

SLOVENSKI STANDARD SIST EN IEC 61689:2022

01-junij-2022

Nadomešča: SIST EN 61689:2013

Ultrazvok - Fizioterapevtski sistemi - Specifikacije polja in merilne metode v frekvenčnem območju od 0,5 MHz do 5 MHz (IEC 61689:2022)

Ultrasonics - Physiotherapy systems - Field specifications and methods of measurement in the frequency range 0,5 MHz to 5 MHz (IEC 61689:2022)

iTeh STANDARD

Ultraschall - Physiotherapiesysteme - Feldspezifikation und Messverfahren im Frequenzbereich von 0,5 MHz bis 5 MHz (IEC 61689:2022)

Ultrasons - Systèmes de physiothérapie Spécifications des champs et méthodes de mesure dans la gamme de fréquences de 0,5 MHz à 5 MHz (IEC 61689:2022)

SIST EN IEC 61689:2022 Ta slovenski standard je jstoveten z:2000 EN IEC 61689:2022

/bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

ICS:

11.040.60 Terapevtska oprema

Therapy equipment

SIST EN IEC 61689:2022

en



iTeh STANDARD PREVIEW (standards.iteh.ai)

SIST EN IEC 61689:2022 https://standards.iteh.ai/catalog/standards/sist/a5a60639-7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

SIST EN IEC 61689:2022

EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

EN IEC 61689

April 2022

ICS 11.040.60

Supersedes EN 61689:2013

English Version

Ultrasonics - Physiotherapy systems - Field specifications and methods of measurement in the frequency range 0,5 MHz to 5 MHz (IEC 61689:2022)

Ultrasons - Systèmes de physiothérapie - Spécifications des champs et méthodes de mesure dans la plage de fréquences de 0,5 MHz à 5 MHz (IEC 61689:2022) Ultraschall - Physiotherapiesysteme - Feldspezifikation und Messverfahren im Frequenzbereich von 0,5 MHz bis 5 MHz (IEC 61689:2022)

This European Standard was approved by CENELEC on 2022-04-12, CENELEC members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration.

Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the CEN-CENELEC Management Centre or to any CENELEC member.

This European Standard exists in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CENELEC member into its own language and notified to the CEN-CENELEC Management Centre has the same status as the official versions.

CENELEC members are the national electrotechnical committees of Austria, Belgium, Bulgaria, Croatia, Cyprus, the Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Uthuania, Luxembourg, Malta, the Netherlands, Norway, Poland, Portugal, Republic of North Macedonia, Romania, Serbia, Slovakia, Slovenia, Spain, Sweden, Switzerland, Turkey and the United Kingdom.



European Committee for Electrotechnical Standardization Comité Européen de Normalisation Electrotechnique Europäisches Komitee für Elektrotechnische Normung

CEN-CENELEC Management Centre: Rue de la Science 23, B-1040 Brussels

European foreword

The text of document 87/784/FDIS, future edition 4 of IEC 61689, prepared by IEC/TC 87 "Ultrasonics" was submitted to the IEC-CENELEC parallel vote and approved by CENELEC as EN IEC 61689:2022.

The following dates are fixed:

- latest date by which the document has to be implemented at national (dop) 2023-01-12 level by publication of an identical national standard or by endorsement
- latest date by which the national standards conflicting with the (dow) 2025-04-12 document have to be withdrawn

This document supersedes EN 61689:2013 and all of its amendments and corrigenda (if any).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CENELEC shall not be held responsible for identifying any or all such patent rights.

Any feedback and questions on this document should be directed to the users' national committee. A complete listing of these bodies can be found on the CENELEC website.

iTeh STANDARD Endorsement notice

The text of the International Standard IEC 61689:2022 was approved by CENELEC as a European Standard without any modification.

In the official version, for Bibliography, the following notes have to be added for the standards indicated:

7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

- IEC 61828 NOTE Harmonized as EN IEC 61828
- IEC 62127-2 NOTE Harmonized as EN 62127-2
- IEC 62127-3 NOTE Harmonized as EN 62127-3
- IEC 62555 NOTE Harmonized as EN 62555
- IEC 63009 NOTE Harmonized as EN IEC 63009

Annex ZA (normative)

Normative references to international publications with their corresponding European publications

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

NOTE 1 Where an International Publication has been modified by common modifications, indicated by (mod), the relevant EN/HD applies.

NOTE 2 Up-to-date information on the latest versions of the European Standards listed in this annex is available here: <u>www.cenelec.eu</u>.

Publication	Year	<u>Title</u>	<u>EN/HD</u>	Year
IEC 60601-1	-	Medical electrical equipment - Part 1: General requirements for basic safety and essential	EN 60601-1	-
IEC 60601-2-5	-	Medical electrical equipment - Part 2-5: Particular requirements for the basic safety and essential performance of ultrasonic	EN 60601-2-5	-
IEC 61161	-	physiotherapy equipment Ultrasonics - Power measurement - Radiation force balances and performance requirements	EN 61161	-
IEC 62127-1	https 7bf5	Ultrasonic <u>SIST ENHydrophones:2022</u> Part 1: Measurement and characterization of medical (ultrasonic fields521f2c038e/sist-en-iec-61689		-



iTeh STANDARD PREVIEW (standards.iteh.ai)

SIST EN IEC 61689:2022 https://standards.iteh.ai/catalog/standards/sist/a5a60639-7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022



IEC 61689

Edition 4.0 2022-03

INTERNATIONAL STANDARD

NORME INTERNATIONALE

iTeh STANDARD

Ultrasonics – Physiotherapy systems – Field specifications and methods of measurement in the frequency range 0,5 MHz to 5 MHz

Ultrasons – Systèmes de physiothérapie – Spécifications des champs et méthodes de mesure dans la plage de fréquences de 0,5 MHz à 5 MHz

SIST EN IEC 61689:2022 https://standards.iteh.ai/catalog/standards/sist/a5a60639-7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

INTERNATIONAL ELECTROTECHNICAL COMMISSION

COMMISSION ELECTROTECHNIQUE INTERNATIONALE

ICS 11.040.60

ISBN 978-2-8322-1080-0

Warning! Make sure that you obtained this publication from an authorized distributor. Attention! Veuillez vous assurer que vous avez obtenu cette publication via un distributeur agréé.

 Registered trademark of the International Electrotechnical Commission Marque déposée de la Commission Electrotechnique Internationale

– 2 – IEC 61689:2022 © IEC 2022

CONTENTS

FOF	REWORD	5
INT	RODUCTION	7
1	Scope	8
2	Normative references	8
3	Terms and definitions	9
4	Symbols	18
5	Ultrasonic field specifications	19
6	Conditions of measurement and test equipment used	20
6	1 General	20
6	.2 Test vessel	
6	.3 Hydrophone	21
6	.4 RMS peak signal measurement	22
7	Type testing reference procedures and measurements	22
7	.1 General	22
7	.2 Rated output power	23
7	.3 Hydrophone measurements	23
7	.4 Effective radiating area	24
	7.4.1 Effective radiating area measurements	24
	7.4.2 Hydrophone positioning	24
	7.4.3 Beam cross-sectional area determination	24
	7.4.4 Active area gradient determination	24
	7.4.5 Beam type determination	25
	7.4.6 Effective radiating area calculation (00):2022	25
	7.4.7 Beam non-uniformity ratio calculation	25
-	7.4.8 Testing requirements	
/	.5 Reference type testing parameters	
0	.6 Acceptance criteria for reference type testing	20
0		
8	Deted extruct newer	21
0 0	2 Effective redicting cros	21 27
0 8	A Beam non-uniformity ratio	21 27
8	5 Effective intensity	27 28
8	6 Acceptance criteria for routine testing	20
9	Sampling and uncertainty determination	
9	1 Reference type testing measurements	28
9	2 Routine measurements	
9	.3 Uncertainty determination	
Ann	ex A (normative) Guidance for performance and safety	
А	.1 General	
A	A.2 Rated output power	
A		
A		
	A.4.1 General	

A.4.2 Rationale behind using a limiting value for the beam non-uniformity ratio 30 Annex B (normative) Raster scan measurement and analysis procedures 35 B.1 General 35 B.2 Requirements for raster scans 35 B.3 Requirements for analysis of raster scan data. 36 B.3.1 General 36 B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area, A_{BCS} . 36 Annex C (normative) Diametrical or line scans 37 C.1 General 37 C.2 Requirements for line scans 37 Annex D (informative) Rationale concerning the beam cross-sectional area definition. 41 Annex E (informative) Rationale concerning the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}). 42 Annex F (informative) Determining acoustic power through radiation force 44 Annex A (informative) Validity bit on power measurements of the beam cross-sectional area (A_{BCS}). 46 Annex H (informative) Effective radiating area measurements of the beam cross-sectional area (A_{BCS}). 49 1.2 Coccept of aperture method. 4	IEC 61689	9:2022 © IEC 2022 - 3 -			
Annex B (normative) Raster scan measurement and analysis procedures	A.4.2	Rationale behind using a limiting value for the beam non-uniformity ratio (<i>R</i> _{BN})	. 30		
B.1 General 35 B.2 Requirements for raster scans 35 B.3 Requirements for analysis of raster scan data 36 B.3.1 General 36 B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area, A_{BCS} 36 Annex C (normative) Diametrical or line scans 37 C.1 General 37 C.2 Requirements for line scans 37 C.3 Analysis of scans 37 C.3 Analysis of scans 37 Annex D (informative) Factor used to convert the beam cross-sectional area definition 41 Annex F (informative) Determining acoustic power through radiation force 44 Annex A (informative) Influence of hydrophone effective tradiation force 46 Annex H (informative) Influence of hydrophone effective tradiation force 47 Annex I (informative) Effective radiating area measurements using a radiation force 49 1.1 General 49 49 41 Annex I (informative) Effective radiating area 52	Annex B ((normative) Raster scan measurement and analysis procedures	.35		
B.2 Requirements for raster scans 35 B.3 Requirements for analysis of raster scan data 36 B.3.1 General 36 B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area, A_{BCS} 36 Annex C (normative) Diametrical or line scan measurement and analysis procedures 37 C.1 General 37 C.2 Requirements for line scans 37 C.3 Analysis of scans 37 Annex E (informative) Fationale concerning the beam cross-sectional area definition 41 Annex E (informative) Determining acoustic power through radiation force 44 Annex G (informative) Validity bitour power measurements of the beam cross-sectional area (A_{BCS}) 46 Annex H (informative) Influence of hydrophone effective traination force 49 1.1 General 49 49 1.2 Concept of aperture method: ENULG (4649) 2022 50 1.3.1 Requirements for the aperture method: ENULG (4649) 2022 50 1.3.2 Apertures 50 51 1.3 <td< td=""><td>B.1</td><td>General</td><td>.35</td></td<>	B.1	General	.35		
B.3 Requirements for analysis of raster scan data 36 B.3.1 General 36 B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area. A_{BCS} 36 Annex C (normative) Diametrical or line scan measurement and analysis procedures 37 C.1 General 37 C.2 Requirements for line scans 37 C.3 Analysis of scans 37 C.4 General 37 C.5 Analysis of scans 37 Annex E (informative) Rationale concerning the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}) 42 Annex F (informative) Determining acoustic power through radiation force 44 Annex A (informative) Influence of hydrophone effective viameter 47 Annex I (informative) Influence of hydrophone effective viameter 47 Annex I (informative) Effective radiating area measurements using a radiation force balance and absorbing aperture method; ENLEC 61689:2022 49 1.1 General 49 49 49 1.2 Concept of aperture m	B.2	Requirements for raster scans	.35		
B.3.1 General 36 B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area, A_{BCS} . 36 Annex C (normative) Diametrical or line scan measurement and analysis procedures. 37 C.1 General 37 C.2 Requirements for line scans. 37 C.3 Analysis of scans 37 C.3 Analysis of scans 37 C.4 General 41 Annex D (informative) Rationale concerning the beam cross-sectional area definition 41 Annex E (informative) Rationale concerning the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}). 42 Annex K (informative) Determining acoustic power through radiation force 44 Annex K (informative) Influence of nydophone effective tradiation force 44 Annex K (informative) Effective radiating area measurements using a radiation force 49 1.1 General 49 49 49 49 1.2 Concept of aperture method. <i>Ext. Mac. 6.16.89.0022</i> 50 50 1.3.1 Ra	B.3	Requirements for analysis of raster scan data	.36		
B.3.2 Total mean square acoustic pressure 36 B.3.3 Calculation of the beam cross-sectional area, A_{BCS}	B.3.1	General	.36		
B.3.3 Calculation of the beam cross-sectional area, A_{BCS}	B.3.2	2 Total mean square acoustic pressure	.36		
Annex C (normative) Diametrical or line scan measurement and analysis procedures 37 C.1 General	B.3.3	Calculation of the beam cross-sectional area, <i>A</i> _{BCS}	.36		
C.1 General. 37 C.2 Requirements for line scans. 37 C.3 Analysis of scans. 37 Annex D (informative) Rationale concerning the beam cross-sectional area definition. 41 Annex E (informative) Factor used to convert the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}). 42 Annex F (informative) Determining acoustic power through radiation force measurements. 44 Annex G (informative) Validity brow-power measurements of the beam cross-sectional area (A_{BCS}). 46 Annex H (informative) Influence of hydrophone effective tradiation force balance and absorbing apertures radiation area measurements using a radiation force balance and absorbing apertures and the standard stata stat	Annex C ((normative) Diametrical or line scan measurement and analysis procedures	.37		
C.2 Requirements for line scans 37 C.3 Analysis of scans 37 Annex D (informative) Rationale concerning the beam cross-sectional area definition 41 Annex E (informative) Factor used to convert the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}) 42 Annex F (informative) Determining acoustic power through radiation force measurements 44 Annex G (informative) Validity bit on power measurements of the beam cross-sectional area (A_{ECS}) 46 Annex H (informative) Influence of hydrophone effective diameter 47 Annex I (informative) Effective radiating area measurements using a radiation force balance and absorbing apertures 49 1.1 General 49 1.2 Concept of aperture method, ENULEC 61689;2022 50 1.3 Requirements for the aperture method, ENULEC 61689;2022 50 1.3.1 Radiation force balance 521;2c(13&c/sist-cn-icc-fa1689;2022 50 1.3.2 Apertures 50 1.4 Measurement procedure for determining the effective radiating area 52 1.6 Implementation of the aperture technique 58 1.7 <td< td=""><td>C.1</td><td>General</td><td>. 37</td></td<>	C.1	General	. 37		
C.3 Analysis of scans 37 Annex D (informative) Rationale concerning the beam cross-sectional area definition 41 Annex E (informative) Factor used to convert the beam cross-sectional area (A_{BCS}) at the face of the treatment head to the effective radiating area (A_{ER}) 42 Annex F (informative) Determining acoustic power through radiation force measurements 44 Annex G (informative) Validity of ton-power measurements of the beam cross-sectional area (A_{BCS}) 46 Annex I (informative) Influence of hydrophone effective fiameter 47 Annex I (informative) Effective radiating area measurements using a radiation force balance and absorbing aper ures 49 1.1 General 49 1.2 Concept of aperture metbod, EN.IEC.61689;2022 49 1.3 Requirements for the aperture metbod, EN.IEC.61689;2022 50 1.3.1 Radiation force balance 5212/2/0138/sist.en.icc.61689;2022 50 1.3.2 Apertures 50 1.4 Measurement procedure for determining the effective radiating area 51 1.5 Analysis of raw data to derive the effective radiating area 52 1.6 Implementation of the aperture techinque 58 <t< td=""><td>C.2</td><td>Requirements for line scans</td><td>. 37</td></t<>	C.2	Requirements for line scans	. 37		
Annex D (informative) Rationale concerning the beam cross-sectional area definition	C.3	Analysis of scans	. 37		
Annex E (informative) Factor used to convert the beam cross-sectional area (A_{ECS}) at the face of the treatment head to the effective radiating area (A_{EC}). 42 Annex F (informative) Determining acoustic power through radiation force 44 Annex G (informative) Validity of too power measurements of the beam cross-sectional area (A_{ECS}). 46 Annex H (informative) Influence of hydrophone effective fiameter 47 Annex I (informative) Effective radiating area measurements using a radiation force 49 1.1 General. 49 1.2 Concept of aperture method. EN IEC 41689:3022 49 1.3 Requirements for the aperture method glandards/sist/s5a60639 50 1.3.1 Radiation force balance 521/2c038c/sist-encice/51689-2022 50 1.3.2 Apertures 50 1.4 Measurement procedure for determining the effective radiating area 51 1.5 Analysis of raw data to derive the effective radiating area 52 1.6 Implementation of the aperture technique 58 1.7 Relationship of results to reference testing method 62 Bibliography 64 Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , whe	Annex D ((informative) Rationale concerning the beam cross-sectional area definition	.41		
the face of the treatment head to the effective radiating area (A_{ER})	Annex E ((informative) Factor used to convert the beam cross-sectional area ($A_{\sf BCS}$) at			
Annex F (informative) Determining acoustic power through radiation force 44 Annex G (informative) Validity of two-power measurements of the beam cross-sectional area (A_{BCS}) 46 Annex I (informative) Influence of hydrophone effective diameter 47 Annex I (informative) Effective radiating area measurements using a radiation force balance and absorbing apertures and an encourcements using a radiation force balance and absorbing apertures and an encourcements using a radiation force balance and absorbing apertures and an encourcements and an encourcements and the effective radiating force balance 321f2c038c/sist.en.ice.fol.689.2022 49 1.1 General 49 1.2 Concept of aperture method. EN IEC 61689.2022 50 1.3.1 Radiation force balance 521f2c038c/sist.en.ice.fol.689.2022 50 1.3.2 Apertures 50 1.4 Measurement procedure for determining the effective radiating area 51 1.5 Analysis of raw data to derive the effective radiating area 52 1.6 Implementation of the aperture technique 58 1.7 Relationship of results to reference testing method 59 Annex J (informative) Guidance on uncertainty determination 60 Annex J (informative) Guidance on uncertainty determination 61 Annex	the face o	of the treatment head to the effective radiating area (A _{ER})	.42		
Annex G (informative)Validity of low-power measurements of the beam cross- sectional area (A_{BCS})	Annex F (measurem	(informative) Determining acoustic power through radiation force nents	.44		
Annex H (informative) Influence of hydrophone effective diameter	Annex G ((informative) Validity of low-power measurements of the beam cross-	46		
Annex I (informative) Effective radiating area measurements using a radiation force balance and absorbing apertures and a radiation force. 49 1.1 General	Annex H ((informative) Influence of hydrophone effective diameter	.40		
balance and absorbing apertures critical. List in the interval of the second critical interval of the second	Annex I (i	nformative) Effective radiating area measurements using a radiation force	1		
1.1General.491.2Concept of aperture method r.E.N.IEC. 61689;2022491.3Requirements for the aperture method gistandards/sist/a5a60639.501.3.1Radiation force balance 52112c03&c/sist.en.icc.61689.2022501.3.2Apertures501.4Measurement procedure for determining the effective radiating area511.5Analysis of raw data to derive the effective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of $R_{\rm BN}$ values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor $F_{\rm ac}$ as a function of the ka product for ka product between 40 and 16043Figure I.1 – Schematic representation of aperture measurement set-up50Figure I.2 – Measured power as a function of aperture diameter for commercially	balance a		.49		
1.2Concept of aperture method C.EN.IEC.61689:2022491.3Requirements for the aperture method gistandards/sist/a5a60639501.3.1Radiation force balance52112c03&c/sist-en-icc-61689-2022501.3.2Apertures501.4Measurement procedure for determining the effective radiating area511.5Analysis of raw data to derive the effective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 16043Figure I.2 – Measured power as a function of aperture diameter for commercially50	I.1	General	.49		
1.3 Requirements for the aperture method gistandards/sista/add/6/34	1.2	Concept of aperture method <u>F.EN.IEC.61689:2022</u>	.49		
1.3.1Radiation-force-balance S2112CUSACISUS-CH-ECC-DEDS-2022501.3.2Apertures501.4Measurement procedure for determining the effective radiating area511.5Analysis of raw data to derive the effective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 16043Figure I.1 – Schematic representation of aperture measurement set-up50Figure I.2 – Measured power as a function of aperture diameter for commercially50	1.3	Requirements rotaneapenture methoog standards/sist/aba60639-	.50		
1.3.2Apertures501.4Measurement procedure for determining the effective radiating area511.5Analysis of raw data to derive the effective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 16043Figure I.1 – Schematic representation of aperture measurement set-up50Figure I.2 – Measured power as a function of aperture diameter for commercially	1.3.1	Radiation-force-balance)32112CU3&e/Sist-en-iec-01089-2022	.50		
1.4Measurement procedure for determining the effective radiating area511.5Analysis of raw data to derive the effective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 16043Figure I.1 – Schematic representation of aperture measurement set-up50Figure I.2 – Measured power as a function of aperture diameter for commercially	1.3.2	Apertures	.50		
1.5Analysis of Yaw data to derive the elective radiating area521.6Implementation of the aperture technique581.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$	1.4	Analysis of row data to derive the offective radiating area	.01		
1.0Implementation of the aperture technique561.7Relationship of results to reference testing method59Annex J (informative)Guidance on uncertainty determination60Annex K (informative)Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ 33Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies34Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 16043Figure I.1 – Schematic representation of aperture measurement set-up50Figure I.2 – Measured power as a function of aperture diameter for commercially	1.5	Implementation of the aperture technique	. 52 59		
Annex J (informative) Guidance on uncertainty determination60Annex K (informative) Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$ Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and 	1.0	Relationship of results to reference testing method	.50		
Annex K (informative) Examples of pulse duration and pulse repetition period of amplitude modulated waves	Δnnev I (i	informative) Guidance on uncertainty determination	60		
Armex K (mormative) Examples of pulse duration and pulse repetition period of amplitude modulated waves62Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$		(informative) Examples of pulse duration and pulse repetition period of	.00		
Bibliography64Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$	amplitude	modulated waves	.62		
Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$	Bibliograp	bhy	.64		
Figure A.1 – Normalized, time-averaged values of acoustic intensity (solid line) and of one of its plane-wave approximations (broken line), existing on the axis of a circular piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$					
piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$	Figure A.1 one of its	1 – Normalized, time-averaged values of acoustic intensity (solid line) and of plane-wave approximations (broken line), existing on the axis of a circular			
Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and frequencies	piston sou	piston source of $ka = 30$, plotted against the normalized distance s_n , where $s_n = \lambda z/a^2$			
frequencies 34 Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product 34 between 40 and 160 43 Figure I.1 – Schematic representation of aperture measurement set-up 50 Figure I.2 – Measured power as a function of aperture diameter for commercially	Figure A.2	Figure A.2 – Histogram of R_{BN} values for 37 treatment heads of various diameters and			
 Figure E.1 – Conversion factor F_{ac} as a function of the ka product for ka product between 40 and 160	frequencies				
Figure I.1 – Schematic representation of aperture measurement set-up	Figure E.1 – Conversion factor F_{ac} as a function of the <i>ka</i> product for <i>ka</i> product				
Figure 1.1 – Schematic representation of aperture measurement set-up	Eigure 1.1 Schematic representation of exerture measurement act up				
Figure 1.2 – Measured power as a function of aperture diameter for commercially		Eigure 1.2 Measured power on a function of aperture diameter for commercially			
available 1 MHz physiotherapy treatment heads54	.54				

Figure I.3 – Cumulative sum of annular power contributions, previously sorted in descending order of intensity contributions, plotted against the cumulative sum of their	
respective annular areas	58
Figure K.1 – Example 1: Tone-burst (i.e. rectangular modulation waveform)	62
Figure K.2 – Example 2: Half-wave modulation with no filtering of the AC mains voltage	62
Figure K.3 – Example 3: Full-wave modulation with no filtering of the AC mains voltage	62
Figure K.4 – Example 4: Half-wave modulation with filtering of the AC mains voltage; filtering insufficient to define the wave as continuous wave (3.17)	63
Figure K.5 – Example 5: Full-wave modulation with filtering of the AC mains voltage; filtering insufficient to define the wave as continuous wave (3.17)	63
Table C.1 – Constitution of the transformed array [B] used for the analysis of half-line scans	39
Table F.1 – Necessary target size, expressed as the minimum target radius b , as a function of the ultrasonic frequency, f , the effective radius of the treatment head, a_1 , and the terms distance is calculated in accordance with $A = 2.4$ of $I = 0.6446442042$	
(see [8])	45
Table G.1 – Variation of the beam cross-sectional area $A_{BCS}(z)$ with the indicated	
output power from two transducers	46
Table H.1 – Comparison of measurements of the beam cross-sectional area $A_{BCS}(z)$ made using hydrophones of geometrical active element radii 0,3 mm, 0,5 mm and	
2,0 mm	48
Table I.1 – Aperture measurement check sheet	53
Table I.2 – Annular power contributions I.2. C.S. II.C.II.2.I.	55
Table I.3 – Annular intensity contributions	55
Table I.4 – Annular intensity contributions, sorted in descending order	56
Table I.5 – Annular power contributions, sorted in descending order of intensity contribution	56
Table I.6 – Cumulative sum of annular power contributions, previously sorted in descending order of intensity contribution, and the cumulative sum of their respective	F7
amual aleas	57

IEC 61689:2022 © IEC 2022

INTERNATIONAL ELECTROTECHNICAL COMMISSION

ULTRASONICS – PHYSIOTHERAPY SYSTEMS – FIELD SPECIFICATIONS AND METHODS OF MEASUREMENT IN THE FREQUENCY RANGE 0,5 MHz TO 5 MHz

FOREWORD

- 1) The International Electrotechnical Commission (IEC) is a worldwide organization for standardization comprising all national electrotechnical committees (IEC National Committees). The object of IEC is to promote international co-operation on all questions concerning standardization in the electrical and electronic fields. To this end and in addition to other activities, IEC publishes International Standards, Technical Specifications, Technical Reports, Publicly Available Specifications (PAS) and Guides (hereafter referred to as "IEC Publication(s)"). Their preparation is entrusted to technical committees; any IEC National Committee interested in the subject dealt with may participate in this preparatory work. International, governmental and non-governmental organizations for Standardization (ISO) in accordance with conditions determined by agreement between the two organizations.
- The formal decisions or agreements of IEC on technical matters express, as nearly as possible, an international consensus of opinion on the relevant subjects since each technical committee has representation from all interested IEC National Committees.
- 3) IEC Publications have the form of recommendations for international use and are accepted by IEC National Committees in that sense. While all reasonable efforts are made to ensure that the technical content of IEC Publications is accurate, IEC cannot be held responsible for the way in which they are used or for any misinterpretation by any end user.
- 4) In order to promote international uniformity, IEC National Committees undertake to apply IEC Publications transparently to the maximum extent possible in their national and regional publications. Any divergence between any IEC Publication and the corresponding national or regional publication shall be clearly indicated in the latter.
- 5) IEC itself does not provide any attestation of conformity. Independent certification bodies provide conformity assessment services and, in some areas, access to IEC marks of conformity. IEC is not responsible for any services carried out by independent certification bodies.
- 6) All users should ensure that they have the latest edition of this publication.
- 7) No liability shall attach to IEC or its directors, employees, servants or agents including individual experts and members of its technical committees and IEC National Committees for any personal injury, property damage or other damage of any nature whatsoever, whether direct or indirect, or for costs (including legal fees) and expenses arising out of the publication, use of, or reliance upon, this IEC Publication or any other IEC Publications.
- 8) Attention is drawn to the Normative references cited in this publication. Use of the referenced publications is indispensable for the correct application of this publication.
- 9) Attention is drawn to the possibility that some of the elements of this IEC Publication may be the subject of patent rights. IEC shall not be held responsible for identifying any or all such patent rights.

IEC 61689 has been prepared by IEC technical committee 87: Ultrasonics. It is an International Standard.

This fourth edition cancels and replaces the third edition published in 2013. This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition.

- a) The requirement on water oxygen content is specified in 6.1.
- b) Former recommendations in 6.2 have been changed to become requirements.
- c) Several definitions in Clause 3 have been updated in line with other TC 87 documents.
- d) The formerly informative Annex A has been changed to become normative, and now contains details on how conformance with IEC 60601-2-5 requirements is checked.
- e) Annex D has been considerably shortened and reference to a now withdrawn regulatory document has been removed.

- 6 -

IEC 61689:2022 © IEC 2022

The text of this International Standard is based on the following documents:

Draft	Report on voting	
87/784/FDIS	87/789/RVD	

Full information on the voting for its approval can be found in the report on voting indicated in the above table.

The language used for the development of this International Standard is English.

This document was drafted in accordance with ISO/IEC Directives, Part 2, and developed in accordance with ISO/IEC Directives, Part 1 and ISO/IEC Directives, IEC Supplement, available at www.iec.ch/members_experts/refdocs. The main document types developed by IEC are described in greater detail at www.iec.ch/standardsdev/publications.

NOTE The following print types are used:

- Requirements: in Arial 10 point
- Notes: in Arial 8 point
- Words in **bold** in the text are defined in Clause 3
- Symbols and formulae: Times New Roman + Italic
- 'ANDARD Compliance clauses: in Arial Italic 'eh S'I

The committee has decided that the contents of this document will remain unchanged until the stability date indicated on the IEC website under webstore.iec.ch in the data related to the specific document. At this date, the document will be

reconfirmed, •



- withdrawn, .
- replaced by a revised edition, or https://standards.iteh.ai/catalog/standards/sist/a5a60639-
- amended. 7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

IEC 61689:2022 © IEC 2022

- 7 -

INTRODUCTION

Ultrasound at low megahertz frequencies is widely used in medicine for the purposes of physiotherapy. Such equipment consists of a generator of high frequency electrical energy and usually a hand-held **treatment head**, often referred to as an applicator. The **treatment head** contains a transducer, usually a disc of piezoelectric material, for converting the electrical energy to **ultrasound** and is often designed for contact with the human body.

iTeh STANDARD PREVIEW (standards.iteh.ai)

SIST EN IEC 61689:2022 https://standards.iteh.ai/catalog/standards/sist/a5a60639-7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

ULTRASONICS – PHYSIOTHERAPY SYSTEMS – FIELD SPECIFICATIONS AND METHODS OF MEASUREMENT IN THE FREQUENCY RANGE 0,5 MHz TO 5 MHz

1 Scope

This document is applicable to ultrasonic equipment designed for physiotherapy containing an **ultrasonic transducer** generating continuous or quasi-continuous (e.g. tone burst) wave **ultrasound** in the frequency range 0,5 MHz to 5 MHz. This document only relates to **ultrasonic physiotherapy equipment** employing a single plane non-focusing circular transducer per **treatment head**, producing static beams perpendicular to the face of the **treatment head**.

This document specifies:

- methods of measurement and characterization of the output of ultrasonic physiotherapy equipment based on reference testing methods;
- characteristics to be specified by manufacturers of ultrasonic physiotherapy equipment based on reference testing methods;
- guidelines for safety of the ultrasonic field generated by ultrasonic physiotherapy equipment;
- methods of measurement and characterization of the output of ultrasonic physiotherapy equipment based on routine testing methods;
- acceptance criteria for aspects of the output of ultrasonic physiotherapy equipment based on routine testing methods.

Therapeutic value and methods of <u>use of ultrasonic physio</u>therapy equipment are not within the scope of this document_{tandards.iteh.ai/catalog/standards/sist/a5a60639-}

7bf5-463a-8b83-d6521f2c038e/sist-en-iec-61689-2022

Ultrasonic physiotherapy equipment using **ultrasound** in the frequency range from 20 kHz to 500 kHz is dealt with in IEC 63009.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60601-1, Medical electrical equipment – Part 1: General requirements for basic safety and essential performance

IEC 60601-2-5, Medical electrical equipment – Part 2-5: Particular requirements for the basic safety and essential performance of ultrasonic physiotherapy equipment

IEC 61161, Ultrasonics – Power measurement – Radiation force balances and performance requirements

IEC 62127-1, Ultrasonics – Hydrophones – Part 1: Measurement and characterization of medical ultrasonic fields

IEC 61689:2022 © IEC 2022 - 9 -

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

3.1

absolute maximum rated output power

sum of the **rated output power**, the 95 % confidence overall uncertainty in the **rated output power**, and the maximum increase in the **rated output power** for a ± 10 % variation in the rated value of the mains voltage

Note 1 to entry: The possibility of variation in the **rated output power** resulting from ± 10 % variation in the rated value of the mains voltage should be checked by using a variable output transformer between the mains voltage supply and the **ultrasonic physiotherapy equipment**. See Clause A.2 for further guidance.

Note 2 to entry: Absolute maximum rated output power is expressed in watts (W).

3.2

active area coefficient

 \tilde{q} uotient of the active area gradient, *m*, and the beam cross-sectional area at 0,3 cm from the face of the treatment head, $A_{BCS}(0.3 \text{ cm})$

i'l'eh S'l'ANI

Note 1 to entry: Active area coefficient is expressed in units of one per metre (m^{-1}) .

3.3

active area gradient

SIST EN IEC 61689:2022

^m https://standards.iteh.ai/catalog/standards/sist/a5a60639ratio of the difference of the **beam cross-sectional area** at z_N , $A_{BCS}(z_N)$ and the **beam crosssectional area** at 0,3 cm from the face of the **treatment head**, $A_{BCS}(0,3 \text{ cm})$, divided by the difference of the respective distances

$$m = \frac{A_{\text{BCS}}(z_N) - A_{\text{BCS}}(0,3 \text{ cm})}{z_N - 0,3 \text{ cm}}$$
(1)

where

 A_{BCS} is the beam cross-sectional area;

 z_N is the distance from the face of the **treatment head** to the last maximum of the **RMS** acoustic pressure on the beam alignment axis

Note 1 to entry: Active area gradient is expressed in metres (m).

[SOURCE: IEC 61689:2013, 3.3, modified – The calculation scheme of the gradient was added to the definition, and the formula was added.]

3.4

absolute maximum beam non-uniformity ratio

beam non-uniformity ratio plus the 95 $\bar{\%}$ confidence overall uncertainty in the beam non-uniformity ratio