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Merjenje pretoka fluida na osnovi tlačne razlike, povzročene z napravo, vstavljeno v polno zapolnjen vod s krožnim prerezom - 3. del: Šobe in Venturijeve šobe (ISO 5167-3:2022)

Measurement of fluid flow by means of pressure differential devices inserted in circular cross-section conduits running full - Part 3: Nozzles and Venturi nozzles (ISO 5167-3:2022)

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Durchflussmessung von Fluiden mit Drosselgeräten in voll durchströmten Leitungen mit Kreisquerschnitt - Teil 3: Düsen und Venturidüsen (ISO 5167-3:2022)

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Mesurage du débit des fluides au moyen d'appareils déprimogènes insérés dans des conduites en charge de section circulaire - Partie 3: Tuyères et Venturi-tuyères (ISO 5167-3:2022)

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Measurement of fluid flow by means of pressure
differential devices inserted in circular cross-section
conduits running full - Part 3: Nozzles and Venturi nozzles
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This European Standard was approved by CEN on 22 October 2022.

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European foreword

This document (EN ISO 5167-3:2022) has been prepared by Technical Committee ISO/TC 30 "Measurement of fluid flow in closed conduits" in collaboration with CCMC.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by May 2023, and conflicting national standards shall be withdrawn at the latest by May 2023.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN shall not be held responsible for identifying any or all such patent rights.

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2022-10

**Measurement of fluid flow by means of
pressure differential devices inserted
in circular cross-section conduits
running full —**

**Part 3:
Nozzles and Venturi nozzles**

*Mesurage du débit des fluides au moyen d'appareils déprimogènes
insérés dans des conduites en charge de section circulaire —*

Partie 3: Tuyères et Venturi-tuyères

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 30, *Measurement of fluid flow in closed conduits*, Subcommittee SC 2, *Pressure differential devices*, in collaboration with the European Committee for Standardization (CEN) Technical Committee CEN/SS F05, *Measuring instruments*, in accordance with the Agreement on technical cooperation between ISO and CEN (Vienna Agreement).

This third edition cancels and replaces the second edition (ISO 5167-3:2020), of which it constitutes a minor revision. The main changes are as follows:

- harmonization with ISO/IEC Guide 98-3;
- minor changes to give harmonization with the other parts of ISO 5167.

A list of all parts in the ISO 5167 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

ISO 5167-3:2022(E)**Introduction**

ISO 5167, consisting of six parts, covers the geometry and method of use (installation and operating conditions) of orifice plates, nozzles, Venturi tubes, cone meters and wedge meters when they are inserted in a conduit running full to determine the flowrate of the fluid flowing in the conduit. It also gives necessary information for calculating the flowrate and its associated uncertainty.

ISO 5167 (all parts) is applicable only to pressure differential devices in which the flow remains subsonic throughout the measuring section and where the fluid can be considered as single-phase, but is not applicable to the measurement of pulsating flow. Furthermore, each of these devices can only be used within specified limits of pipe size and Reynolds number.

ISO 5167 (all parts) deals with devices for which direct calibration experiments have been made, sufficient in number, spread and quality to enable coherent systems of application to be based on their results and coefficients to be given with certain predictable limits of uncertainty. ISO 5167 also provides methodology for bespoke calibration of differential pressure meters.

The devices introduced into the pipe are called primary devices. The term primary device also includes the pressure tappings. All other instruments or devices required to facilitate the instrument readings are known as secondary devices, and the flow computer that receives these readings and performs the algorithms is known as a tertiary device. ISO 5167 (all parts) covers primary devices; secondary devices (ISO 2186) and tertiary devices will be mentioned only occasionally.

Aspects of safety are not dealt within ISO 5167-1 to ISO 5167-6. It is the responsibility of the user to ensure that the system meets applicable safety regulations.

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Measurement of fluid flow by means of pressure differential devices inserted in circular cross-section conduits running full —

Part 3: Nozzles and Venturi nozzles

1 Scope

This document specifies the geometry and method of use (installation and operating conditions) of nozzles and Venturi nozzles when they are inserted in a conduit running full to determine the flowrate of the fluid flowing in the conduit.

This document also provides background information for calculating the flowrate and is applicable in conjunction with the requirements given in ISO 5167-1.

This document is applicable to nozzles and Venturi nozzles in which the flow remains subsonic throughout the measuring section and where the fluid can be considered as single-phase. In addition, each of the devices can only be used within specified limits of pipe size and Reynolds number. It is not applicable to the measurement of pulsating flow. It does not cover the use of nozzles and Venturi nozzles in pipe sizes less than 50 mm or more than 630 mm, or where the pipe Reynolds numbers are below 10 000.

This document deals with

a) three types of standard nozzles:

- 1) ISA 1932¹⁾ nozzle;
- 2) the long radius nozzle²⁾;
- 3) the throat-tapped nozzle

b) the Venturi nozzle.

The three types of standard nozzle are fundamentally different and are described separately in this document. The Venturi nozzle has the same upstream face as the ISA 1932 nozzle, but has a divergent section and, therefore, a different location for the downstream pressure tappings, and is described separately. This design has a lower pressure loss than a similar nozzle. For all of these nozzles and for the Venturi nozzle direct calibration experiments have been made, sufficient in number, spread and quality to enable coherent systems of application to be based on their results and coefficients to be given with certain predictable limits of uncertainty.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

1) ISA is the abbreviation for the International Federation of the National Standardizing Associations, which was superseded by ISO in 1946.

2) The long radius nozzle differs from the ISA 1932 nozzle in shape and in the position of the pressure tappings.

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ISO 4006, *Measurement of fluid flow in closed conduits — Vocabulary and symbols*

ISO 5167-1, *Measurement of fluid flow by means of pressure differential devices inserted in circular cross-section conduits running full — Part 1: General principles and requirements*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 4006 and ISO 5167-1 apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

4 Principles of the method of measurement and computation

The principle of the method of measurement is based on the installation of a nozzle or a Venturi nozzle into a pipeline in which a fluid is running full. The installation of the primary device causes a static pressure difference between the upstream side and the throat. The flowrate can be determined from the measured value of this pressure difference and from the knowledge of the characteristics of the flowing fluid as well as the circumstances under which the device is being used. It is assumed that the device is geometrically similar to one on which calibration has been carried out and that the conditions of use are the same, i.e. that it is in accordance with this document.

The mass flowrate can be determined by [Formula \(1\)](#):

$$q_m = \frac{C}{\sqrt{1-\beta^4}} \varepsilon \frac{\pi}{4} d^2 \sqrt{2\Delta p \rho_1} \quad (1)$$

The uncertainty limits can be calculated using the procedure given in ISO 5167-1:2022, Clause 8.

Similarly, the value of the volume flowrate can be calculated by [Formula \(2\)](#) since

$$q_V = \frac{q_m}{\rho} \quad (2)$$

where

ρ is the fluid density at the temperature and pressure for which the volume is stated;

q_V is the volume flowrate.

Computation of the flowrate, which is a purely arithmetic process, is performed by replacing the different items on the right-hand side of [Formula \(1\)](#) by their numerical values. [Tables A.1](#) to [A.5](#) are given for convenience. [Tables A.1](#), [A.2](#) and [A.4](#) give the values of C as a function of β . [Table A.3](#) gives the values of C as a function of Re_d . [Table A.5](#) gives expansibility (expansion) factors, ε . They are not intended for precise interpolation. Extrapolation is not permitted.

The discharge coefficient C may be dependent on Re_D or Re_d which is itself dependent on q_m and has to be obtained by iteration. (See ISO 5167-1 for guidance regarding the choice of the iteration procedure and initial estimates.)

The diameters d and D mentioned in [Formula \(1\)](#) are the values of the diameters at working conditions. Measurements taken at any other conditions should be corrected for any possible expansion or contraction of the primary device and the pipe due to the values of the temperature and pressure of the fluid during the measurement.

It is necessary to know the density and the viscosity of the fluid at working conditions. In the case of a compressible fluid, it is also necessary to know the isentropic exponent of the fluid at working conditions.

5 Nozzles and Venturi nozzles

5.1 ISA 1932 nozzle

5.1.1 General shape

The part of the nozzle inside the pipe is circular. The nozzle consists of a convergent section with a rounded profile, and a cylindrical throat.

[Figure 1](#) shows the cross-section of an ISA 1932 nozzle at a plane passing through the centreline of the throat.

The letters in the following text refer to those shown on [Figure 1](#).

5.1.2 Nozzle profile

5.1.2.1 The profile of the nozzle may be characterized by distinguishing:

- a flat inlet part A, perpendicular to the centreline;
- a convergent section defined by two arcs of circumference B and C;
- a cylindrical throat E;
- a recess F which is optional (it is required only if damage to the edge G is feared).

5.1.2.2 The flat inlet part A is limited by a circumference centred on the axis of revolution, with a diameter of $1,5d$, and by the inside circumference of the pipe, of diameter D .

When $d = (2/3)D$, the radial width of this flat part is zero.

When d is greater than $(2/3)D$, the upstream face of the nozzle does not include a flat inlet part within the pipe. In this case, the nozzle is manufactured as if D were greater than $1,5d$, and the inlet flat part is then faced off so that the largest diameter of the convergent profile is just equal to D [see [5.1.2.7](#) and [Figure 1 b](#)].

5.1.2.3 The arc of circumference B is tangential to the flat inlet part A when $d < (2/3)D$ while its radius R_1 is equal to $0,2d \pm 0,02d$ for $\beta < 0,5$ and to $0,2d \pm 0,006d$ for $\beta \geq 0,5$. Its centre is at $0,2d$ from the inlet plane and at $0,75d$ from the axial centreline.

5.1.2.4 The arc of circumference C is tangential to the arc of circumference B and to the throat E. Its radius R_2 is equal to $d/3 \pm 0,033d$ for $\beta < 0,5$ and to $d/3 \pm 0,01d$ for $\beta \geq 0,5$. Its centre is at $d/2 + d/3 = (5/6)d$ from the axial centreline and as given by [Formula \(3\)](#), at

$$a_n = \left(\frac{12 + \sqrt{39}}{60} \right) d = 0,3041 d \quad (3)$$

from the flat inlet part A.