
**Dielektrične in uporovne lastnosti trdnih izolacijskih materialov - 2-3. del:
Določanje relativne permitivnosti in faktorja dielektričnih izgub (metode AC) -
Metoda kontaktne elektrode za izolacijske folije**

Dielectric and resistive properties of solid insulating materials - Part 2-3: Determination of relative permittivity and dielectric dissipation factor (AC methods) - Contact electrode method for insulating films

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TITLE:

Dielectric and resistive properties of solid insulating materials - Part 2-3: Determination of relative permittivity and dielectric dissipation factor (AC methods) - Contact electrode method for insulating films

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

DIELECTRIC AND RESISTIVE PROPERTIES OF SOLID INSULATING MATERIALS -**Part 2-3: Determination of relative permittivity and dielectric dissipation factor (AC methods) - Contact electrode method for insulating films**

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The text of this International Standard is based on the following documents:

FDIS	Report on voting
112/XX/FDIS	112/XX/RVD

Full information on the voting for the approval of this International Standard can be found in the report on voting indicated in the above table.

This document has been drafted in accordance with the ISO/IEC Directives, Part 2.

95 The committee has decided that the contents of this document will remain unchanged until the
96 stability date indicated on the IEC website under "http://webstore.iec.ch" in the data related to
97 the specific document. At this date, the document will be

- 98 • reconfirmed,
- 99 • withdrawn,
- 100 • replaced by a revised edition, or
- 101 • amended.

102

103 The National Committees are requested to note that for this document the stability date
104 is 2027.

105 THIS TEXT IS INCLUDED FOR THE INFORMATION OF THE NATIONAL COMMITTEES AND WILL BE DELETED
106 AT THE PUBLICATION STAGE.

107

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108

INTRODUCTION

109 Measuring the relative permittivity and the dielectric dissipation factor ($\tan \delta$) of insulating
110 polymer film with very thin thickness (about 10-100 μm) without any additional layer is important
111 for insulation applications. Now, there is lack of suitable technology and standard for a single
112 layer polymer film with very thin thickness. Using multilayer polymer films with 20-50 layers it
113 can be feasible to get the average value of the relative permittivity and dielectric dissipation
114 factor of insulating polymer film, but the effect of airgap inside may not be ignored. With
115 metalized electrodes on the surface of polymer film, it is possible to get acceptable results of
116 the relative permittivity and dielectric dissipation factor of insulating polymer film in research
117 laboratory. In this standard, the measuring technology and the test method are provided for
118 relative permittivity and dielectric dissipation factor of insulating polymer film with very thin
119 thickness without any additional layer or metallization on the sample, under technical frequency.

120

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DIELECTRIC AND RESISTIVE PROPERTIES OF SOLID INSULATING MATERIALS –

Part 2-3: Determination of relative permittivity and dielectric dissipation factor (AC methods) - Contact electrode method for insulating films

1 Scope

This International Standard of IEC 62631-2-3 specifies the measuring technology and the test method for relative permittivity and dielectric dissipation factor of insulating polymer film with very thin thickness without any additional layer and metallization on the sample surface. The adaptive thickness range is about from 10 to 100 μm . The proposed frequency is the power frequency (50 or 60 Hz), and it is also suitable in the technical frequency range from 1 Hz to 1 MHz.

2 Normative references

IEC 60050-212:2010, International Electrotechnical Vocabulary — Part 212: Electrical insulating solids, liquids, and gases

IEC 62631-2-1:2018, Dielectric and resistive properties of solid insulating materials - Part 2-1: Relative permittivity and dissipation factor-Technical frequency (0.1 Hz to 10 MHz) – AC methods

ISO 4593:1993, Plastics — Film and sheeting — Determination of thickness by mechanical scanning

IEC 60674-2:2019, Specification for plastic films for electrical purposes — Part 2: Methods of test

ISO 14644-1:2015, Cleanrooms and associated controlled environments — Part 1: Classification of air cleanliness by particle concentration

ISO 21920-2:2021, Geometrical product specifications (GPS) — Surface texture: Profile — Part 2: Terms, definitions and surface texture parameters

ISO 25178-2:2012, Geometrical product specifications (GPS) — Surface texture: Areal — Part 2: Terms, definitions and surface texture parameters

ISO 3534-1:2006, Statistics — Vocabulary and symbols —Part 1: General statistical terms and terms used in probability

ISO 3434-2:2006, Statistics — Vocabulary and symbols —Part 2: Applied statistics

ISO 3534-3:2013, Statistics — Vocabulary and symbols —Part 3: Design of experiments

3 Terms definitions and abbreviated terms

3.1 Terms and definitions

3.1.1 thin insulating film

an insulating polymer film without any additional layer, with 10 to 100 μm uniform thickness, planar, even and smooth.

160 **3.1.2 AC bridge**

161 an instrument to use balance method to measure the capacitance and loss of capacitor sample
162 under AC voltage, for example, a capacitor bridge.

163 Note 1 to entry: Usually, it works under power frequency with very high accuracy and with low applied
164 voltage.

165 Note 2 to entry: In some special case, it is also possible to work under technical frequency.

166 **3.1.3 impedance material analyzer**

167 an instrument to use AC current method to measure the capacitance and dielectric loss of a
168 capacitor.

169 Note 1 to entry: It works under a relatively low voltage and with large band range, but its accuracy is
170 usually relatively low.

171 Note 2 to entry: It uses five terminals to measure the device parameters so that it needs a suitable adaptor
172 for the three electrodes sample.

173 **3.1.4 power frequency**

174 the frequency used for power system, is usually at 50 Hz or 60 Hz.

175 **3.1.5 technical frequency**

176 the frequency for technical application, is usually from 1 Hz to 1 MHz.

177 **3.1.6 measuring voltage**

178 the voltage applied on the measuring sample during the measurement, should be lower than
179 the voltage induced by partial discharge.

180 **3.1.7 apparent thickness (mechanical thickness)**

181 the thickness of sample measured by a mechanical apparatus, which is equivalent to “bulking
182 thickness” in IEC 60674-2.

183 **3.1.8 density thickness**

184 the thickness of sample measured from the density of sample, which is equivalent to “gravimetric
185 thickness” in IEC 60674-2.

186 **3.1.9 void ratio α**

187 the percentage increase between the apparent thickness and the density thickness, which is
188 dependent on the surface roughness.

189 Note 1 to entry: For the sample with scabrous surface, the apparent thickness and the density
190 thickness are different.

191 Note 2 to entry: The void ratio α (%) is defined by the following formula:

$$192 \quad \alpha = \frac{d_x - d_d}{d_x} \cdot 100(\%) \quad (1)$$

193 where,

194 d_x is the apparent thickness of sample in μm ;

195 d_d is the density thickness of sample in μm .

196 Note 3 to entry: The apparent thickness and the density thickness should be measured by using
197 the same sample in accordance with ISO 4593.

198 3.1.10 contact ratio η

199 the percentage ratio of contact area over the total area.

200 Note 1 to entry: For the sample with scabrous surface, it cannot make perfect contact with the
201 high flatness and low roughness surface of electrode.

202 Note 2 to entry: It is dependent on the sample surface roughness and is defined by the following
203 formula:

$$204 \quad \eta = \frac{\text{contact area}}{\text{total area}} \cdot 100 (\%) \quad (2)$$

205 where, η is the contact ratio in %.

206 3.1.11 surface roughness of sample R_a

207 is defined by the following formula according to ISO 21920-2:

$$208 \quad R_a = \frac{1}{l_e} \int_0^{l_e} |z(x)| dx \quad (3)$$

209 where

210 l_e is the evaluation length of the sample profile,

211 $z(x)$ is the function that described the height of the assessed scale-limited profile,

212 R_a is the arithmetic mean height in μm of the sample profile, also called the surface roughness
213 of sample in this standard.

214 3.2 Abbreviated terms

215 AC - Alternating Current

216 α – void ratio

217 η - contact ratio

218 R_a - surface roughness of sample in μm

219 4 Principle of method

220 4.1 The principle of measurement

221 The complex capacitance \dot{C}_x of the dielectric sample with electrode can be obtained by using
222 an AC bridge or an impedance/material analyzer. For planar, even and smooth film sample, the
223 relationship between the complex permittivity $\dot{\epsilon}_x$ and the complex capacitance \dot{C}_x can be
224 shown as follows,

$$225 \quad \dot{C}_x = \frac{\varepsilon_0 \dot{\varepsilon}_x S}{d_x}, \quad (4)$$

226 where, d_x is the thickness of planar film sample, S is the area of electrode and ε_0 is the
227 electric constant (also called permittivity of vacuum). Therefore, the complex permittivity of the
228 dielectric materials can be derived as,

$$229 \quad \dot{\varepsilon}_x = \frac{d_x}{\varepsilon_0 S} \dot{C}_x. \quad (5)$$

230 The relationship of the complex permittivity $\dot{\varepsilon}_x$ with real part ε' , imaginary part ε'' and
231 dielectric dissipation factor $\tan \delta$ (also marked D_x) can be shown as follows,

$$232 \quad \begin{cases} \dot{\varepsilon}_x = \varepsilon' + j\varepsilon'' \\ \tan \delta = \frac{\varepsilon''}{\varepsilon'} \\ \varepsilon_x = \varepsilon' \end{cases}, \quad (6)$$

233 where, the real part ε' is called relative permittivity ε_x , and the imaginary part ε'' is called
234 dielectric loss index. By using an AC bridge, the dielectric dissipation factor $\tan \delta$ and the real
235 part C_x of complex capacitance \dot{C}_x can be measured directly. The relative permittivity ε_x of
236 dielectric material can be obtained from

$$237 \quad \varepsilon_x = \frac{d_x}{\varepsilon_0 S} C_x \quad (7)$$

238 4.2 The edge effect of electrodes

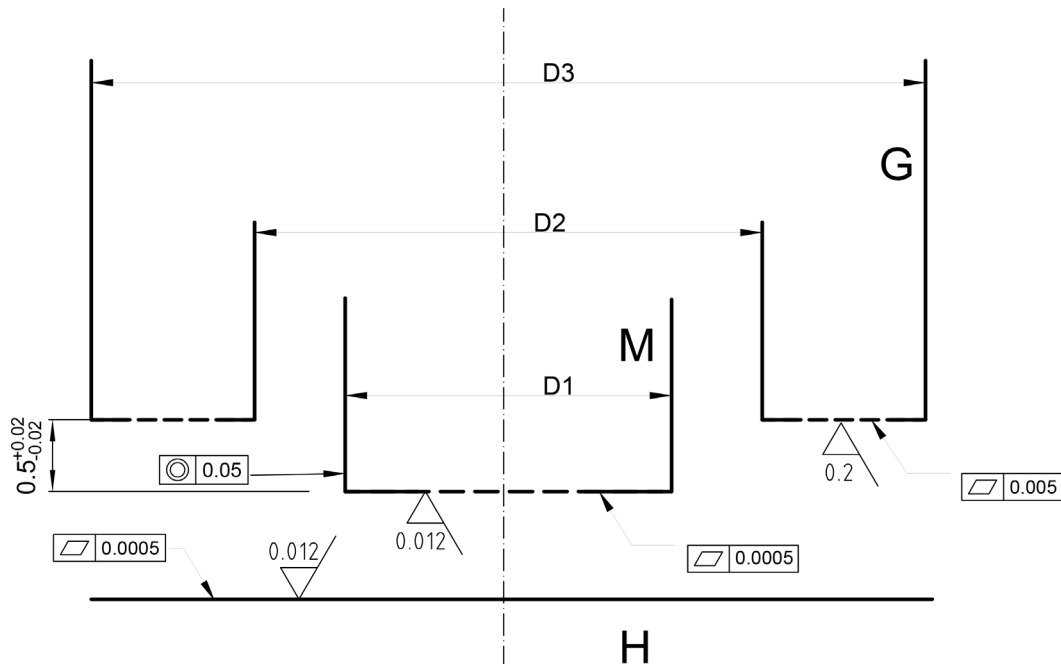
239 Due to the limitation of mechanical manufacture, the gap between the measuring electrode and
240 the guard ring will be bigger than 0.5 mm. Generally, there is edge effect of electrodes in the
241 dielectric measurement. In the case of sample with thick thickness (the thickness > 0,5 mm), the
242 guard ring electrode is effective to reduce the edge effect of electrodes. However, for the
243 sample with thin thickness (the thickness < 0,5 mm), the guard ring electrode does not
244 significantly reduce the edge effect because the gap between the measuring electrode and the
245 guard ring is much bigger than the thickness of sample. In this case, due to the limitation of
246 mechanical manufacture, the gap between the measuring electrode and the guard ring will be
247 much bigger than the thickness of sample. See also Clause 5.2.

248 5 The electrodes

249 5.1 Design and manufacture of electrodes

250 It is the most important requirement in the standard to design and manufacture the measuring
251 electrodes. It is a system with three electrodes, including a measuring electrode (M), a guarded
252 electrode (G) and a high voltage electrode (H). For example, the possible dimension of three
253 electrodes is shown in Table 1, and key requirements of three electrodes for manufacture are
254 noted in Figure 1. As the thickness of sample is relatively thin, the diameter of the measuring
255 electrode should not be too large to avoid a large measured capacitance that would make the
256 choice of measuring instrument difficult. The most important requirements on the manufacture
257 are the situation of the surface of the measuring electrode and the surface of high voltage
258 electrode. They must satisfy the following conditions: the roughness < 0.012 μm and the flatness

259 <0.5 μm . The surface condition is very important for keeping good contact between the
 260 electrode and the measured dielectric film.



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Figure 1 – The diagram of the system with three electrodes

D1: the diameter of the measuring electrode M

D2: the inner diameter of the guarded electrode G

D3: the outer diameter of the guarded electrode G

D4: the diameter of the high voltage electrode H.

266

267 With Figure 1, g is the gap between the guarded electrode and the measuring electrode the
 268 gap $g=(D2-D1)/2$ is kept to about 1 mm.

269 The material of electrode M and electrode H must satisfy the following condition: good
 270 conductivity, non-ferromagnetic, anti-rust, and enough rigidity and hardness. The suggested
 271 hardness is within HRC 58 to 62. The possible optional material is the alloy
 272 7Mn15Cr2Al3V2WMo (C 0.65-0.75, Si \leq 0.80, Mn14.50-16.00, Cr 2.00-2.50, Mo 0.50-0.80, W
 273 0.50-0.80, V 1.50-2.00, Al 2.70-3.30, P \leq 0.040, S \leq 0.030), which is an Austenitic non-magnetic
 274 tool steel. More information about the manufacture of electrodes can be found in Annex B

275 The material of electrode G can be a metal material with good conductivity, non-ferromagnetic,
 276 anti-rust, like stainless or brass with surface plating protection, etc.

277 **Table 1 – The diameter parameters of the three electrodes system and the relationship**
 278 **of measured ϵ_x for the thickness of sample and the measured capacitance**

D1 (mm)	D2 (mm)	D3 (mm)	D4 (mm)	ϵ_x
35.68 ± 0.05	37.68 ± 0.1	58	70	$C_x (pF) \cdot d_x (mm) / 8.85$ $= C_x (nF) \cdot d_x (\mu m) / 8.85$