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Steel — Conversion of elongation values — Part I : Carbon and low alloy steels

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FOREWORD

ISO (the International Organization for Standardization) is a worldwide federation of national standards institutes (ISO Member Bodies). The work of developing International Standards is carried out through ISO Technical Committees. Every Member Body interested in a subject for which a Technical Committee has been set up has the right to be represented on that Committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work.

Draft International Standards adopted by the Technical Committees are circulated to the Member Bodies for approval before their acceptance as International Standards by the ISO Council.

International Standard ISO 2566/1 was drawn up by Technical Committee ISO/TC 17, *Steel*, and circulated to the Member Bodies in March 1972.

It has been approved by the Member Bodies of the following countries :

| | | |
|---------------------|-------------|-----------------------|
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| Canada | Israel | Spain |
| Czechoslovakia | Italy | Sweden |
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The Member Body of the following country expressed disapproval of the document on technical grounds :

Belgium

Steel — Conversion of elongation values — Part I : Carbon and low alloy steels

0 INTRODUCTION

Several different gauge lengths are commonly in use for the determination of percentage elongation of steels in tensile testing. In metric units, gauge lengths of 50, 100 and 200 mm are used, while in inch units, gauge lengths of 2, 4 and 8 in are used. Proportional gauge lengths of $k\sqrt{S_o}$ are also used for flat and round test pieces, where k may be one of a number of values, i.e. 4 – 5,65 – 8,16 – 11,3.

Discussion within ISO Technical Committee 17, *Steel*, has resulted in the adoption of $5,65\sqrt{S_o}$ as the internationally preferred proportional gauge length.

Arising from this agreement and the existence of specifications stipulating minimum percentage elongations on different gauge lengths, a growing need has been evident for an International Standard which could be used to convert test results into values based on the different gauge lengths. This document accordingly includes tables of conversion factors, tables of actual conversions for some of the more commonly used gauge lengths and elongation values, and charts which may also be used for such conversions. When using these conversions, however, note should be taken of the limitations on their applicability as stated in section 1.

While, as indicated, the conversions are considered to be reliable within the stated limitations and may generally be used for acceptance purposes, because of the various factors influencing the determination of percentage elongations, in cases of dispute the elongation shall be determined on the gauge length stated in the relevant material specification.

1 SCOPE AND FIELD OF APPLICATION

This International Standard specifies a method of converting percentage elongations after fracture obtained on various proportional and non-proportional gauge lengths to other gauge lengths.

The formula (see section 4) on which the conversions are based is considered to be reliable when applied to carbon, carbon manganese, molybdenum and chromium molybdenum steels within the tensile strength range 300 to 700 N/mm² and in the hot-rolled, hot-rolled and normalized or annealed condition, with or without tempering.

These conversions are not applicable to

- cold reduced steels;
- quenched and tempered steels;
- austenitic steels;

nor should they be used where the gauge length exceeds $25\sqrt{S_o}$ or the width to thickness ratio of the test piece exceeds 20.

2 SYMBOLS

In this International Standard the following symbols are used:

| Symbol | Description |
|--------|---|
| A | Percentage elongation on gauge length L_o after fracture, obtained on test. |
| A_r | Percentage elongation on a different gauge length, required by conversion. |
| d | Diameter of test piece. |
| L_o | Original gauge length. |
| S_o | Original cross-sectional area of test piece. |

3 DEFINITIONS

For the purposes of this International Standard, the following definitions apply :

3.1 gauge length : Any length of the parallel portion of the test piece used for measurement of strain. The term is hereafter used in this International Standard to denote the original gauge length L_o marked on the test piece for the determination of percentage elongation after fracture (A).

3.2 proportional gauge length : A gauge length having a specified relation to the square root of the cross-sectional area, for example, $5,65\sqrt{S_o}$.

3.3 non-proportional gauge length : A gauge length not specifically related to the cross-sectional area of the test piece, usually expressed as a given dimension, for example 50 mm or 2 in.

4 BASIC FORMULA

The data contained in this International Standard are based on the "Oliver" formula¹⁾ which is now widely used for such elongation conversions.

The Oliver formula can, in a simplified form, be expressed as

$$A_r = 1,74A \left(\frac{\sqrt{S_o}}{L_o} \right)^{0,4}$$

where

A_r is the required elongation on gauge length L_o ;

A is the elongation on a gauge length of $4\sqrt{S_o}$.

This formula gives a direct conversion of elongation on $4\sqrt{S_o}$ to the equivalent for a test piece of cross-sectional area S_o , and a gauge length L_o . Expressed in terms of $5,65\sqrt{S_o}$, which is now regarded as the internationally accepted standard gauge length, it becomes

$$A_r = 2A \left(\frac{\sqrt{S_o}}{L_o} \right)^{0,4}$$

where A is the elongation on a gauge length of $5,65\sqrt{S_o}$.

Tables 1 to 10 and Charts 1, 2 and 3 have been prepared on the basis of the above formulae.

5 CONVERSION FROM ONE PROPORTIONAL GAUGE LENGTH TO ANOTHER PROPORTIONAL GAUGE LENGTH

Simple multiplying factors based on the formula are used for such conversions, and the relationships between a number of the more widely used proportional gauge lengths are given in Table 1. Detailed conversions of elongations obtained on $4\sqrt{S_o}$ to $5,65\sqrt{S_o}$ are given in Table 4.

6 CONVERSION FROM ONE NON-PROPORTIONAL GAUGE LENGTH TO ANOTHER NON-PROPORTIONAL GAUGE LENGTH FOR TEST PIECES OF EQUAL CROSS-SECTIONAL AREA

The conversion of elongation values of different fixed gauge lengths on test pieces of equal cross-sectional area are also made by simple factors. Conversion factors for metric gauge lengths of 50, 100, 150, 200 and 250 mm, and for inch gauge lengths of 2, 4, 6, 8 and 10 in are given in Table 2.

7 CONVERSION FROM A PROPORTIONAL GAUGE LENGTH TO A NON-PROPORTIONAL GAUGE LENGTH

The conversion factors are variable according to the cross-sectional area of the non-proportional test piece. Table 3 gives the multiplying factors for conversion from elongation on $5,65\sqrt{S_o}$ to the equivalent on fixed metric gauge lengths of 50, 100, 150 and 200 mm, and fixed inch

gauge lengths of 2, 4, 6 and 8 in for a range of cross-sectional areas. For conversions in the reverse direction, i.e. elongation on a fixed gauge length to the equivalent on $5,65\sqrt{S_o}$, the reciprocal of the factor is used.

Examples :

a) Elongation of 20 % on $5,65\sqrt{S_o}$ is equivalent to $20 \times 1,139 = 22,78$ % on a 25 mm wide test piece of 6 mm thickness with a 50 mm gauge length (see Table 3).

b) Elongation of 25 % on a 40 mm X 10 mm test piece of 200 mm gauge length is equivalent to $25 \times 1/0,796 = 31,4$ % on $5,65\sqrt{S_o}$ (see Table 3).

From the examples shown it will be seen that conversions involving other proportional gauge lengths can be obtained by prior or subsequent use of the factors shown in Table 1.

Tables 5, 6 and 7 can be used to obtain some of these conversions.

Similarly, Tables 8, 9 and 10 can be used for conversions to $4\sqrt{S_o}$.

8 CONVERSION FROM A NON-PROPORTIONAL GAUGE LENGTH TO ANOTHER NON-PROPORTIONAL GAUGE LENGTH FOR TEST PIECES OF DIFFERENT CROSS-SECTIONAL AREAS

It is preferable for this calculation to be made in two stages with an initial conversion to $5,65\sqrt{S_o}$.

Example :

Elongation of 24 % on 200 mm for a 40 mm X 15 mm test piece in terms of equivalent on a 30 mm X 10 mm test piece with gauge lengths equal to 200 mm, 100 mm and 50 mm.

$24 \times 1/0,863 = 27,8$ % on $5,65\sqrt{S_o}$ (see Table 3).

and $27,8 \times 0,752 = 20,8$ % on 30 mm X 10 mm with 200 mm gauge length.

$27,8 \times 0,992 = 27,5$ % on 30 mm X 10 mm with 100 mm gauge length.

$27,8 \times 1,309 = 36,1$ % on 30 mm X 10 mm with 50 mm gauge length.

Elongation on other proportional gauge lengths can be obtained by using the factors given in Table 1.

9 USE OF CHARTS 1, 2 AND 3

9.1 Charts 1, 2 and 3 may be used as an alternative quick method to obtain elongation conversions.

1) D.A. Oliver, Proc. Inst. Mech. E., Vol. 11 (1928), page 827.

9.2 Charts 1 and 2 may be used for conversions between $5,65\sqrt{S_0}$ or $4\sqrt{S_0}$ respectively and 50 mm (2 in) and 200 mm (8 in) gauge lengths.

Example :

To find the equivalent elongation on $5,65\sqrt{S_0}$ and $4\sqrt{S_0}$ to an elongation of 21 % on a 200 mm (8 in) gauge length of a 25 mm (1 in) X 12,5 mm (0.5 in) test piece.

Cross-sectional area = 312,5 mm² (0.5 in²).

The intersection of this ordinate with the abscissa representing an elongation of 21 % on a 200 mm (8 in) gauge length lies on the sloping line representing an elongation of 28 % on $5,65\sqrt{S_0}$ on Chart 1 and at a position relative to the sloping lines on Chart 2 approximating to an elongation of 32,2 on $4\sqrt{S_0}$.

Abscissae representing elongations on a 50 mm (2 in) gauge length appear on the left-hand side of the charts.

9.3 Chart 3 may be used for the calculation of all elongation conversions.

The Oliver formula may be re-written as

$$A_2 = A_1 \left(\frac{K_1}{K_2} \right)^{0,4} = \lambda_{1,2} \times A_1$$

where K_1 and K_2 designate the proportionality ratios of any two test pieces.

$$\left[K_1 = \frac{L_1}{\sqrt{S_1}} \text{ and } K_2 = \frac{L_2}{\sqrt{S_2}} \right]$$

Chart 3 shows the values of $\lambda_{1,2} = \left(\frac{K_1}{K_2} \right)^{0,4}$

To use Chart 3 it is necessary to perform the following operations :

- a) calculate the values of proportionality $K_1 = \frac{L_1}{\sqrt{S_1}}$, and $K_2 = \frac{L_2}{\sqrt{S_2}}$, for two test pieces;
- b) read graphically the coefficient $\lambda_{1,2} = \left(\frac{K_1}{K_2} \right)^{0,4}$;
- c) the elongation obtained is $A_2 = \lambda_{1,2} \times A_1$.

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TABLE 1 – Conversion factors : Proportional gauge lengths

| Conversion from | Factor for conversion to | | | | | | |
|------------------|--------------------------|------------------|------------------|------------------|-------|-------|-------|
| | $4\sqrt{S_0}$ | $5,65\sqrt{S_0}$ | $8,16\sqrt{S_0}$ | $11,3\sqrt{S_0}$ | $4d$ | $5d$ | $8d$ |
| $4\sqrt{S_0}$ | 1,000 | 0,870 | 0,752 | 0,661 | 0,953 | 0,870 | 0,721 |
| $5,65\sqrt{S_0}$ | 1,149 | 1,000 | 0,863 | 0,759 | 1,093 | 1,000 | 0,828 |
| $8,16\sqrt{S_0}$ | 1,330 | 1,158 | 1,000 | 0,879 | 1,268 | 1,158 | 0,960 |
| $11,3\sqrt{S_0}$ | 1,514 | 1,317 | 1,137 | 1,000 | 1,443 | 1,317 | 1,091 |
| $4d$ | 1,050 | 0,916 | 0,790 | 0,694 | 1,000 | 0,916 | 0,758 |
| $5d$ | 1,149 | 1,000 | 0,863 | 0,759 | 1,093 | 1,000 | 0,828 |
| $8d$ | 1,389 | 1,207 | 1,042 | 0,918 | 1,319 | 1,207 | 1,000 |

TABLE 3 – Conversion factors from $5,65\sqrt{S_0}$ to non-proportional gauge lengths (See also Chart 1)

Factors shown under "Non-proportional gauge lengths" give the value of

$$2\left(\frac{\sqrt{S_0}}{L}\right)^{0,4}$$

To convert from values on a gauge length of $5,65\sqrt{S_0}$ to a non-proportional gauge length, multiply by the appropriate factor.

To convert from values on a non-proportional gauge length to $5,65\sqrt{S_0}$, divide by the appropriate factor.

a) Metric units

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|--------|--------|-------|
| | 200 mm | 150 mm | 100 mm | 50 mm |
| mm ² | | | | |
| 5 | 0,331 | 0,372 | 0,437 | 0,577 |
| 10 | 0,381 | 0,427 | 0,502 | 0,653 |
| 15 | 0,413 | 0,463 | 0,545 | 0,719 |
| 20 | 0,437 | 0,491 | 0,577 | 0,761 |
| 25 | 0,457 | 0,513 | 0,603 | 0,796 |
| 30 | 0,474 | 0,532 | 0,626 | 0,826 |
| 35 | 0,489 | 0,549 | 0,645 | 0,852 |
| 40 | 0,502 | 0,564 | 0,663 | 0,875 |
| 45 | 0,514 | 0,577 | 0,679 | 0,896 |
| 50 | 0,525 | 0,589 | 0,693 | 0,915 |
| 55 | 0,535 | 0,601 | 0,706 | 0,932 |
| 60 | 0,545 | 0,611 | 0,719 | 0,949 |
| 70 | 0,562 | 0,630 | 0,741 | 0,978 |
| 80 | 0,577 | 0,647 | 0,761 | 1,005 |
| 90 | 0,591 | 0,663 | 0,780 | 1,029 |
| 100 | 0,603 | 0,677 | 0,796 | 1,051 |
| 110 | 0,615 | 0,690 | 0,812 | 1,071 |
| 120 | 0,626 | 0,702 | 0,826 | 1,090 |
| 130 | 0,636 | 0,713 | 0,839 | 1,107 |
| 140 | 0,645 | 0,724 | 0,852 | 1,124 |
| 150 | 0,654 | 0,734 | 0,863 | 1,139 |
| 160 | 0,663 | 0,744 | 0,875 | 1,154 |
| 170 | 0,671 | 0,753 | 0,885 | 1,168 |
| 180 | 0,679 | 0,761 | 0,896 | 1,182 |
| 190 | 0,686 | 0,770 | 0,905 | 1,195 |
| 200 | 0,693 | 0,778 | 0,915 | 1,207 |
| 210 | 0,700 | 0,785 | 0,924 | 1,219 |
| 220 | 0,706 | 0,793 | 0,932 | 1,230 |
| 230 | 0,713 | 0,800 | 0,941 | 1,241 |
| 240 | 0,719 | 0,807 | 0,949 | 1,252 |
| 250 | 0,725 | 0,813 | 0,956 | 1,262 |
| 260 | 0,730 | 0,820 | 0,964 | 1,272 |
| 270 | 0,736 | 0,826 | 0,971 | 1,281 |
| 280 | 0,741 | 0,832 | 0,978 | 1,291 |
| 290 | 0,747 | 0,838 | 0,985 | 1,300 |

TABLE 2 – Conversion factors : Non-proportional gauge lengths (Provided cross-sectional areas are the same)

a) Metric units

| Conversion from | Factor for conversion to | | | | |
|-----------------|--------------------------|--------|--------|--------|--------|
| | 50 mm | 100 mm | 150 mm | 200 mm | 250 mm |
| 50 mm | 1,000 | 0,758 | 0,644 | 0,574 | 0,525 |
| 100 mm | 1,320 | 1,000 | 0,850 | 0,758 | 0,693 |
| 150 mm | 1,552 | 1,176 | 1,000 | 0,891 | 0,815 |
| 200 mm | 1,741 | 1,320 | 1,122 | 1,000 | 0,915 |
| 250 mm | 1,904 | 1,443 | 1,227 | 1,093 | 1,000 |

b) Inch units

| Conversion from | Factor for conversion to | | | | |
|-----------------|--------------------------|-------|-------|-------|-------|
| | 2 in | 4 in | 6 in | 8 in | 10 in |
| 2 in | 1,000 | 0,758 | 0,644 | 0,574 | 0,525 |
| 4 in | 1,320 | 1,000 | 0,850 | 0,758 | 0,693 |
| 6 in | 1,552 | 1,176 | 1,000 | 0,891 | 0,815 |
| 8 in | 1,741 | 1,320 | 1,122 | 1,000 | 0,915 |
| 10 in | 1,904 | 1,443 | 1,227 | 1,093 | 1,000 |

TABLE 3 (continued)

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|--------|--------|-------|
| | 200 mm | 150 mm | 100 mm | 50 mm |
| mm ² | | | | |
| 300 | 0,752 | 0,843 | 0,992 | 1,309 |
| 310 | 0,757 | 0,849 | 0,998 | 1,317 |
| 320 | 0,761 | 0,854 | 1,005 | 1,326 |
| 330 | 0,766 | 0,860 | 1,011 | 1,334 |
| 340 | 0,771 | 0,865 | 1,017 | 1,342 |
| 350 | 0,775 | 0,870 | 1,023 | 1,350 |
| 360 | 0,780 | 0,875 | 1,029 | 1,357 |
| 370 | 0,784 | 0,879 | 1,034 | 1,365 |
| 380 | 0,788 | 0,884 | 1,040 | 1,372 |
| 390 | 0,792 | 0,889 | 1,045 | 1,379 |
| 400 | 0,796 | 0,893 | 1,051 | 1,386 |
| 410 | 0,800 | 0,898 | 1,056 | 1,393 |
| 420 | 0,804 | 0,902 | 1,061 | 1,400 |
| 430 | 0,808 | 0,906 | 1,066 | 1,406 |
| 440 | 0,812 | 0,911 | 1,071 | 1,413 |
| 450 | 0,815 | 0,915 | 1,076 | 1,419 |
| 460 | 0,819 | 0,919 | 1,080 | 1,426 |
| 470 | 0,822 | 0,923 | 1,085 | 1,432 |
| 480 | 0,826 | 0,926 | 1,090 | 1,438 |
| 490 | 0,829 | 0,930 | 1,094 | 1,444 |
| 500 | 0,833 | 0,934 | 1,099 | 1,450 |
| 550 | 0,849 | 0,952 | 1,120 | 1,477 |
| 600 | 0,863 | 0,969 | 1,139 | 1,503 |
| 650 | 0,877 | 0,984 | 1,158 | 1,528 |
| 700 | 0,891 | 0,999 | 1,175 | 1,550 |
| 750 | 0,903 | 1,013 | 1,191 | 1,572 |
| 800 | 0,915 | 1,026 | 1,207 | 1,592 |
| 850 | 0,926 | 1,039 | 1,222 | 1,612 |
| 900 | 0,936 | 1,051 | 1,236 | 1,630 |
| 950 | 0,947 | 1,062 | 1,249 | 1,648 |
| 1 000 | 0,956 | 1,073 | 1,262 | 1,665 |
| 1 050 | 0,966 | 1,084 | 1,274 | 1,681 |
| 1 100 | 0,975 | 1,094 | 1,286 | 1,697 |
| 1 150 | 0,983 | 1,103 | 1,298 | 1,712 |
| 1 200 | 0,992 | 1,113 | 1,309 | 1,727 |
| 1 250 | 1,000 | 1,122 | 1,320 | 1,741 |
| 1 300 | 1,008 | 1,131 | 1,330 | 1,755 |
| 1 350 | 1,016 | 1,139 | 1,340 | 1,768 |
| 1 400 | 1,023 | 1,148 | 1,350 | 1,781 |
| 1 450 | 1,030 | 1,156 | 1,359 | 1,794 |
| 1 500 | 1,037 | 1,164 | 1,369 | 1,806 |
| 1 550 | 1,044 | 1,171 | 1,378 | 1,818 |
| 1 600 | 1,051 | 1,179 | 1,386 | 1,829 |
| 1 650 | 1,057 | 1,186 | 1,395 | 1,841 |
| 1 700 | 1,063 | 1,193 | 1,403 | 1,852 |
| 1 750 | 1,070 | 1,200 | 1,411 | 1,862 |
| 1 800 | 1,076 | 1,207 | 1,419 | 1,873 |
| 1 850 | 1,082 | 1,213 | 1,427 | 1,883 |
| 1 900 | 1,087 | 1,220 | 1,435 | 1,893 |
| 1 950 | 1,093 | 1,226 | 1,442 | 1,903 |

TABLE 3 (continued)

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|--------|--------|-------|
| | 200 mm | 150 mm | 100 mm | 50 mm |
| mm ² | | | | |
| 2 000 | 1,099 | 1,233 | 1,450 | 1,913 |
| 2 050 | 1,104 | 1,239 | 1,457 | 1,922 |
| 2 100 | 1,109 | 1,245 | 1,464 | 1,931 |
| 2 150 | 1,115 | 1,250 | 1,471 | 1,941 |
| 2 200 | 1,120 | 1,256 | 1,477 | 1,950 |
| 2 250 | 1,125 | 1,262 | 1,484 | 1,958 |
| 2 300 | 1,130 | 1,267 | 1,491 | 1,967 |
| 2 350 | 1,135 | 1,273 | 1,497 | 1,975 |
| 2 400 | 1,139 | 1,278 | 1,503 | 1,984 |
| 2 450 | 1,144 | 1,284 | 1,510 | 1,992 |
| 2 500 | 1,149 | 1,289 | 1,516 | 2,000 |
| 2 550 | 1,153 | 1,294 | 1,522 | 2,008 |
| 2 600 | 1,158 | 1,299 | 1,528 | 2,016 |
| 2 650 | 1,162 | 1,304 | 1,533 | 2,023 |
| 2 700 | 1,167 | 1,309 | 1,539 | 2,031 |
| 2 750 | 1,171 | 1,314 | 1,545 | 2,038 |
| 2 800 | 1,175 | 1,318 | 1,550 | 2,046 |
| 2 850 | 1,179 | 1,323 | 1,556 | 2,053 |
| 2 900 | 1,183 | 1,328 | 1,561 | 2,060 |
| 2 950 | 1,187 | 1,332 | 1,567 | 2,067 |
| 3 000 | 1,191 | 1,337 | 1,572 | 2,074 |

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b) Inch units

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|-------|-------|-------|
| | 8 in | 6 in | 4 in | 2 in |
| in ² | | | | |
| 0.010 | 0.347 | 0.389 | 0.457 | 0.603 |
| 0.020 | 0.398 | 0.447 | 0.525 | 0.693 |
| 0.030 | 0.432 | 0.484 | 0.570 | 0.752 |
| 0.040 | 0.457 | 0.513 | 0.603 | 0.796 |
| 0.050 | 0.478 | 0.536 | 0.631 | 0.833 |
| 0.060 | 0.496 | 0.556 | 0.654 | 0.863 |
| 0.070 | 0.511 | 0.574 | 0.675 | 0.891 |
| 0.080 | 0.525 | 0.589 | 0.693 | 0.915 |
| 0.090 | 0.538 | 0.603 | 0.710 | 0.936 |
| 0.100 | 0.549 | 0.616 | 0.725 | 0.956 |
| 0.110 | 0.560 | 0.628 | 0.739 | 0.975 |
| 0.120 | 0.570 | 0.639 | 0.752 | 0.992 |
| 0.130 | 0.579 | 0.649 | 0.764 | 1.008 |
| 0.140 | 0.588 | 0.659 | 0.775 | 1.023 |
| 0.150 | 0.596 | 0.668 | 0.786 | 1.037 |
| 0.160 | 0.603 | 0.677 | 0.796 | 1.051 |
| 0.170 | 0.611 | 0.685 | 0.806 | 1.063 |
| 0.180 | 0.618 | 0.693 | 0.815 | 1.076 |
| 0.190 | 0.625 | 0.701 | 0.824 | 1.087 |
| 0.200 | 0.631 | 0.708 | 0.833 | 1.099 |

TABLE 3 (continued)

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|-------|-------|-------|
| | 8 in | 6 in | 4 in | 2 in |
| 0.210 | 0.637 | 0.715 | 0.841 | 1.109 |
| 0.220 | 0.643 | 0.722 | 0.849 | 1.120 |
| 0.230 | 0.649 | 0.728 | 0.856 | 1.130 |
| 0.240 | 0.654 | 0.734 | 0.863 | 1.139 |
| 0.250 | 0.660 | 0.740 | 0.871 | 1.149 |
| 0.260 | 0.665 | 0.746 | 0.877 | 1.158 |
| 0.270 | 0.670 | 0.752 | 0.884 | 1.167 |
| 0.280 | 0.675 | 0.757 | 0.891 | 1.175 |
| 0.290 | 0.680 | 0.763 | 0.897 | 1.183 |
| 0.300 | 0.684 | 0.768 | 0.903 | 1.191 |
| 0.310 | 0.689 | 0.773 | 0.909 | 1.199 |
| 0.320 | 0.693 | 0.778 | 0.915 | 1.207 |
| 0.330 | 0.697 | 0.782 | 0.920 | 1.214 |
| 0.340 | 0.702 | 0.787 | 0.926 | 1.222 |
| 0.350 | 0.706 | 0.792 | 0.931 | 1.229 |
| 0.360 | 0.710 | 0.796 | 0.936 | 1.236 |
| 0.370 | 0.714 | 0.801 | 0.942 | 1.242 |
| 0.380 | 0.717 | 0.805 | 0.947 | 1.249 |
| 0.390 | 0.721 | 0.809 | 0.952 | 1.256 |
| 0.400 | 0.725 | 0.813 | 0.956 | 1.262 |
| 0.410 | 0.728 | 0.817 | 0.961 | 1.268 |
| 0.420 | 0.732 | 0.821 | 0.966 | 1.274 |
| 0.430 | 0.735 | 0.825 | 0.970 | 1.280 |
| 0.440 | 0.739 | 0.829 | 0.975 | 1.286 |
| 0.450 | 0.742 | 0.833 | 0.979 | 1.292 |
| 0.460 | 0.745 | 0.836 | 0.983 | 1.298 |
| 0.470 | 0.749 | 0.840 | 0.988 | 1.303 |
| 0.480 | 0.752 | 0.843 | 0.992 | 1.309 |
| 0.490 | 0.755 | 0.847 | 0.996 | 1.314 |
| 0.500 | 0.758 | 0.850 | 1.000 | 1.320 |
| 0.550 | 0.772 | 0.867 | 1.019 | 1.345 |
| 0.600 | 0.786 | 0.882 | 1.037 | 1.369 |
| 0.650 | 0.799 | 0.896 | 1.054 | 1.391 |
| 0.700 | 0.811 | 0.909 | 1.070 | 1.411 |
| 0.750 | 0.822 | 0.922 | 1.084 | 1.431 |
| 0.800 | 0.833 | 0.934 | 1.099 | 1.450 |
| 0.850 | 0.843 | 0.945 | 1.112 | 1.467 |
| 0.900 | 0.852 | 0.956 | 1.125 | 1.484 |
| 0.950 | 0.862 | 0.967 | 1.137 | 1.500 |
| 1.000 | 0.871 | 0.977 | 1.149 | 1.516 |
| 1.050 | 0.879 | 0.986 | 1.160 | 1.531 |
| 1.100 | 0.887 | 0.996 | 1.171 | 1.545 |
| 1.150 | 0.895 | 1.004 | 1.181 | 1.559 |
| 1.200 | 0.903 | 1.013 | 1.191 | 1.572 |
| 1.250 | 0.910 | 1.021 | 1.201 | 1.585 |
| 1.300 | 0.917 | 1.029 | 1.211 | 1.597 |
| 1.350 | 0.924 | 1.037 | 1.220 | 1.609 |
| 1.400 | 0.931 | 1.045 | 1.229 | 1.621 |
| 1.450 | 0.938 | 1.052 | 1.237 | 1.633 |
| 1.500 | 0.944 | 1.059 | 1.246 | 1.644 |

TABLE 3 (concluded)

| Cross-sectional area of test piece | Factor for non-proportional gauge length of | | | |
|------------------------------------|---|-------|-------|-------|
| | 8 in | 6 in | 4 in | 2 in |
| 1.550 | 0.950 | 1.066 | 1.254 | 1.655 |
| 1.600 | 0.956 | 1.073 | 1.262 | 1.665 |
| 1.650 | 0.962 | 1.080 | 1.270 | 1.675 |
| 1.700 | 0.968 | 1.086 | 1.277 | 1.685 |
| 1.750 | 0.974 | 1.092 | 1.285 | 1.695 |
| 1.800 | 0.979 | 1.099 | 1.292 | 1.705 |
| 1.850 | 0.985 | 1.105 | 1.299 | 1.714 |
| 1.900 | 0.990 | 1.111 | 1.306 | 1.723 |
| 1.950 | 0.995 | 1.116 | 1.313 | 1.732 |
| 2.000 | 1.000 | 1.122 | 1.320 | 1.741 |
| 2.050 | 1.005 | 1.128 | 1.326 | 1.750 |
| 2.100 | 1.010 | 1.133 | 1.332 | 1.758 |
| 2.150 | 1.015 | 1.138 | 1.339 | 1.766 |
| 2.200 | 1.019 | 1.144 | 1.345 | 1.775 |
| 2.250 | 1.024 | 1.149 | 1.351 | 1.783 |
| 2.300 | 1.028 | 1.154 | 1.357 | 1.790 |
| 2.350 | 1.033 | 1.159 | 1.363 | 1.798 |
| 2.400 | 1.037 | 1.164 | 1.369 | 1.806 |
| 2.450 | 1.041 | 1.168 | 1.374 | 1.813 |
| 2.500 | 1.046 | 1.173 | 1.380 | 1.821 |
| 2.550 | 1.050 | 1.178 | 1.385 | 1.828 |
| 2.600 | 1.054 | 1.182 | 1.391 | 1.835 |
| 2.650 | 1.058 | 1.187 | 1.396 | 1.842 |
| 2.700 | 1.062 | 1.191 | 1.401 | 1.849 |
| 2.750 | 1.066 | 1.196 | 1.406 | 1.856 |
| 2.800 | 1.070 | 1.200 | 1.411 | 1.862 |
| 2.850 | 1.073 | 1.204 | 1.416 | 1.869 |
| 2.900 | 1.077 | 1.209 | 1.421 | 1.875 |
| 2.950 | 1.081 | 1.213 | 1.426 | 1.882 |
| 3.000 | 1.084 | 1.217 | 1.431 | 1.888 |
| 3.050 | 1.088 | 1.221 | 1.436 | 1.894 |
| 3.100 | 1.092 | 1.225 | 1.440 | 1.901 |
| 3.150 | 1.095 | 1.229 | 1.445 | 1.907 |
| 3.200 | 1.099 | 1.233 | 1.450 | 1.913 |
| 3.250 | 1.102 | 1.236 | 1.454 | 1.919 |
| 3.300 | 1.105 | 1.240 | 1.459 | 1.925 |
| 3.350 | 1.109 | 1.244 | 1.463 | 1.930 |
| 3.400 | 1.112 | 1.248 | 1.467 | 1.936 |
| 3.450 | 1.115 | 1.251 | 1.472 | 1.942 |
| 3.500 | 1.188 | 1.255 | 1.476 | 1.947 |
| 3.550 | 1.122 | 1.258 | 1.480 | 1.953 |
| 3.600 | 1.125 | 1.262 | 1.484 | 1.958 |
| 3.650 | 1.128 | 1.265 | 1.488 | 1.964 |
| 3.700 | 1.131 | 1.269 | 1.492 | 1.969 |
| 3.750 | 1.134 | 1.272 | 1.496 | 1.974 |
| 3.800 | 1.137 | 1.276 | 1.500 | 1.980 |
| 3.850 | 1.140 | 1.279 | 1.504 | 1.985 |
| 3.900 | 1.143 | 1.282 | 1.508 | 1.990 |
| 3.950 | 1.146 | 1.286 | 1.512 | 1.995 |
| 4.000 | 1.149 | 1.289 | 1.516 | 2.000 |

TABLE 4 – Elongation values on $5,65 \sqrt{S_0}$ corresponding to those obtained on $4 \sqrt{S_0}$ gauge length
(Factor 0,87; rounded to nearest whole number)

| Actual per cent elongation measured on $4 \sqrt{S_0}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|---|--|----|----|----|----|----|----|----|----|----|
| | Corresponding per cent elongation on $5,65 \sqrt{S_0}$ | | | | | | | | | |
| 10 | 9 | 10 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 |
| 20 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 23 | 24 | 25 |
| 30 | 26 | 27 | 28 | 29 | 30 | 30 | 31 | 32 | 33 | 34 |
| 40 | 35 | 36 | 37 | 37 | 38 | 39 | 40 | 41 | 42 | 43 |
| 50 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 50 | 51 |

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TABLE 5a) — Elongation values on $5,65\sqrt{S_0}$ corresponding to those obtained on 50 mm gauge length

(Rounded to the nearest whole number)

| Actual per cent elongation on 50 mm gauge length | Corresponding per cent elongation on $5,65\sqrt{S_0}$ gauge length if cross-sectional area in square millimetres is : | | | | | | | | | | | | | | | | | | | | | |
|--|---|----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|
| | 5 | 10 | 20 | 40 | 60 | 80 | 100 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1 000 | 1 200 | 1 500 | 2 000 | 2 500 |
| 18 | 31 | 27 | 24 | 21 | 19 | 18 | 17 | 16 | 15 | 14 | 14 | 13 | 12 | 12 | 12 | 11 | 11 | 11 | 10 | 10 | 9 | 9 |
| 19 | 33 | 29 | 25 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | 13 | 12 | 12 | 12 | 11 | 11 | 11 | 10 | 10 |
| 20 | 35 | 30 | 26 | 23 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 12 | 11 | 10 | 10 |
| 21 | 36 | 32 | 28 | 24 | 22 | 21 | 20 | 18 | 17 | 17 | 16 | 15 | 14 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 11 | 11 |
| 22 | 38 | 33 | 29 | 25 | 23 | 22 | 21 | 19 | 18 | 17 | 17 | 16 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 11 |
| 23 | 40 | 35 | 30 | 26 | 24 | 23 | 22 | 20 | 19 | 18 | 18 | 17 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 13 | 12 | 12 |
| 24 | 42 | 36 | 32 | 27 | 25 | 24 | 23 | 21 | 20 | 19 | 18 | 17 | 17 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 12 |
| 25 | 43 | 38 | 33 | 29 | 26 | 25 | 24 | 22 | 21 | 20 | 19 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 13 | 13 |
| 26 | 45 | 39 | 34 | 30 | 27 | 26 | 25 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 17 | 16 | 16 | 16 | 15 | 14 | 14 | 13 |
| 27 | 47 | 41 | 35 | 31 | 28 | 27 | 26 | 24 | 22 | 21 | 21 | 19 | 19 | 18 | 17 | 17 | 17 | 16 | 16 | 15 | 14 | 14 |
| 28 | 49 | 42 | 37 | 32 | 30 | 28 | 27 | 25 | 23 | 22 | 21 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 14 |
| 29 | 50 | 44 | 38 | 33 | 31 | 29 | 28 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 15 | 15 |
| 30 | 52 | 45 | 39 | 34 | 32 | 30 | 29 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 15 |
| 31 | 54 | 47 | 41 | 35 | 33 | 31 | 30 | 27 | 26 | 25 | 24 | 22 | 21 | 21 | 20 | 19 | 19 | 18 | 17 | 17 | 16 | 16 |
| 32 | 55 | 48 | 42 | 37 | 34 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 22 | 21 | 21 | 20 | 19 | 19 | 18 | 17 | 16 | 16 |
| 33 | 57 | 50 | 43 | 38 | 35 | 33 | 31 | 29 | 27 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 20 | 19 | 18 | 17 | 17 | 17 |
| 34 | 59 | 51 | 45 | 39 | 36 | 34 | 32 | 30 | 28 | 27 | 26 | 25 | 23 | 23 | 22 | 21 | 21 | 20 | 20 | 19 | 18 | 17 |
| 35 | 61 | 53 | 46 | 40 | 37 | 35 | 33 | 31 | 29 | 28 | 27 | 25 | 24 | 23 | 23 | 22 | 21 | 21 | 20 | 19 | 18 | 18 |
| 36 | 62 | 54 | 47 | 41 | 38 | 36 | 34 | 32 | 30 | 29 | 28 | 26 | 25 | 24 | 23 | 23 | 22 | 22 | 21 | 20 | 19 | 18 |
| 37 | 64 | 56 | 49 | 42 | 39 | 37 | 35 | 32 | 31 | 29 | 28 | 27 | 26 | 25 | 24 | 23 | 23 | 22 | 21 | 20 | 19 | 19 |
| 38 | 66 | 57 | 50 | 43 | 40 | 38 | 36 | 33 | 31 | 30 | 29 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 22 | 21 | 20 | 19 |
| 39 | 68 | 59 | 51 | 45 | 41 | 39 | 37 | 34 | 32 | 31 | 30 | 28 | 27 | 26 | 25 | 24 | 24 | 23 | 23 | 22 | 20 | 20 |
| 40 | 69 | 60 | 53 | 46 | 42 | 40 | 38 | 35 | 33 | 32 | 31 | 29 | 28 | 27 | 26 | 25 | 25 | 24 | 23 | 22 | 21 | 20 |
| 41 | 71 | 62 | 54 | 47 | 43 | 41 | 39 | 36 | 34 | 32 | 31 | 30 | 28 | 27 | 26 | 26 | 25 | 25 | 24 | 23 | 21 | 21 |
| 42 | 73 | 63 | 55 | 48 | 44 | 42 | 40 | 37 | 35 | 33 | 32 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 23 | 22 | 21 |
| 43 | 75 | 65 | 56 | 49 | 45 | 43 | 41 | 38 | 36 | 34 | 33 | 31 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 22 | 22 |
| 44 | 76 | 66 | 58 | 50 | 46 | 44 | 42 | 39 | 36 | 35 | 34 | 32 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 24 | 23 | 22 |
| 45 | 78 | 68 | 59 | 51 | 47 | 45 | 43 | 39 | 37 | 36 | 34 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 24 | 23 |
| 46 | 80 | 69 | 60 | 53 | 48 | 46 | 44 | 40 | 38 | 36 | 35 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 25 | 24 | 23 |
| 47 | 81 | 71 | 62 | 54 | 50 | 47 | 45 | 41 | 39 | 37 | 36 | 34 | 32 | 31 | 30 | 30 | 29 | 28 | 27 | 26 | 25 | 24 |

TABLE 5b) – Elongation values on $5,65 \sqrt{S_0}$ corresponding to those obtained on 2 in gauge length
(Rounded to the nearest whole number)

| Actual per cent elongation on 2 in gauge length | Corresponding per cent elongation on $5,65 \sqrt{S_0}$ gauge length if cross-sectional area in square inches is : | | | | | | | | | | | | | | | | | | | | | |
|---|---|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|
| | 0.05 | 0.10 | 0.15 | 0.20 | 0.25 | 0.30 | 0.35 | 0.40 | 0.45 | 0.50 | 0.60 | 0.70 | 0.80 | 0.90 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 | 3.0 | 4.0 |
| 18 | 22 | 19 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 13 | 12 | 12 | 12 | 11 | 11 | 11 | 11 | 10 | 10 | 9 |
| 19 | 23 | 20 | 18 | 17 | 17 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 13 | 12 | 12 | 11 | 11 | 11 | 10 | 9 |
| 20 | 24 | 21 | 19 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 12 | 12 | 11 | 10 |
| 21 | 25 | 22 | 20 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 11 | 10 |
| 22 | 26 | 23 | 21 | 20 | 19 | 18 | 18 | 17 | 17 | 17 | 16 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 11 |
| 23 | 28 | 24 | 22 | 21 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 12 | 11 |
| 24 | 29 | 25 | 23 | 22 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 12 |
| 25 | 30 | 26 | 24 | 23 | 22 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 17 | 16 | 15 | 15 | 15 | 14 | 13 | 12 |
| 26 | 31 | 27 | 25 | 24 | 23 | 22 | 21 | 21 | 20 | 20 | 19 | 18 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 14 | 13 |
| 27 | 32 | 28 | 26 | 25 | 24 | 23 | 22 | 21 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 16 | 14 | 13 |
| 28 | 34 | 29 | 27 | 26 | 24 | 24 | 23 | 22 | 22 | 21 | 20 | 20 | 19 | 19 | 19 | 18 | 17 | 17 | 16 | 16 | 15 | 14 |
| 29 | 35 | 30 | 28 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 21 | 20 | 20 | 19 | 18 | 18 | 17 | 17 | 17 | 15 | 14 |
| 30 | 36 | 31 | 29 | 27 | 26 | 25 | 24 | 24 | 23 | 23 | 22 | 21 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 16 | 15 |
| 31 | 37 | 32 | 30 | 28 | 27 | 26 | 25 | 25 | 24 | 24 | 23 | 22 | 21 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 16 | 15 |
| 32 | 38 | 33 | 31 | 29 | 28 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 22 | 22 | 21 | 20 | 20 | 19 | 19 | 18 | 17 | 16 |
| 33 | 40 | 34 | 32 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 23 | 23 | 22 | 22 | 21 | 20 | 20 | 19 | 19 | 17 | 16 |
| 34 | 41 | 36 | 33 | 31 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 23 | 23 | 22 | 22 | 21 | 20 | 20 | 20 | 18 | 17 |
| 35 | 42 | 37 | 34 | 32 | 30 | 29 | 28 | 28 | 27 | 27 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 21 | 20 | 19 | 17 |
| 36 | 43 | 38 | 35 | 33 | 31 | 30 | 29 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 21 | 19 | 18 |
| 37 | 44 | 39 | 36 | 34 | 32 | 31 | 30 | 29 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 20 | 18 |
| 38 | 46 | 40 | 37 | 35 | 33 | 32 | 31 | 30 | 29 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 23 | 23 | 22 | 22 | 20 | 19 |
| 39 | 47 | 41 | 38 | 36 | 34 | 33 | 32 | 31 | 30 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 23 | 23 | 22 | 21 | 19 |
| 40 | 48 | 42 | 39 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 21 | 20 |
| 41 | 49 | 43 | 40 | 37 | 36 | 34 | 33 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 25 | 24 | 24 | 22 | 20 |
| 42 | 50 | 44 | 40 | 38 | 37 | 35 | 34 | 33 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 25 | 24 | 22 | 21 |
| 43 | 52 | 45 | 41 | 39 | 37 | 36 | 35 | 34 | 33 | 33 | 31 | 30 | 30 | 29 | 28 | 27 | 27 | 26 | 25 | 25 | 23 | 21 |
| 44 | 53 | 46 | 42 | 40 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 23 | 22 |
| 45 | | 47 | 43 | 41 | 39 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 30 | 29 | 28 | 27 | 26 | 26 | 24 | 22 |
| 46 | | 48 | 44 | 42 | 40 | 39 | 37 | 36 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 24 | 23 |
| 47 | | 49 | 45 | 43 | 41 | 39 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 25 | 23 |