



SLOVENSKI STANDARD
oSIST prEN IEC 60034-2-2:2023
01-januar-2023

Električni rotacijski stroji - 2-2. del: Posebne metode za ugotavljanje posameznih izgub velikih strojev s preskušanjem - Dodatek k IEC 60034-2-1

Rotating electrical machines - Part 2-2: Specific methods for determining separate losses of large machines from tests - Supplement to IEC 60034-2-1

Drehende elektrische Maschinen - Teil 2-2: Besondere Verfahren zur Bestimmung der Einzelverluste großer elektrischer Maschinen aus Prüfungen - Ergänzung zu IEC 60034-2-1

Machines électriques tournantes - Partie 2-2: Méthodes spécifiques pour déterminer les pertes séparées des machines de grande taille à partir d'essais - Complément à l'IEC 60034-2-1

Ta slovenski standard je istoveten z: prEN IEC 60034-2-2:2022

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SECRETARIAT:

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SECRETARY:

Mr Charles Whitlock

OF INTEREST TO THE FOLLOWING COMMITTEES:

PROPOSED HORIZONTAL STANDARD:

Other TC/SCs are requested to indicate their interest, if any, in this CDV to the secretary.

FUNCTIONS CONCERNED:

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TITLE:

Rotating electrical machines – Part 2-2: Specific methods for determining separate losses of large machines from tests – Supplement to IEC 60034-2-1

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

ROTATING ELECTRICAL MACHINES –

**Part 2-2: Specific methods for determining
separate losses of large machines from tests –
Supplement to IEC 60034-2-1**

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International Standard IEC 60034-2-2 has been prepared by IEC technical committee 2: Rotating machinery.

The text of this standard is based on the following documents:

FDIS	Report on voting

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

NOTE A table of cross-references of all IEC TC 2 publications can be found in the IEC TC 2 dashboard on the IEC website.

The committee has decided that the contents of this amendment and the base publication will remain unchanged until the stability date indicated on the IEC web site under "http://webstore.iec.ch" in the data related to the specific publication. At this date, the publication will be

- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

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1 **ROTATING ELECTRICAL MACHINES –**
2
3 **Part 2-2: Specific methods for determining**
4 **separate losses of large machines from tests –**
5 **Supplement to IEC 60034-2-1**
6
7
8

9 **1 Scope**

10 This part of IEC 60034 applies to large rotating electrical machines and establishes additional
11 methods of determining separate losses and to define an efficiency supplementing
12 IEC 60034-2-1. These methods apply when full-load testing is not practical and result in a
13 greater uncertainty.

14 NOTE In situ testing according to the calorimetric method for full-load conditions is recognized.

15 The specific methods described are:

- 16 – Calibrated-machine method.
- 17 – Retardation method.
- 18 – Calorimetric method.
- 19 – Summation of losses for permanent magnet excited synchronous machines.

20 **2 Normative references**

21 The following referenced documents are indispensable for the application of this document.
22 For dated references, only the edition cited applies. For undated references, the latest edition
23 of the referenced document (including any amendments) applies.

24 IEC 60034-1, *Rotating electrical machines – Part 1: Rating and performance*

25 IEC 60034-2-1, *Rotating electrical machines – Part 2-1: Standard methods for determining*
26 *losses and efficiency from tests (excluding machines for traction vehicles)*

27 IEC 60034-4-1:2018, *Rotating electrical machines – Part 4-1: Methods for determining*
28 *synchronous machine quantities from tests*

29 **3 Terms and definitions**

30 For the purposes of this document, the terms and definitions given in IEC 60034-1 and
31 IEC 60034-2-1 apply, as well as the following.

32 **3.1**

33 **calibrated machine**

34 machine whose mechanical power input/output is determined, with low uncertainty, using
35 measured electrical output/input values according to a defined test procedure

36 **3.2**

37 **calibrated-machine method**

38 method in which the mechanical input/output to/from an electrical machine under test is
39 determined from the measurement of the electrical input/output of a calibrated machine
40 mechanically coupled to the test machine

41 **3.3**42 **retardation method**

43 method in which the separate losses in a machine under test are deduced from the
44 measurements of the deceleration rate of its rotating components when only these losses are
45 present

46 **3.4**47 **calorimetric method**

48 method in which the losses in a machine are deduced from the measurements of the heat
49 generated by them

50 **3.5**51 **thermal equilibrium**

52 the state reached when the temperature rises of the several parts of the machine do not vary
53 by more than rate of change 1 K per half hour

54 [IEV 411-51-08]

55 **4 Symbols and abbreviations**56 **4.1 Symbols**

57	A	is an area, m^2 ,
58	C	is the retardation constant, $kg\ m^2\ s^{-2}$,
59	c_p	is the specific heat capacity of the cooling medium, $J/(kg\ K)$,
60	h	is the coefficient of heat transfer, $W/(m^2\ K)$,
61	J	is the moment of inertia, $kg\ m^2$,
62	n	is the operating speed, s^{-1} ,
63	P_1	is the input power, W ,
64	P_{1E}	is the excitation power supplied by a separate source, W ,
65	P_2	is the output power, W ,
66	P_a	is the I^2R armature-winding losses (interpole, compensation and series field 67 winding loss in case of d.c. machines), W ,
68	P_b	is the brush losses, W ,
69	P_c	is the constant losses, W ,
70	P_e	is the excitation circuit losses, W ,
71	P_{Ed}	is the exciter losses, W ,
72	P_{el}	is the electrical power, excluding excitation, W ,
73	P_f	is the excitation (field winding) losses, W ,
74	P_{fe}	is the iron losses, W ,
75	P_{fw}	is the friction and windage losses, W ,
76	P_k	is the short-circuit losses, W ,
77	P_{LL}	is the additional load losses, W ,
78	P_{mech}	is the mechanical power, W ,
79	P_r	is the I^2R rotor winding losses, W ,
80	P_s	is the stator I^2R winding losses, W ,
81	P_T	is the total losses, W ,
82	Q	is the volume rate of flow of the cooling medium, m^3/s ,
83	t	is the time, s ,

84	v	is the exit velocity of cooling medium, m/s,
85	Δp	is the difference between the static pressure in the intake nozzle and ambient
86		pressure, N/m ² ,
87	$\Delta\theta$	is the temperature rise of the cooling medium, or the temperature difference
88		between the machine reference surface and the external ambient temperature, K,
89	δ	is the per unit deviation of rotational speed from rated speed,
90	ρ	is the density of the cooling medium, kg/m ³ ,
91	θ	is the temperature, °C.

92 4.2 Additional subscripts

93	c	for the cooling circuit,
94	E	for exciter,
95	ers	for outside reference surface,
96	i	for inner voltage
97	irs	for inside reference surface,
98	rs	for the reference surface,
99	RR	for test with rotor removed,
100	t	test,
101	0	no-load,
102	1	input,
103	2	output.

104 5 Basic requirements

105 5.1 Direct and indirect efficiency determination

106 Tests can be grouped in the following categories.

107 5.1.1 Direct

108 Input-output measurements on a single machine are considered to be direct. This involves the
109 measurement of electrical or mechanical power into, and mechanical or electrical power out of
110 a machine.

111 5.1.2 Indirect

112 Measurements of the separate losses in a machine under a particular condition are
113 considered to be indirect. This is not usually the total loss but comprises certain loss
114 components. The method may, however, be used to calculate the total loss or to calculate a
115 loss component.

116 The determination of total loss shall be carried out by one of the following methods:

- 117 – direct measurement of total losses;
- 118 – summation of separate losses.

119 NOTE The methods for determining the efficiency of machines are based on a number of assumptions. Therefore,
120 it is not possible to make a comparison between the values of efficiency obtained by different methods.

121 5.2 Uncertainty

122 Uncertainty as used in this standard is the uncertainty of determining a true efficiency. It
123 reflects variations in the test procedure and the test equipment.

124 Although uncertainty should be expressed as a numerical value, such a requirement needs
125 sufficient testing to determine representative and comparative values.
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127 **6 Additional test methods for the determination of the efficiency of large**
 128 **machines**

129 **6.1 General**

130 For the determination of performance when machine load and/or size exceed test capabilities
 131 (described in IEC 60034-2-1), the following test methods may be used.

132 **Table 1 – Additional methods for large machines**

Ref	Method	Description	Subclause	Application	Required facility
2-2-A	Calibrated Machine	Loss measurement via calibrated machine	6.2	All types of machines	Calibrated machine
2-2-B	Retardation Method	Loss measurement by retardation	6.3	Applicable for factory and on-site measurements	
2-2-C	Calorimetric Method	Loss measurement in the primary and secondary coolant	6.4	Applicable for factory and on-site measurements	

133 NOTE These methods are generally applicable to large machines where the facility cost for other methods is not
 134 economical.

135 Losses relative to machine load (with lowest uncertainty) are best determined from actual
 136 measurements. For example: measurements of current, resistance, etc. under full-load
 137 operation.

138 When this is not possible, these values shall be obtained from calculation of the parameters
 139 during the design stage.

140 Determination of losses not itemized in this part may be found in IEC 60034-2-1.

141 **6.1.1 Efficiency**

142 Efficiency is:

143
$$\eta = \frac{P_1 + P_{1E} - P_T}{P_1 + P_{1E}} = \frac{P_2}{P_2 + P_T}$$

144 where

145 P_1 is the input power excluding excitation power from a separate source;

146 P_2 is the output power;

147 P_{1E} is the excitation power supplied by a separate source;

148 P_T is the total loss

149 NOTE 1 Input power P_1 and output power P_2 are as follows:

150 in motor operation: $P_1 = P_{el}$; $P_2 = P_{mech}$;

151 in generator operation: $P_1 = P_{mech}$; $P_2 = P_{el}$.

152 NOTE 2 P_T includes the excitation power P_e of the machine where applicable.