



SLOVENSKI STANDARD
oSIST prEN IEC 60034-2-3:2023
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Električni rotacijski stroji - 2-3. del: Posebne preskusne metode za ugotavljanje izgub in izkoristka motorja na izmenični tok, napajanega prek pretvornikov

Rotating electrical machines - Part 2-3: Specific test methods for determining losses and efficiency of converter-fed AC motors

Drehende elektrische Maschinen – Teil 2-3: Besondere Verfahren zur Bestimmung der Verluste und des Wirkungsgrades von umrichter gespeisten Wechselstrommaschinen

Machines électriques tournantes - Partie 2-3: Méthodes d'essai spécifiques pour la détermination des pertes et du rendement des moteurs à courant alternatif alimentés par convertisseur

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| OF INTEREST TO THE FOLLOWING COMMITTEES: | PROPOSED HORIZONTAL STANDARD: <input type="checkbox"/> Other TC/SCs are requested to indicate their interest, if any, in this CDV to the secretary. |
| FUNCTIONS CONCERNED: <input type="checkbox"/> EMC <input type="checkbox"/> ENVIRONMENT <input type="checkbox"/> QUALITY ASSURANCE <input type="checkbox"/> SAFETY | |
| <input checked="" type="checkbox"/> SUBMITTED FOR CENELEC PARALLEL VOTING Attention IEC-CENELEC parallel voting The attention of IEC National Committees, members of CENELEC, is drawn to the fact that this Committee Draft for Vote (CDV) is submitted for parallel voting. https://standards.iteh.ai/catalog/standards/sist/7b997e89-5e24-4794-a454-a1d78fc60d0f/osist-pr-en-iec-60034-2-3-2023 The CENELEC members are invited to vote through the CENELEC online voting system. | <input type="checkbox"/> NOT SUBMITTED FOR CENELEC PARALLEL VOTING |

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| TITLE: Rotating electrical machines – Part 2-3: Specific test methods for determining losses and efficiency of converter-fed AC motors |
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| NOTE FROM TC/SC OFFICERS: |
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INTERNATIONAL ELECTROTECHNICAL COMMISSION

ROTATING ELECTRICAL MACHINES –

Part 2-3: Specific test methods for determining losses and efficiency of converter-fed AC motors

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International Standard IEC 60034-2-3 has been prepared by IEC technical committee 2: Rotating machinery.

This second edition cancels and replaces the first edition of IEC 60034-2-3, published in 2020.

The text of this International Standard is based on the following documents:

| FDIS | Report on voting |
|------|------------------|
| | |

Full information on the voting for the approval of this International Standard can be found in the report on voting indicated in the above table.

This document has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts in the IEC 60034 series, published under the general title *Rotating electrical machines*, can be found on the IEC website.

The committee has decided that the contents of this document will remain unchanged until the stability date indicated on the IEC website under "<http://webstore.iec.ch>" in the data related to the specific document. At this date, the document will be

- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

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1

INTRODUCTION

2 The objective of this document is to define test methods for determining total losses including
3 additional high frequency motor losses and efficiency of converter-fed motors. Additional high
4 frequency losses appear in addition to the losses on nominally sinusoidal power supply as
5 determined by the methods of IEC 60034-2-1. Results determined according to this document
6 are intended to allow comparison of losses and efficiency of different motors if fed by
7 converters.

8 Furthermore, the document gives seven standardized operating points to characterize the
9 development of losses and efficiency across the whole torque/speed range. An interpolation
10 procedure is provided to calculate losses and efficiency at any operating point (torque, speed).

11 In power-drive systems (PDS), the motor and the frequency converter are often manufactured
12 by different suppliers. Motors of the same design are produced in large quantities. They may
13 be operated from the grid or from frequency converters of many different types, supplied by
14 many different manufacturers. The individual converter properties (switching frequency, DC link
15 voltage level, etc.) will also influence the system efficiency. As it is impractical to determine
16 motor losses for every combination of motor, frequency converter, connection cable, output
17 filter and parameter settings, this document describes a limited number of approaches,
18 depending on the voltage level and the rating of the motor under test.

19 The losses determined with the comparable converter as defined in this document are not
20 intended to represent the losses in the final application. They provide, however, an objective
21 basis for comparing different motor designs with respect to suitability for converter operation.

22 In general, if fed from a converter, motor losses are higher than during operation on a nominally
23 sinusoidal system, even though the converter normally enables vast energy savings overall on
24 system level, if the motor and the load application can be operated with variable speed. The
25 additional high frequency losses depend on the harmonic spectrum of the impressed converter
26 output quantity (either current or voltage) which is influenced by its circuitry and control method.
27 For further information, see IEC TS 60034-25.

28 It is not the purpose of this document to define test procedures either for power drive systems
29 or for frequency converters alone.

30 **Comparable converter**

31 Latest experience and theoretical analysis have shown that the additional high frequency motor
32 losses generally do not increase much with load. The methods in this document are mainly
33 based on supplies from converters with pulse width modulation (PWM).

34 With respect to these types of converters and the growing need for verification of compliance
35 with national energy efficiency regulations, this document defines a so-called comparable
36 converter for testing of low voltage motors.

37 In principle, the comparable converter is a voltage source with a typical high frequency harmonic
38 content supplying the motor under test. It is not applicable to medium voltage motors.

39 **Limitations for the application of the comparable converter**

40 It must be noted that the test method with the comparable converter described herein is a
41 standardized method intended to give comparable efficiency figures for standardized test
42 conditions. A motor ranking with respect to suitability for converter operation may be derived,
43 but it is not equivalent to determining of the actual motor losses for operation with a specific

44 converter which requires a test of the whole power drive system (PDS) with the specific
45 converter used in the final application.

46 Deviations are also expected for motors driven by multi-level voltage source or current source
47 converters where the additional high frequency motor losses differ much more depending on
48 speed and load than for two-level voltage source converters. Hence the determination of losses
49 and efficiency should use procedures where the motor is operated together with the same
50 converter with which it is driven in service.

51 Another option is the determination of the additional high frequency motor losses by calculation.
52 If this is requested, then the pulse pattern of the converter is required. Such procedures are not
53 part of this standard.

54 The interpolation of losses and efficiency at any operating point (torque, speed) is applicable
55 to the constant flux range and the field weakening and overload range.

56

57

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ROTATING ELECTRICAL MACHINES –

Part 2-3: Specific test methods for determining losses and efficiency of converter-fed AC motors

65 **1 Scope**

66 This part of IEC 60034 specifies test methods and an interpolation procedure for determining
67 losses and efficiencies of converter-fed motors. The motor is then part of a variable frequency
68 power drive system (PDS) as defined in IEC 61800-9-2.

69 Applying the approach of the comparable converter, the motor efficiency determined by use of
70 this document is applicable for comparison of different low voltage motor designs only. The
71 comparable converter approach is not applicable to medium voltage motors.

72 The document also specifies procedures to determine motor losses at any load point (torque,
73 speed) within the constant flux range (constant torque range, base speed range), the field
74 weakening range and the overload range based on determination of losses at seven
75 standardized load points. This procedure is applicable to any variable speed AC motor
76 (induction and synchronous) rated according to IEC 60034-1 for operation on a variable
77 frequency and variable voltage power supply.

78 **2 Normative references**

79 The following documents are referred to in the text in such a way that some or all of their content
80 constitutes requirements of this document. For dated references, only the edition cited applies.
81 For undated references, the latest edition of the referenced document (including any
82 amendments) applies.

83 IEC 60034-1, *Rotating electrical machines – Part 1: Rating and performance*

84 IEC 60034-2-1, *Rotating electrical machines – Part 2-1: Standard methods for determining
85 losses and efficiency from tests (excluding machines for traction vehicles)*

86 IEC 60034-30-1, *Rotating electrical machines – Part 30-1: Efficiency classes of line operated
87 AC motors (IE code)*

88 IEC 61000-2-4, *Electromagnetic compatibility (EMC) – Part 2-4: Environment – Compatibility
89 levels in industrial plants for low-frequency conducted disturbances*

90 IEC 61800-9-2, *Adjustable speed electrical power drive systems – Part 9-2: Ecodesign for
91 power drive systems, motor starters, power electronics and their driven applications – Energy
92 efficiency indicators for power drive systems and motor starters*

93 **3 Terms and definitions**

94 For the purposes of this document, the terms and definitions given in IEC 60034-1, IEC 60034-
95 2-1 as well as the following apply.

96 ISO and IEC maintain terminological databases for use in standardization at the following
97 addresses:

- 98 • IEC Electropedia: available at <http://www.electropedia.org/>
- 99 • ISO Online browsing platform: available at <http://www.iso.org/obp>

100 3.1

101 **additional high frequency losses**

102 additional high frequency losses are produced in the motor by the non-sinusoidal voltage and
103 current waveforms generated by the converter and are in addition to the losses of iron, friction
104 and windage, rotor winding, stator winding and additional load loss (fundamental losses)

105 3.2

106 **constant flux range**

107 speed range from standstill up to the highest speed where the motor can be supplied with a
108 voltage that changes in proportion to the speed so that the magnetic flux remains constant
109 (constant ratio U/f) for induction motors and according to the MTPA (maximum torque per
110 ampere) for synchronous motors. Within the constant flux range, the maximum motor torque is
111 constant (constant torque range), if constant flux control is used.

112 3.3

113 **fundamental losses**

114 fundamental losses in the motor can be segregated into five different components: iron losses
115 (varying with motor frequency and applied fundamental voltage), friction and windage losses
116 (varying with motor speed), rotor winding losses, stator winding losses and additional load
117 losses (all three varying with motor current). Fundamental losses are the losses of a motor
118 running with application of rated voltage at fundamental frequency that does not contain any
119 higher frequencies.

120 3.4

121 **motor losses with converter supply**

122 if powered by a converter, motor losses are a combination of losses caused by fundamental
123 frequency and losses caused by the converter high frequencies

124 3.5

125 **multi-level voltage source converter**

126 a frequency converter topology, where the output voltage (phase-to-ground) is switched in three
127 or more steps or levels up to the maximum possible output value of voltage in both plus and
128 minus

129 3.6 **switching event**

130 an operation sequence of one semiconductor with switching once on and switching once off

131 3.7

132 **switching frequency**

133 number of switching events of one semiconductor within one second. It determines, together
134 with the selected pulse pattern and the converter topology, the lowest frequency of non-
135 controllable high frequencies or inter-harmonics at the IPC (in-plant point of coupling) or the
136 motor

137 3.8

138 **thermal equilibrium**

139 steady state temperature level of a motor which is reached, if the rate of change of temperature
140 is 1 K or less per half hour

141 **3.9**
 142 **two-level voltage source converter**
 143 a frequency converter topology, where the output voltage (phase-to-ground) is switched in one
 144 step or level up to the maximum possible output voltage

145 Note For a two-level converter, the pulse frequency measured phase to phase is two times the switching frequency
 146 defined in 3.5 in case of continuous modulation and about 1,33 times the switching frequency defined in 3.5 in case
 147 of discontinuous modulation.

148 **4 Symbols and abbreviated terms**

| | | |
|-----|--------------------|---|
| 149 | c_{BH} | Loss separation coefficient for friction and windage losses and hysteresis losses |
| 150 | c_{Con} | Winding connection coefficient |
| 151 | c_{fe} | Loss separation coefficient for hysteresis losses and eddy current losses |
| 152 | c_{LL} | Loss separation coefficient for additional load losses |
| 153 | c_{Volt} | Voltage coefficient |
| 154 | c_{WHf} | Loss separation coefficient for winding losses and high frequency losses |
| 155 | f | Frequency, Hz |
| 156 | f_{Mot} | Fundamental motor frequency, Hz |
| 157 | f_N | Rated motor frequency, Hz |
| 158 | f_{sw} | Switching frequency, Hz |
| 159 | I_0 | No-load current, A |
| 160 | I_N | Rated current, A |
| 161 | MTPA | Maximum torque per ampere control applied to synchronous motors |
| 162 | n | Speed, s ⁻¹ |
| 163 | n_N | Rated speed, s ⁻¹ |
| 164 | n_{ref} | Reference speed, s ⁻¹ |
| 165 | n_{FW} | Relative speed at which field weakening range starts, |
| 166 | P | Power, W |
| 167 | P_{Ccon} | Constant losses if supplied by a converter, W |
| 168 | P_{Csin} | Constant losses at sinusoidal supply according to IEC 60034-2-1, W |
| 169 | PDS | Power drive system |
| 170 | P_{LHL} | Additional high frequency loss due to converter supply, W |
| 171 | P_N | Rated power, W |
| 172 | P_{ref} | Reference power, W |
| 173 | P_{1C} | Motor input power if supplied by a converter, W |
| 174 | $P_{1_60034-2-1}$ | Motor input power at sinusoidal supply according to IEC 60034-2-1, W |
| 175 | P_{2C} | Motor output power if supplied by a converter, W |
| 176 | $P_{2_60034-2-1}$ | Motor output power at sinusoidal supply according to IEC 60034-2-1, W |
| 177 | PWM | Pulse width modulation |
| 178 | T | Motor torque, Nm |
| 179 | T_C | Motor torque if supplied by a converter, Nm |