion engine types*, one that is designed to be normally operated at substantially less than its peak output.
- 3.1.8.1 *Discussion*—This type of engine is typically installed in automobiles and small trucks, vans, and buses.
- 3.1.9 *lugging*, *adj—in internal combustion engine operation*, characterized by a combined mode of relatively lowspeed and high-power output.
  - 3.2 Definitions of Terms Specific to This Standard:
- 3.2.1 *C category*, *n*—the group of engine oils that are intended primarily for use in diesel and certain gasoline-powered vehicles.
- 3.2.2 Energy Conserving category, n—the group of engine oils that have demonstrated fuel economy benefits and are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.
- 3.2.3 *S category*, *n*—the group of engine oils that are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.

#### 4. Performance Classification

- 4.1 Automotive engine oils are classified in three general arrangements, as defined in 3.2; that is, S, C, and Energy Conserving. These arrangements are further divided into categories with performance measured as follows:
- 4.1.1 *SH*—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.1.1 Test Method D5844, the Sequence IID gasoline engine test, has been correlated with vehicles used in short-trip service prior to 1978,<sup>4.8</sup> particularly with regard to rusting. (An alternative is Test Method D6557, the Ball Rust Test.)
- 4.1.1.2 Test Method D5533, the Sequence IIIE gasoline engine test, has been correlated with vehicles used in high-temperature service prior to 1988, particularly with regard to oil thickening and valve train wear. (Alternatives are Test Method D6984, the Sequence IIIF test, or Test Method D7320, the Sequence IIIG test.)
- 4.1.1.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stopand-go service prior to 1988, 10 particularly with regard to
- <sup>8</sup> Available from ASTM International in STP 3151 (Part 1). Also available from the Society of Automotive Engineers as Technical Paper No. 780931.
- <sup>9</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1225.
- <sup>10</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1226.

- sludge and valve train wear. (An alternative is the combination of Test Method D6593, the Sequence VG test, and Test Method D6891, the Sequence IVA test.)
- 4.1.1.4 Test Method D5119, the L-38 gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions. (An alternative is Test Method D6709, the Sequence VIII test.)
- (1) Test Method D5119 (or Test Method D6709) is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.1.5 In addition to passing performance in the engine tests, specific viscosity grades shall also meet bench test requirements (see Table 2), which are discussed in the following subsections:
- (1) The volatility of engine oils relates to engine oil consumption.
- (2) Test Method D6795, the Engine Oil Filterability Test (EOFT) screens for the formation of precipitates that can cause oil filter plugging.
- (3) Phosphorus compounds can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency.
- (4) The flash point can indicate if residual solvents and low-boiling fractions remain in the finished oil.
- (5) Foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
- (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- 4.1.1.6 Licensing of the API SH category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification. (See Appendix X3 for more information.)
- 4.1.2 *SJ*—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.2.1 Test Method D5844, the Sequence IID, gasoline engine test has been correlated with vehicles used in short-trip service prior to 1978, particularly with regard to rusting. (An alternative is Test Method D6557, the Ball Rust Test.)
- 4.1.2.2 Test Method D5533, the Sequence IIIE gasoline engine test, has been correlated with vehicles used in high-temperature service prior to 1988, particularly with regard to oil thickening and valve train wear. (Alternatives are Test Method D6984, the Sequence IIIF test, or Test Method D7320, the Sequence IIIG test.)
- 4.1.2.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stop-and-go service prior to 1988, particularly with regard to sludge and valve train wear. (An alternative is the combination of Test Method D6593, the Sequence VG test, and Test Method D6891, the Sequence IVA test.)



## TABLE 2 S Engine Oil Categories

	API SI	H Category			
Engine Test Method	Rated or Me	asured Parameter	Primary Pe	erformance Criteria	
D5844 <sup>A,B</sup> (Sequence IID)	Average engine rust r			8.5	
- A :-	Number stuck lifters			none	
or D6557 <sup>A</sup> (Ball Rust Test)	Average gray value, n			100	
D5533 <sup>B,D</sup> (Sequence IIIE)	Hours to 375 % kinem	-		64	
	increase at 40 °C, mir				
	Average engine sludg			9.2	
	Average piston skirt v			8.9	
	Average oil ring land	deposit rating," min		3.5	
	Lifter sticking			none	
	Scuffing and wear Cam or lifter scuffin	_			
	Cam plus lifter wea			none	
	Average, max	ι, μπι		30	
	Maximum, max			64	
	Ring sticking (oil-relate	ed <sup>G</sup> )		none	
or D6984 (Sequence IIIF)D		increase at 40 °C, max		325 <sup>H</sup>	
(	Average piston skirt v			8.5 <sup>'</sup>	
	Weighted piston depo			3.2 <sup>1</sup>	
		m-plus-lifter wear, µm, max		20 <sup>I,K</sup>	
	Hot stuck rings			none <sup>1</sup>	
or D7320 (Sequence IIIG) <sup>L</sup>		increase at 40 °C, max		150	
	Weighted piston depo			3.5	
	Cam-plus-lifter wear a	ιvg, μm, max		60	
	Hot stuck rings	_		none	
D5302 <sup>B,N</sup> (Sequence VE)	Average engine sludg			9.0	
	Rocker arm cover slue			7.0	
	Average piston skirt v			6.5	
		Average engine varnish rating, min		5.0	
		Oil ring clogging, %		report	
	Oil screen clogging, %			20.0	
	Compression ring stic	king (not stuck)		none	
	Cam wear, µm Average, max			127	
	Maximum, max			380	
or D6891 (Sequence IVA) <sup>N</sup>	Average cam wear, µr	m <sup>O</sup>		120	
plus, D6593 <sup>N</sup> (Sequence VG)		Average engine sludge rating, <sup>E</sup> min		7.8	
p.a.c, _ (0.14a)	Rocker arm cover sluc			8.0	
	Average piston skirt v			7.5	
	Average engine varnis	sh rating, P min		8.9	
	Oil screen clogging, %	, max		20	
	Hot stuck compression			none	
D5119 <sup>a</sup> (L-38), iteh ai/catalog/sta	Bearing weight loss, r	$max_{0}-4626-8e72$		m404485-09	
or D6709 <sup>Q</sup> (Sequence VIII)	Shear stability Bearing weight loss, r	ng may		26.4	
or Devos " (Sequence viii)	Shear stability	ny, max		20.4 R	
Bench Test and Measured Parameter (eff-	ective January 1, 1992)		osity Grade Performance Crit	eria <sup>s</sup>	
(OII		SAE 5W-30	SAE 10W-30	SAE 15W-40	
Test Method D5800 volatility loss, % max	T	25	20	18	
Test Method D2887 volatility loss at 371 $^{\circ}$	,	20	17	15	
Test Method D6795 (EOFT), % flow reduce		50	50	$NR^{\mathcal{U}}$	
Test Method D4951 or D5185, mass fracti		0.12	0.12	NR	
Test Method D4951 or D5185, mass fracti	ion phosphorus %, min	0.06	0.06	0.06	
(all viscosity grades)					
(unless valid passing Test Method D530	results are obtained)	000	00-	0.1=	
Test Method D92 flash point, °C, min <sup>V</sup>		200	205	215	
Test Method D93 flash point, °C, min <sup>V</sup>	ian A)	185	190	200	
Test Method D892 foaming tendency (Opt	uon A)	10/0	10/0	10/0	
Sequence I, max, foaming/settling <sup>W</sup>		10/0	10/0	10/0	
Sequence II, max, foaming/settling <sup>W</sup> Sequence III, max, foaming/settling <sup>W</sup>		50/0 10/0	50/0 10/0	50/0 10/0	
Test Method D6082 (optional blending red	uired)	10/0 report <sup>X</sup>	10/0 report <sup>X</sup>	10/0 report <sup>x</sup>	
Test Method D6922 homogeneity and mis		Y	report	report	
	API S	J Category			
Engine Test Method	Rated or Meas	sured Parameter	Primary F	Performance Criteria	
		· · —			

Average gray value, min Hours to 375 % kinematic viscosity increase at 40  $^{\circ}\text{C},$  min

8.5 none

100 64

Average engine rust rating,  $^{C}$  min Number stuck lifters

D5844<sup>A,B</sup> (Sequence IID)

or D6557<sup>A</sup> (Ball Rust Test) D5533<sup>B,D</sup> (Sequence IIIE)



#### TABLE 2 Continued

91	Category

Engine Test Method	Rated or Measured Parameter	Primary Performance Criteria
	Average engine sludge rating, <sup>E</sup> min	9.2
	Average piston skirt varnish rating, F min	8.9
	Average oil ring land deposit rating, min	3.5
	Lifter sticking	none
	Scuffing and wear	
	Cam or lifter scuffing	none
	Cam plus lifter wear, µm	
	Average, max	30
	Maximum, max	64
	Ring sticking (oil-related) <sup>G</sup>	none
or D6984 (Sequence	Kinematic viscosity, % increase at 40 °C, max	325 <sup>H</sup>
IIIF) <sup>D</sup>		
	Average piston skirt varnish rating, min	8.5 <sup>'</sup>
	Weighted piston deposit rating, min	3.2 <sup>1</sup>
	Screened average cam-plus-lifter wear, µm, max	20 <sup>/,K</sup>
	Hot stuck rings	none <sup>/</sup>
or D7320 (Sequence IIIG) <sup>L</sup>	Kinematic viscosity, % increase at 40 °C, max	150
•	Weighted piston deposit rating, mmin	3.5
	Cam-plus-lifter wear avg, µm, max	60
	Hot stuck rings	none
D5302 <sup>B,N</sup> (Sequence VE)	Average engine sludge rating, <sup>E</sup> min	9.0
,	Rocker arm cover sludge rating, <sup>E</sup> min	7.0
	Average piston skirt varnish rating, F min	6.5
	Average engine varnish rating, min	5.0
	Oil ring clogging, %	report
	Oil screen clogging, %, max	20.0
	Compression ring sticking (hot stuck)	none
	Cam wear, µm	
	Average, max	127
	Maximum, max	380
or D6891 (Sequence	Average cam wear, µm <sup>O</sup>	120
IVA) <sup>N</sup>	ttng. //standards itch ai)	0
plus, D6593 <sup>N</sup>	Average engine sludge rating, <sup>E</sup> min	7.8
(Sequence VG)	Rocker arm cover sludge rating, F min	8.0
(3343530 + 3)	Average piston skirt varnish rating, F min	7.5
	Average engine varnish rating, min	8.9
	Oil screen clogging, %, max	20
	Hot stuck compression rings	none
D5119 <sup>Q</sup> (L-38)	Bearing weight loss, mg, max	40
DOTTO (L-30)	Shear stability	40 R
or D6709 <sup>Q</sup> (Sequence	Bearing weight loss, mg, max	26.4
VIII)	og/standards/SISV/C8aa/92-1006-4626-8e72-0c4cdd6	59496/astm-d4485-09
v,	Shear stability	R

	Viscosity Grade Per	ormance Criteria	
Bench Test and Measured Parameter	SAE 0W-20, SAE 5W-20, SAE 5W-30, SAE 10W-30	All Others	
Test Method D5800 volatility loss, % max <sup>Z</sup>	22	20 <sup>AA</sup>	
Test Method D6417 volatility loss at 371 °C, % max <sup>Z</sup>	17	15 <sup>AA</sup>	
Test Method D5480 volatility loss at 371 °C, % max <sup>Z</sup>	17	15 <sup>AA</sup>	
Test Method D6795 (EOFT), % flow reduction, max	50	50	
Test Method D6794 (EOWTT), % flow reduction, max			
with 0.6 % H <sub>2</sub> 0	report	report	
with 1.0 % H <sub>2</sub> 0	report	report	
with 2.0 % H <sub>2</sub> 0	report	report	
with 3.0 % H <sub>2</sub> 0	report	report	
Test Method D4951 or D5185, mass fraction phosphorus, %, max	0.10 <sup>AB</sup>	$NR^{\mathit{U}}$	
Test Method D4951 or D5185, mass fraction phosphorus, %, min (unless valid passing Test Method D5302 results are obtained)	0.06	0.06	
Test Method D92 flash point, °C, min <sup>V</sup>	200	$NR^{\mathit{U}}$	
Test Method D93 flash point, °C, min <sup>V</sup>	185	$NR^{\mathit{U}}$	
Test Method D892 foaming tendency (Option A)			
Sequence I, max, foaming/settling <sup>AC</sup>	10/0	10/0	
Sequence II, max, foaming/settling <sup>AC</sup>	50/0	50/0	
Sequence III, max, foaming/settling <sup>AC</sup>	10/0	10/0	
Test Method D6082 (optional blending required) Static foam, max, tendency/stability	200/50 <sup>AD</sup>	200/50 <sup>AD</sup>	
Test Method D6922 homogeneity and miscibility	Y	Y	

#### TABLE 2 Continued

	Viscosity Grade Performance Criteria		
Bench Test and Measured Parameter	SAE 0W-20, SAE 5W-20, SAE 5W-30, SAE 10W-30	All Others	
Test Method D6335 High temperature deposits (TEOST 33), deposit wt, mg, max	60	60	
Test Method D5133 Gelation Index, max	12	$NR^{\mathcal{U}}$	

#### APLSI Category

Engine Test Method	Rated or Measured Parameter	Primary Performance Criteria
D6984 (Sequence IIIF)	Kinematic viscosity, % increase at 40 °C, max	275
	Average piston skirt varnish rating, min	9.0
	Weighted piston deposit rating, min	4.0
	Screened average cam-plus-lifter wear, µm, max	20 <sup>K</sup>
	Hot Stuck Rings	none
	Low temperature viscosity performance <sup>AE</sup>	report
or D7320 (Sequence IIIG) <sup>L</sup>	Kinematic viscosity, % increase at 40 °C, max	150
	Weighted piston deposit rating, <sup>M</sup> min	3.5
	Cam-plus-lifter wear avg, µm, max	60
	Hot stuck rings	none
	Low temperature viscosity performance <sup>AF</sup>	report
D6891 (Sequence IVA)	Cam wear average, $\mu$ m, $^{\mathcal{O}}$ max	120
D5302 <sup>B</sup>	Cam wear average, µm, max	127
(Sequence VE <sup>AG</sup> ) D6593	Cam wear max, µm, max	380
(Sequence VG)	Average engine sludge rating, E min	7.8
	Rocker arm cover sludge rating, <sup>E</sup> min	8.0
	Average piston skirt varnish rating, min	7.5
	Average engine varnish rating, min	8.9
	Oil screen clogging, %, max	20
	Hot stuck Compression rings	none
	Cold stuck rings	report
	Oil screen debris, %	report
	Oil ring clogging, %	report
D6709	Bearing weight loss, mg, max	26.4
(Sequence VIII)	Shear stability	R

Bench Test and Measured Parameter	Performance Criteria
Test Method D6557 (Ball Rust Test), average gray value, min	100
Test Method D5800 volatility loss, % max ASTM D4485-09	15
Test Method D6417 volatility loss at 371 °C, % max D6795 (EOFT), % flow reduction, max	2-0c4cdd659496/a <sub>50</sub> m-d4485-09
D6794 (EOWTT), % flow reduction, max	
With 0.6 % H <sub>2</sub> O	50
With 1.0 % H <sub>2</sub> O	50
With 2.0 % H <sub>2</sub> O	50
With 3.0 % H₂O	50
Test Method D4951 or D5185, mass fraction phosphorus %, max <sup>AH</sup>	0.10 <sup>AB</sup>
Test Method D4951 or D5185, mass fraction phosphorus %, min	0.06
(unless valid passing Test Method D5302 results are obtained)	
Test Method D892 foaming tendency (Option A)	
Sequence I, max, foaming/settling <sup>AC</sup>	10/0
Sequence II, max, foaming/settling <sup>AC</sup>	50/0
Sequence III, max, foaming/settling <sup>AC</sup>	10/0
Test Method D6082 (optional blending required) static foam max, tendency/stability	100/0 <sup>AD</sup>
Test Method D6922 homogeneity and miscibility	Y
Test Method D7097 high temperature deposits (TEOST MHT-4),	
deposit wt, mg, max	45
Test Method D5133 (Gelation Index), max <sup>AH</sup>	12 <sup>AI</sup>

<sup>&</sup>lt;sup>A</sup> Demonstrate passing performance in either Test Method D5844 or D6557.

<sup>&</sup>lt;sup>B</sup> Monitoring of this test method was discontinued in June 20, 2001. Valid test results shall predate the end of the last calibration period for the test stand in which this test method was conducted.

<sup>&</sup>lt;sup>C</sup> CRC Rust Rating Manual No. 7, available from Coordinating Research Council, 219 Perimeter Center Pkwy., Atlanta, GA 30346.

Demonstrate passing performance in either Test Method D5533 or D6984. However, an oil passing Test Method D6984 and containing less than 0.08 % mass phosphorus in the form of ZDDP shall also pass the wear limits in Test Method D5302 (see also footnote <sup>L</sup>).

ECRC Sludge Rating Manual No. 12, available from Coordinating Research Council, 219 Perimeter Center Pkwy., Atlanta, GA 30346.

FCRC Varnish Rating Manual No. 14, available from Coordinating Research Council, 219 Perimeter Center Pkwy., Atlanta, GA 30346.

<sup>&</sup>lt;sup>G</sup> An oil-related stuck ring occurs on a piston with an individual oil ring land deposit rating <2.6.

 $<sup>^{\</sup>it H}$  Determine at 60 h.

Determine at 80 h.



- <sup>J</sup> Determine weighted piston deposits by rating the following piston areas and applying the corresponding weightings: undercrown, 10 %; second land, 15 %; third land, 30 %; piston skirt, 10 %; first groove, 5 %; second groove, 10 %; and third groove, 20 %. Use CRC Varnish Rating Manual No. 14 for all ratings.
- K Calculate by eliminating the highest and lowest cam-plus-lifter wear results and then calculating an average based on the remaining ten rating positions.
- <sup>L</sup> For oils containing at least 0.06 % mass phosphorus in the form of ZDDP, demonstrating passing performance in the Sequence IIIG test obviates the need to also conduct Test Method D5302 (Sequence VE), which was previously required for oils with less than 0.08 % mass phosphorus.
  - <sup>M</sup> Unlike the Sequence IIIF test, piston skirt varnish rating is not required in the Sequence IIIG test.
- <sup>M</sup> Demonstrate passing performance in Test Method D5302, or alternatively, in both Test Method D6891 and Test Method D6593.
- O Determine cam wear according to Test Method D6891. Seven wear measurements are made on each cam lobe and the seven measured values are added to obtain an individual cam lobe wear result. The overall cam wear value is the average of the twelve individual cam lobe wear results.
- P Determine the average engine varnish rating by averaging the piston skirt, right rocker arm cover, and left rocker arm cover varnish ratings. Use the CRC Varnish Rating Manual No. 14 for all ratings.
  - <sup>Q</sup> Demonstrate passing performance in either Test Method D5119 or D6709.
  - R Ten-hour stripped kinematic viscosity (oil shall remain in original viscosity grade).
  - S Passing bench test performance is only required for SAE 5W-30, SAE 10W-30, and SAE 15W-40 viscosity grades as defined in SAE J300.
  - <sup>7</sup> Meet either Test Method D5800 or Test Method D2887 volatility requirement.
  - $^{\prime\prime}$  NR stands for Not Required.
  - <sup>V</sup> Meet either Test Method D92 or Test Method D93 flash point requirement.
  - <sup>W</sup> Determine settling volume at 5 min.
  - $^{X}$  Report kinetic foam volume (mL), static foam volume (mL), and collapse time, s.
  - Y Homogeneous with SAE reference oils.
  - <sup>Z</sup> Meet the volatility requirement in either Test Method D5800, D5480, or D6417.
  - AA Passing volatility loss only required for SAE 15W-40 oils.
  - AB This is a noncritical specification as described in Practice D3244.
  - AC Determine settling volume, in mL, at 10 min.
  - AD Determine settling volume, in mL, at 1 min.
- AE Evaluate the 80-h test oil sample by Test Method D4684 at the temperature indicated by the low temperature grade of oil as determined on the 80-h sample by Test Method D5293.
- AF Measure the viscosity of the EOT oil sample by Test Method D4684. The measured viscosity shall meet the requirements of the original grade or the next higher grade. The EOT sample can be either from a Sequence IIIG or a Sequence IIIGA test. (A Sequence IIIGA test is identical to a Sequence IIIG test, except only low temperature viscosity performance is measured.) Additional details are provided in the Sequence IIIG test method, in Section 13.6.
  - AG Not required for oils containing a minimum of 0.08 % mass phosphorus in the form of ZDDP.
  - AH Requirement applies only to SAE 0W-20, 5W-20, 0W-30, 5W-30, and 10W-30 viscosity grades.
  - <sup>AI</sup> For gelation temperatures at or above the W grade pumpability temperature as defined in SAE J300.

# iTeh Standards

- 4.1.2.4 Test Method D5119, the L-38 gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions. (An alternative is Test Method D6709, the Sequence VIII test.)
- (1) Test Method D5119 (or Test Method D6709) is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.2.5 In addition to passing performance in the engine tests, specific viscosity grades shall also meet bench test requirements (see Table 2), which are discussed in the following subsections:
- (1) The volatility of engine oils is one of several factors that relates to engine oil consumption.
- (2) Test Method D6795, the EOFT screens for the formation of precipitates and gels that form in the presence of water and can cause oil filter plugging.
- (3) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency.
- (4) The flash point may indicate if residual solvents and low-boiling fractions remain in the finished oil.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
- (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test

- Method D6335, the TEOST test, may be useful in determining the deposit control of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low temperature protection not adequately measured by the Test Method D4684.
- 4.1.2.6 Licensing of the API SJ category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.3 *SL*—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.3.1 Test Method D6984, the Sequence IIIF gasoline engine test, is used to measure oil thickening and piston deposits under high temperature conditions and provides information about valve train wear.<sup>11</sup> (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.3.2 Test Method D6891, the Sequence IVA gasoline engine test, has been correlated with the Sequence VE gasoline engine test in terms of overhead cam and slider follower wear control.<sup>12</sup>
- 4.1.3.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stopand-go service prior to 1988, with regard to valve train wear. It

<sup>&</sup>lt;sup>11</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1391.

<sup>&</sup>lt;sup>12</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1473.

is included in the SL performance specification to augment assessment of the wear control performance of oils containing less than 0.08 % mass of phosphorus from ZDDP additive.

Note 1-Prior to May 2004, the API SH, SJ, and SL categories required that oils with passing Test Method D6984 (Sequence IIIF) results, and containing less than 0.08 % mass phosphorus in the form of ZDDP, also demonstrate passing performance in Test Method D5302 (Sequence VE). This requirement was included to address concerns over adequate wear protection with low levels of ZDDP. However, Test Method D5302 has not been available to industry for some time, and an alternative method was needed. In a related activity, the next level of gasoline engine oil performance, the ILSAC GF-4 standard, was developed outside the normal ASTM consensus process. Deliberations during the GF-4 development process included careful consideration of the suitability of Test Method D7320, the Sequence IIIG, a new test, to evaluate the wear protection of oils with less than 0.08 % mass phosphorus. Data on oils with less than 0.08 % mass phosphorus in the form of ZDDP were reviewed by members of the D02.B0 Passenger Car Engine Oil Classification Panel (PCEOCP). These data were from Test Method D7320 (Sequence IIIG) tests and from field tests on large populations of older vehicles with different engine types. Based on these data, the PCEOCP recommended a ballot to allow the use of Test Method D7320 (Sequence IIIG) as an alternative to Test Method D6984 (Sequence IIIF) plus Test Method D5302 (Sequence VE) for demonstration of acceptable API SH, SJ, and SL performance on low phosphorus oils, establishing at least the mass fraction of phosphorus is 0.06 % as the minimum level. That ballot was approved by Subcommittee D02.B0 in May 2004.

- 4.1.3.4 Test Method D6593, the Sequence VG gasoline engine test, has been correlated with the Sequence VE gasoline engine test and with vehicles used in stop-and-go service prior to 2000, with regard to sludge and varnish deposit control.
- 4.1.3.5 Test Method D6709, the Sequence VIII gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions and has been shown to correlate with the L-38 gasoline engine test.<sup>13</sup>
- (1) The Sequence VIII gasoline engine test is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.3.6 In addition to passing performance in the engine tests, oils shall also meet bench test requirements (see Table 2), which are discussed in the following subsections:
- (1) Test Method D6557 (Ball Rust Test), was developed to replace the Sequence IID gasoline engine test, and evaluates the ability of an oil to prevent the formation of rust under short-trip service conditions.
- (2) The volatility of engine oils is one of several factors that relates to engine oil consumption. For this engine oil category, volatility is measured by Test Methods D5800 and D6417.
- (3) Test Method D6795, the Engine Oil Filterability Test (EOFT) and Test Method D6794, the Engine Oil Water Tolerance Test (EOWTT) screen for the formation of precipitates and gels which form in the presence of water and can cause oil filter plugging.
- (4) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency. For this engine oil
- <sup>13</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1471.

- category, phosphorus content is measured by either Test Method D4951 or D5185.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
- (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test Method D7097, the TEOST MHT-4 test may be useful in determining the piston deposit control capability of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low-temperature protection not adequately measured by Test Method D4684.
- 4.1.3.7 Licensing of the API SL category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.4 *CF-4*—Oil meeting the performance requirements in the following diesel and gasoline engine tests and bench test: 4.1.4.1 Test Method D6750, the 1K diesel engine test, has

been correlated with vehicles equipped with engines used in high-speed operation prior to 1989,<sup>14</sup> particularly with regard to deposits and oil consumption.

- 4.1.4.2 The T-6 has been correlated with vehicles equipped with engines used in high-speed operation prior to 1980,<sup>15</sup> particularly with regard to deposits, oil consumption, and ring wear. (An alternative is Test Method D6987/D6987M, the T-10 diesel engine test. See 4.1.9.2.)
- 4.1.4.3 The T-7 test has been correlated with vehicles equipped with engines operated largely under lugging conditions prior to 1984, <sup>16</sup> particularly with regard to oil thickening.
- 4.1.4.4 Test Method D5968, the bench corrosion test, has been shown to predict corrosion of engine oil-lubricated copper, lead, or tin-containing components used in diesel engines.<sup>17</sup> Test Method D5290, the NTC-400 diesel engine test, has been correlated with vehicles equipped with engines in highway operation prior to 1983, <sup>18</sup> particularly with regard to oil consumption control, deposits, and wear. Test Method D5290 is not listed in Table 3, as calibrated test stands are no longer available due to unavailability of critical test parts. It

<sup>&</sup>lt;sup>14</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1273.

<sup>&</sup>lt;sup>15</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1219.

<sup>&</sup>lt;sup>16</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1220.

<sup>&</sup>lt;sup>17</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1322.

<sup>&</sup>lt;sup>18</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report D02-1194.



# TABLE 3 C Engine Oil Categories

Category	Test Method	Rated or Measured Parameter	F	rimary Performance	Criteria
CF-4	D6709 (Sequence VIII)	Bearing weight loss, mg, max	33.0		
	T-6	Merit rating, <sup>A</sup> min	90		
	or	<b>-</b>	4=0		
	D6483 (T-9) <sup>B</sup>	Top piston ring weight loss, <sup>C</sup> average, mg, max	150		
	or Decor/DecorM (T 10)	Liner wear, µm, max	40		
	or, D6987/D6987M (T-10)	Top ring weight loss, mg, max Liner wear, µm, max	180 47		
	T-7	Average rate of kinematic viscosity increase during last	0.040		
	or	50 h, mm <sup>2</sup> /s at 100 °C/h, max	0.010		
	D5967 (T-8A) <sup>B</sup>	Average rate of kinematic viscosity increase from 100 to	0.20		
	, ,	150 h, mm <sup>2</sup> /s at 100 °C/h, max			
	D5968 (CBT) <sup>D</sup>	Copper, mg/kg increase, max	20		
		Lead, mg/kg increase, max	60		
		Tin, mg/kg increase, max	report		
		Copper strip rating, <sup>E</sup> max	3		
			Two-test <sup>F</sup>	Three-test <sup>F</sup>	Four-test <sup>F</sup>
	D6750 (1K)	A 1K test program <sup>F</sup> with a minimum of two tests,			
	, ,	acceptable according to the limits shown in the columns			
		to the right, is required to demonstrate performance for			
		this category.			
		Weighted demerits (WDK), G,H max	332	339	342
		Top groove fill (TGF), <sup>G</sup> %, max	24	26	27
		Top land heavy carbon (TLHC), G % max	4	4	5
		Average oil consumption, g/MJ, (0-252 h), max	0.139	0.139	0.139
		Final Oil consumption, g/MJ, (228-252 h) max	0.075	0.075	0.075
		Piston, ring, and liner scuffing		F	,
		Number of tests allowed	none	none <sup>E</sup>	none <sup>r</sup>
		Piston ring sticking	none	none	none
CF	D6618 (1M-PC)	Top groove fill (TGF), G, max	70 <sup>J</sup>	MTAC <sup>J</sup>	$MTAC^J$
		Weighted total demerits (WTD), max	240 <sup>J</sup>	WITAC	WITAC
		Piston ring sticking	none		
		Piston, ring and liner scuffing	none		
			One-Test	Two-Test <sup>K</sup>	Three-Test <sup>K</sup>
	D6709 (Sequence VIII)	Bearing weight loss, mg, max	29.3	31.9	33.0
CF-2	D6618 (1M-PC)	Weighted total demerits (WTD), <sup>G</sup> max	100 <sup>J</sup>	MTAC <sup>J</sup>	MTAC <sup>J</sup>
	, ,	Document Previ	One-Test	Two-Test <sup>L</sup>	Three-Test <sup>∠</sup>
	D-000 (0) ( 00TA)	0 11 1 11 11 11			
	D5862 (6V 92TA)	Cylinder liner scuffing area, % max	45.0	48.0	50.0
		Cylinder liner port plugging area,	2	2	2
		Average, % max Single cylinder, % max	0.50 0.4.11		
		Piston rings face distress demerits	8e72-0c4cdd	.6594 <mark>9</mark> 6/astm-	d4485-09
		No. 1 (fire ring), max	0.23	0.24	0.26
		Average of No. 2 and 3, max	0.20	0.21	0.22
	D6709 (Sequence VIII)	Bearing weight loss, mg, max	29.3	31.9 <sup>K</sup>	33.0 <sup>K</sup>
	,	3 - 3		Two-Test <sup>M</sup>	Three-Test <sup>M</sup>
			One-Test	I WO- Test	iiiiee-iest"
CG-4	D6750 (1N)	Weighted demerits (WDN) <sup>G,N</sup>	286.2	311.7	323.0
		Top groove fill (TGF), G %, max	20	23	25
		Top land heavy carbon (TLHC), 6 % max	3	4	5
		Oil consumption, g/MJ (0-250) h, max	0.5	0.5	0.5
		Piston, ring, and liner scuffing			,
		Number of tests allowed	none	none	none <sup>7</sup>
			none	none	none
	D5007 (T 0) C	Piston ring sticking			13.0
	D5967 (T-8) <sup>O</sup>	Viscosity increase at 3.8 % soot, mm <sup>2</sup> /s, max	11.5	12.5	100
	D5967 (T-8) <sup>O</sup>	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max	11.5 138	138	138
	. ,	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max	11.5 138 0.0844	138 0.0844	0.0844
	D5967 (T-8) <sup>O</sup> D6984 (Sequence IIIF)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C)	11.5 138	138	
	D6984 (Sequence IIIF)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max	11.5 138 0.0844 325	138 0.0844 349	0.0844 360
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max	11.5 138 0.0844 325	138 0.0844 349 173	0.0844 360 184
	D6984 (Sequence IIIF)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max	11.5 138 0.0844 325	138 0.0844 349	0.0844 360
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE	11.5 138 0.0844 325 150 29.3	138 0.0844 349 173 31.9 <sup>K</sup>	0.0844 360 184 33.0 <sup>K</sup>
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>P</sup> D6709 (Sequence VIII)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max  Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min²	11.5 138 0.0844 325 150 29.3	138 0.0844 349 173 31.9 <sup>K</sup> 0.5	0.0844 360 184 33.0 <sup>K</sup> 0.5
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max	11.5 138 0.0844 325 150 29.3 0.5 0.45	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (μm) max	11.5 138 0.0844 325 150 29.3	138 0.0844 349 173 31.9 <sup>K</sup> 0.5	0.0844 360 184 33.0 <sup>K</sup> 0.5
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)  D892 (Option A	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (µm) max Foaming characteristics	11.5 138 0.0844 325 150 29.3 0.5 0.45	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (µm) max Foaming characteristics Foaming/settling, mL, max	11.5 138 0.0844 325 150 29.3 0.5 0.45 (11.4)	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)  D892 (Option A	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (µm) max Foaming characteristics	11.5 138 0.0844 325 150 29.3 0.5 0.45	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)  D892 (Option A	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (µm) max Foaming characteristics Foaming/settling, max Sequence I	11.5 138 0.0844 325 150 29.3 0.5 0.45 (11.4)	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50
	D6984 (Sequence IIIF) or D7320 (Sequence IIIG) <sup>F</sup> D6709 (Sequence VIII)  D5966 (RFWT)  D892 (Option A	Viscosity increase at 3.8 % soot, mm²/s, max Filter plugging, differential pressure, kPa, max Oil consumption, g/MJ, max 60 h viscosity (at 40 °C) increase from 10 min sample, %, max Kinematic viscosity, % increase at 40 °C max Bearing weight loss, mg, max Used oil viscosity, mm²/s greater than SAE J300 lower limit for grade, min² Wear, mils, max (µm) max Foaming characteristics Foaming/settling, f mL, max Sequence I Sequence II	11.5 138 0.0844 325 150 29.3 0.5 0.45 (11.4)	138 0.0844 349 173 31.9 <sup>K</sup> 0.5 0.49	0.0844 360 184 33.0 <sup>K</sup> 0.5 0.50



## TABLE 3 Continued

Category	Test Method	Rated or Measured Parameter	Prim	ary Performance Cri	teria
		Lead, mg/kg increase, max	60		
		Tin, mg/kg increase, max Copper strip rating, <sup>E</sup> max	report 3		
		Soppor strip rating, max	One-test	Two-test <sup>T</sup>	Three-test $^T$
H-4	D6681 (1P) <sup>U</sup>	Weighted demerits (WDP), max	350	378	390
	( )	Top groove carbon (TGC), demerits, max	36	39	41
		Top land carbon (TLC), demerits, max	40	46	49
		Average Oil Consumption, g/h (0-360 h), max	12.4	12.4	12.4
		Final Oil Consumption, g/h (312-360 h), max	14.6	14.6	14.6
		Piston, ring, and liner scuffing	none	none	none <sup>1</sup>
	D6750 (1K) <sup>H</sup>	Weighted demerits (WDK), %, max	332	347	353
		Top groove fill (TGF), %, max	24	27	29
		Top land heavy carbon (TLHC), %, max	4	5	5
		Average Oil Consumption, g/MJ (0-250) h, max	0.139	0.139	0.139
		Piston, ring, and liner scuffing	none	none	none <sup>r</sup>
	D6483 (T-9)	Average Liner Wear, normalized to 1.75 % soot, µm max	25.4	26.6	27.1
		Average Top Ring Weight Loss, mg max <sup>C</sup>	120	136	144
		EOT Used Oil Lead Content less New Oil Lead			
	D0007/D000714 (T 40)	Content, mg/kg, max	25	32	36
	or, D6987/D6987M (T-10)	Liner wear, µm, max	32	34	35
		Ring wear, mg, max	150	159	163
	D7400 (T40)	Lead content at EOT, mg/kg, max	50	56	59
	or, D7422 (T-12)	Liner wear, µm, max	30.0	30.8	31.1
		Top Ring Weight Loss, mg, max	120	132	137
	DEOCE (DEWT)	Lead content at EOT, mg/kg, max	65	75	79
	D5966 (RFWT)	Average Pin Wear, mils, max	0.30	0.33	0.36
	D0000 (M11) V	(µm) max	(7.6)	(8.4)	(9.1)
	D6838 (M11) <sup>V</sup>	Rocker Pad Average Wt. Loss, normalized to 4.5 % soot,	6.5	7.5	8.0
		mg max Oil Filter Differential Pressure at EOT, kPa max	79	93	100
		Average Engine Sludge, CRC Merits at EOT, min	8.7	8.6	8.5
	or, the Cummins ISM test	Crosshead wear, mg, max	7.5	7.8	7.9
	or, the outlining low test	Oil filter delta pressure, at 150 h, kPa, max	7.5	95	103
		Sludge rating, CRC merits, min	8.1	8.0	8.0
	D5967 (Ext. T-8E) <sup>O</sup>	Relative Viscosity at 4.8 % Soot by	len.ai)	0.0	0.0
		TGA, max	2.1	2.2	2.3
		Viscosity increase at 3.8 % Soot by TGA, mm <sup>2</sup> /s, max	11.5	12.5	13.0
	D6984 (Sequence IIIF)	60 h Viscosity at 40 °C, increase from 10 min sample, %			
		max	295	295 (MTAC)W	295 (MTAC)W
	or D7320 (Sequence IIIG) <sup>P</sup>	Kinematic viscosity, % increase at 40 °C max	150	150 (MTAC)	150 (MTAC)
	D6894 (EOAT) <sup>S</sup>	Aeration, volume, % max	8.0	8.0 (MTAC) W	8.0 (MTAC) <sup>W</sup>
	D6594 (135 °C, HTC BT)	Used Oil Elemental Concentration 34485-09			
		Copper, mg/kg increase, max	82072-0c4cdd65		
		Lead, mg/kg increase, max	120		
		Tin, mg/kg increase	report		
		Copper strip rating, E max	3		
	D892 (Option A	Foaming/Settling, mL, max			
	not allowed)		10/0		
		Sequence I	10/0		
		Sequence II	20/0		
		Sequence III	10/0		
				Q V E 1 E/V/ 10	
	D5800 or	% volatility loss at 250°C may	SAE 10W-30	SAE 15W-40	
	D5800 or	% volatility loss at 250°C, max	SAE 10W-30 20	18	
	D6417	% volatility loss at 371°C, max	SAE 10W-30 20 17	18 15	
		% volatility loss at 371°C, max Kinematic Viscosity after shearing,	SAE 10W-30 20 17 SAE XW-30	18 15 SAE XW-40	
	D6417	% volatility loss at 371°C, max	SAE 10W-30 20 17 SAE XW-30 9.3	18 15 SAE XW-40 12.5	Three-test <sup>X</sup>
	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min	SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test <sup>x</sup>	Three-test <sup>X</sup>
I-4	D6417	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test <sup>x</sup>	402
I-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57	402 59
-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57 35	402 59 36
-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC),	SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57	402 59
1-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1	402 59 36 13.1
I-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption,	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57 35	402 59 36
1-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8	402 59 36 13.1 IOC + 1.8
l-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8	402 59 36 13.1 IOC + 1.8
1-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking	SAE 10W-30 20 17 SAE XW-30 9.3 One-test  382 52 31 13.1 IOC + 1.8 none none	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57 35 13.1 IOC + 1.8 none none	402 59 36 13.1 IOC + 1.8 none none
1-4	D6417 D6278	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350	18 15 SAE XW-40 12.5 Two-test <sup>x</sup> 396 57 35 13.1 IOC + 1.8 none none 378	402 59 36 13.1 IOC + 1.8 none none 390
l-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test  382 52 31 13.1 IOC + 1.8 none none 350 36	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8 none none 378 39	402 59 36 13.1 IOC + 1.8 none none 390 41
I-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max	SAE 10W-30 20 17 SAE XW-30 9.3  One-test  382 52 31 13.1  IOC + 1.8  none none 350 36 40	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8 none none 378 39 46	402 59 36 13.1 IOC + 1.8 none none 390 41 49
:I-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max	SAE 10W-30 20 17 SAE XW-30 9.3  One-test  382 52 31 13.1  IOC + 1.8  none none 350 36 40 12.4	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4
:I-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max	SAE 10W-30 20 17 SAE XW-30 9.3 One-test  382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6
SI-4	D6417 D6278 D6923 (1R)	% volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min  Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max	SAE 10W-30 20 17 SAE XW-30 9.3  One-test  382 52 31 13.1  IOC + 1.8  none none 350 36 40 12.4	18 15 SAE XW-40 12.5 Two-test <sup>X</sup> 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4