



# Standard Test Method for Heat and Visible Smoke Release Rates for Materials and Products Using an Oxygen Consumption Calorimeter<sup>1</sup>

This standard is issued under the fixed designation E1354; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This fire-test-response standard provides for measuring the response of materials exposed to controlled levels of radiant heating with or without an external ignitor.

1.2 This test method is used to determine the ignitability, heat release rates, mass loss rates, effective heat of combustion, and visible smoke development of materials and products.

1.3 The rate of heat release is determined by measurement of the oxygen consumption as determined by the oxygen concentration and the flow rate in the exhaust product stream. The effective heat of combustion is determined from a concomitant measurement of specimen mass loss rate, in combination with the heat release rate. Smoke development is measured by obscuration of light by the combustion product stream.

1.4 Specimens shall be exposed to initial test heat fluxes in the range of 0 to 100 kW/m<sup>2</sup>. External ignition, when used, shall be by electric spark. The value of the initial test heat flux and the use of external ignition are to be as specified in the relevant material or performance standard (see X1.2). The normal specimen testing orientation is horizontal, independent of whether the end-use application involves a horizontal or a vertical orientation. The apparatus also contains provisions for vertical orientation testing; this is used for exploratory or diagnostic studies only.

1.5 Ignitability is determined as a measurement of time from initial exposure to time of sustained flaming.

1.6 This test method has been developed for use for material and product evaluations, mathematical modeling, design purposes, or development and research. Examples of material specimens include portions of an end-use product or the various components used in the end-use product.

1.7 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.8 *This standard is used to measure and describe the response of materials, products, or assemblies to heat and*

*flame under controlled conditions, but does not by itself incorporate all factors required for fire hazard or fire risk assessment of the materials, products, or assemblies under actual fire conditions.*

1.9 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use. For specific hazard statements, see Section 7.*

## 2. Referenced Documents

### 2.1 ASTM Standards:<sup>2</sup>

D5865 Test Method for Gross Calorific Value of Coal and Coke

E176 Terminology of Fire Standards

E177 Practice for Use of the Terms Precision and Bias in ASTM Test Methods

E603 Guide for Room Fire Experiments

E662 Test Method for Specific Optical Density of Smoke Generated by Solid Materials

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

E906 Test Method for Heat and Visible Smoke Release Rates for Materials and Products Using a Thermopile Method

### 2.2 ISO Standards:<sup>3</sup>

ISO 5657-1986(E) Fire Tests—reaction to fire—ignitability of building materials

ISO 5725-2 (1994) Accuracy (trueness and precision) of measurement methods and results — Part 2: Basic method for the determination of repeatability and reproducibility of a standard measurement method

## 3. Terminology

3.1 *Definitions*—For definitions of terms used in this test method, refer to Terminology E176.

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee E05 on Fire Standards and is the direct responsibility of Subcommittee E05.21 on Smoke and Combustion Products.

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<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>3</sup> Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

### 3.2 Definitions of Terms Specific to This Standard:

3.2.1 *effective heat of combustion,  $n$* —the amount of heat generated per unit mass lost by a material, product or assembly, when exposed to specific fire test conditions (contrast *gross heat of combustion*).

3.2.1.1 *Discussion*—The effective heat of combustion depends on the test method and is determined by dividing the measured heat release by the mass loss during a specified period of time under the specified test conditions. Typically, the specified fire test conditions are provided by the specifications of the fire test standard that cites effective heat of combustion as a quantity to be measured. For certain fire test conditions, involving very high heat and high oxygen concentrations under high pressure, the effective heat of combustion will approximate the gross heat of combustion. More often, the fire test conditions will represent or approximate certain real fire exposure conditions, and the effective heat of combustion is the appropriate measure. Typical units are kJ/g or MJ/kg.

3.2.2 *gross heat of combustion,  $n$* —the maximum amount of heat per unit mass that theoretically can be released by the combustion of a material, product, or assembly; it can be determined experimentally and only under conditions of high pressure and in pure oxygen (contrast *effective heat of combustion*).

3.2.3 *heat flux,  $n$* —heat transfer to a surface per unit area, per unit time (see also *initial test heat flux*).

3.2.3.1 *Discussion*—The heat flux from an energy source, such as a radiant heater, can be measured at the initiation of a test (such as Test Method E1354 or Test Method E906) and then reported as the incident heat flux, with the understanding that the burning of the test specimen can generate additional heat flux to the specimen surface. The heat flux can also be measured at any time during a fire test, for example as described in Guide E603, on any surface, and with measurement devices responding to radiative and convective fluxes. Typical units are kW/m<sup>2</sup>, kJ/(s m<sup>2</sup>), W/cm<sup>2</sup>, or BTU/(s ft<sup>2</sup>).

3.2.4 *heat release rate,  $n$* —the heat evolved from the specimen, per unit of time.

3.2.5 *ignitability,  $n$* —the propensity to ignition, as measured by the time to sustained flaming, in seconds, at a specified heating flux.

3.2.6 *initial test heat flux,  $n$* —the heat flux set on the test apparatus at the initiation of the test (see also *heat flux*).

3.2.6.1 *Discussion*—The initial test heat flux is the heat flux value commonly used when describing or setting test conditions.

3.2.7 *net heat of combustion,  $n$* —the oxygen bomb (see Test Method D5865) value for the heat of combustion, corrected for gaseous state of product water.

3.2.7.1 *Discussion*—The net heat of combustion differs from the gross heat of combustion in that the former assesses the heat per unit mass generated from a combustion process that ends with water in the gaseous state while the latter ends with water in the liquid state.

3.2.8 *orientation,  $n$* —the plane in which the exposed face of the specimen is located during testing, either vertical or horizontal facing up.

3.2.9 *oxygen consumption principle,  $n$* —the expression of the relationship between the mass of oxygen consumed during combustion and the heat released.

3.2.10 *smoke obscuration,  $n$* —reduction of light transmission by smoke, as measured by light attenuation.

3.2.11 *sustained flaming,  $n$* —existence of flame on or over most of the specimen surface for periods of at least 4 s.

3.2.11.1 *Discussion*—Flaming of less than 4 s duration is identified as flashing or transitory flaming.

### 3.3 Symbols:

$A_s$	= nominal specimen exposed surface area, 0.01 m <sup>2</sup> .
$C$	= calibration constant for oxygen consumption analysis, m <sup>1/2</sup> – kg <sup>1/2</sup> – K <sup>1/2</sup> .
$\Delta h_c$	= net heat of combustion, kJ/kg.
$\Delta h_{c,eff}$	= effective heat of combustion, kJ/kg.
$I$	= actual beam intensity.
$I_o$	= beam intensity with no smoke.
$k$	= smoke extinction coefficient, m <sup>-1</sup> .
$L$	= extinction beam path length, m.
$m$	= specimen mass, kg.
$m_f$	= final specimen mass, kg.
$m_i$	= initial specimen mass, kg.
$\dot{m}$	= specimen mass loss rate, kg/s.
$\Delta P$	= orifice meter pressure differential, Pa.
$q''_{tot}$	= total heat released, kJ/m <sup>2</sup> (Note that kJ ≡ kW·s).
$\dot{q}$	= heat release rate, kW.
$q''_{max}$	= maximum heat release rate per unit area (kW/m <sup>2</sup> ).
$q''_{180}$	= average heat release rate, per unit area, over the time period starting at $t_{ig}$ and ending 180 s later (kW/m <sup>2</sup> ).
$r$	= repeatability (the units are the same as for the variable being characterized).
$R$	= reproducibility (the units are the same as for the variable being characterized).
$r_o$	= stoichiometric oxygen/fuel mass ratio (–).
$S_r$	= sample-based standard deviation estimate for repeatability (same units as $r$ ).
$S_R$	= sample-based standard deviation estimate for reproducibility (same units as $R$ ).
$t$	= time, s.
$t_d$	= oxygen analyzer delay time, s.
$t_{ig}$	= time to sustained flaming (s).
$\rho$	= density (kg/m <sup>3</sup> ).
$\Delta t$	= sampling time interval, s.
$T_c$	= absolute temperature of gas at the orifice meter, K.
$\dot{V}$	= volume exhaust flow rate, measured at the location of the laser photometer, m <sup>3</sup> /s.
$X_{O_2_0}$	= oxygen analyzer reading, mole fraction O <sub>2</sub> (–).
$X_{O_2_1}$	= initial value of oxygen analyzer reading (–).
$X_{O_2}$	= oxygen analyzer reading, before delay time correction (–).
$\sigma_f$	= specific extinction area, for smoke, m <sup>2</sup> /kg.
$\sigma_r$	= repeatability standard deviation (same units as $r$ ).
$\sigma_R$	= reproducibility standard deviation (same units as $R$ ).

#### 4. Summary of Test Method

4.1 This test method is based on the observation (1)<sup>4</sup> that, generally, the net heat of combustion is directly related to the amount of oxygen required for combustion. The relationship is that approximately  $13.1 \times 10^3$  kJ of heat are released per 1 kg of oxygen consumed. Specimens in the test are burned in ambient air conditions, while being subjected to a predetermined initial test heat flux, which can be set from 0 to 100 kW/m<sup>2</sup>. The test permits burning to occur either with or without spark ignition. The primary measurements are oxygen concentrations and exhaust gas flow rate. Additional measurements include the mass-loss rate of the specimen, the time to sustained flaming and smoke obscuration, or as required in the relevant material or performance standard.

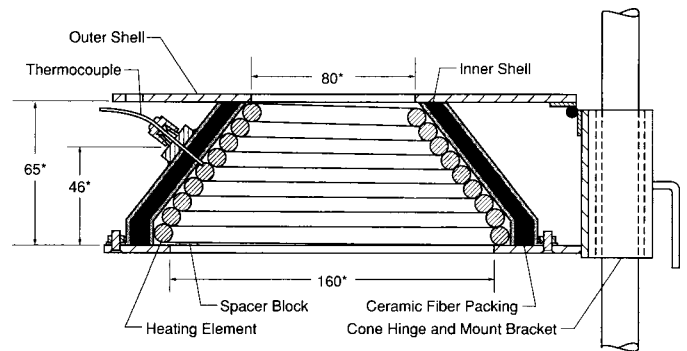
#### 5. Significance and Use

5.1 This test method is used primarily to determine the heat evolved in, or contributed to, a fire involving products of the test material. Also included is a determination of the effective heat of combustion, mass loss rate, the time to sustained flaming, and smoke production. These properties are determined on small size specimens that are representative of those in the intended end use.

5.2 This test method is applicable to various categories of products and is not limited to representing a single fire scenario. Additional guidance for testing is given in X1.2.3 and X1.11.

5.3 This test method is not applicable to end-use products that do not have planar, or nearly planar, external surfaces.

<sup>4</sup> The boldface numbers in parentheses refer to the list of references at the end of this test method.



NOTE 1—All dimensions are in millimetres.

NOTE 2—\* Indicates a critical dimension.

FIG. 2 Cross-Section View Through the Heater

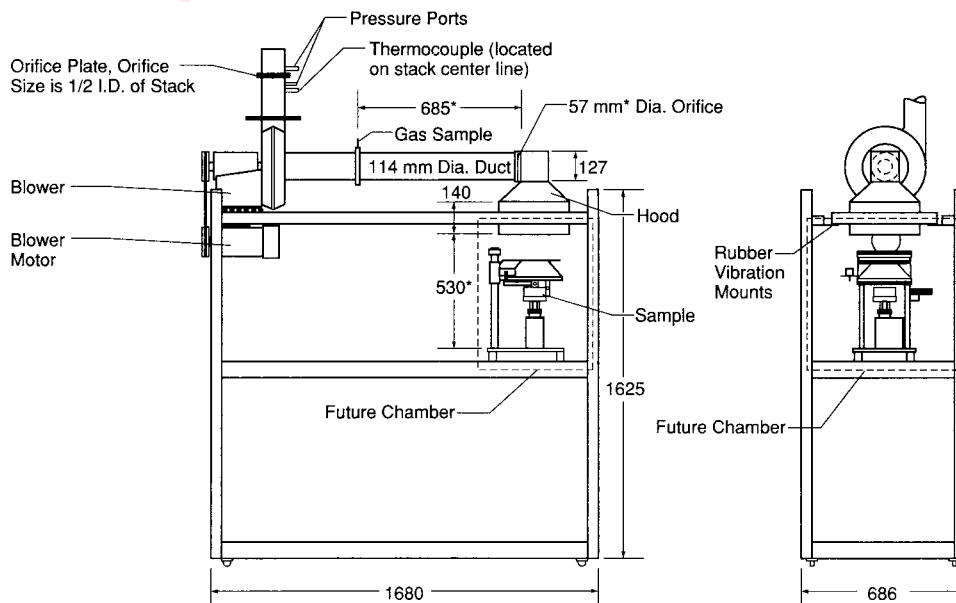
#### 6. Apparatus

##### 6.1 General:

6.1.1 All dimensions given in the figures that are followed by an asterisk are mandatory, and shall be followed within nominal tolerances of  $\pm 1$  mm, unless otherwise specified. Particularly critical dimensions are followed by an asterisk in Figs. 1-12.

6.1.2 The test apparatus<sup>5</sup> shall consist essentially of the following components: a conical radiant electric heater, capable of horizontal or vertical orientation; specimen holders, different for the two orientations; an exhaust gas system with oxygen monitoring and flow measuring instrumentation; an electric ignition spark plug; a data collection and analysis system; and a load cell for measuring specimen mass loss. A

<sup>5</sup> A list of suppliers of this apparatus is available from ASTM Headquarters.



NOTE 1—All dimensions are in millimetres.

NOTE 2—\* Indicates a critical dimension.

FIG. 1 Overall View of Apparatus

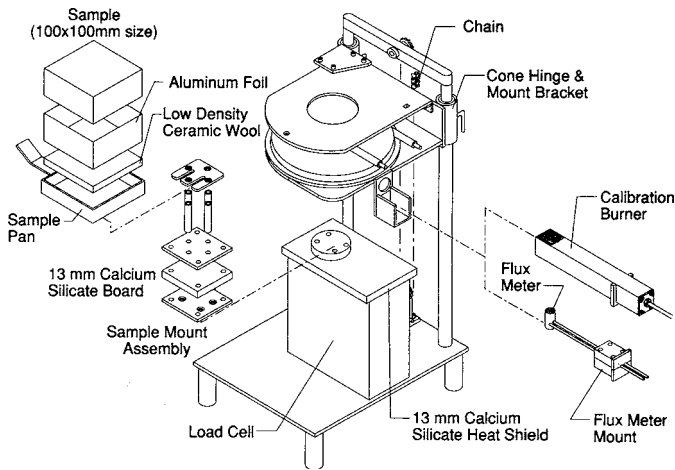


FIG. 3 Exploded View, Horizontal Orientation

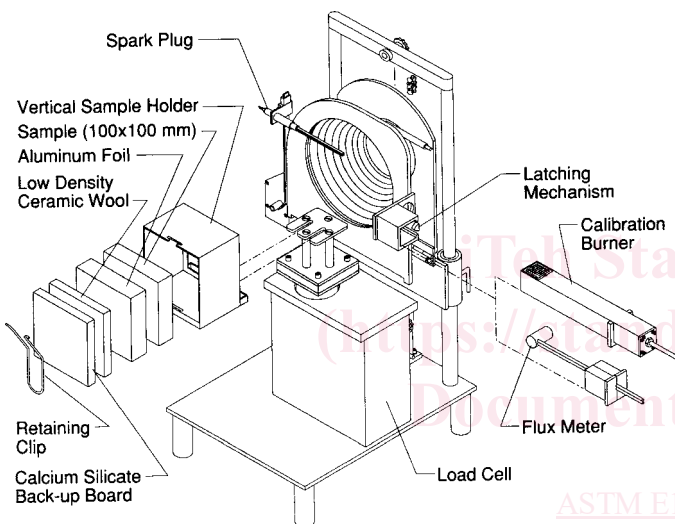


FIG. 4 Exploded View, Vertical Orientation

general view of the apparatus is shown in Fig. 1; a cross section through the heater in Fig. 2; and exploded views of horizontal and vertical orientations in Fig. 3 and Fig. 4.

6.1.3 Additional details describing features and operation of the test apparatus are given in Ref (2).

6.2 Conical Heater:

6.2.1 The active element of the heater shall consist of an electrical heater rod, rated at 5000 W at 240 V, tightly wound into the shape of a truncated cone (Fig. 2 and Fig. 4). The heater shall be encased on the outside with a double-wall stainless steel cone, packed with a refractory fiber material of approximately 100 kg/m<sup>3</sup> density.

6.2.2 The heater shall be hinged so it can be swung into either a horizontal or a vertical orientation. The heater shall be capable of producing irradiances on the surface of the specimen of up to 100 kW/m<sup>2</sup>. The irradiance shall be uniform within the central 50 by 50-mm area of the specimen to within ±2 % in the horizontal orientation and to within ±10 % in the vertical orientation. As the geometry of the heater is critical, the dimensions on Fig. 2 are mandatory.

6.2.3 The irradiance from the heater shall be capable of being held at a preset level by means of a temperature

controller and three type K stainless steel sheathed thermocouples, symmetrically disposed and in contact with, but not welded to, the heater element (see Fig. 2). The thermocouples shall be of equal length and wired in parallel to the temperature controller. The standard thermocouples are sheathed, 1.5 and 1.6 mm outside diameter, with an unexposed hot junction. Alternatively, either 3 mm outside diameter sheathed thermocouples with an exposed hot junction or 1 mm outside diameter sheathed thermocouples with unexposed hot junction can be used.

6.3 Temperature Controller:

6.3.1 The temperature controller for the heater shall be capable of holding the element temperature steady to within ±2°C. A suitable system is a 3-term controller (proportional, integral, and derivative) and a thyristor unit capable of switching currents up to 25 A at 240 V.

6.3.2 The controller shall have a temperature input range of 0 to 1000°C; a set scale capable of being read to 2°C or better; and automatic cold junction compensation. The controller shall be equipped with a safety feature such that in the event of an open circuit in the thermocouple line, it will cause the temperature to fall to near the bottom of its range.

6.3.3 The thyristor unit shall be of the zero crossing and not of the phase angle type.

6.3.4 The heater temperature shall be monitored by a meter capable of being read to ±2°C, or better. It shall be permitted to be incorporated into the temperature controller.

6.4 Exhaust System:

6.4.1 The exhaust-gas system shall consist of a high temperature centrifugal exhaust fan, a hood, intake and exhaust ducts for the fan, and an orifice plate flowmeter (Fig. 5). The exhaust system shall be capable of developing flows from 0.012 to 0.035 m<sup>3</sup>/s.

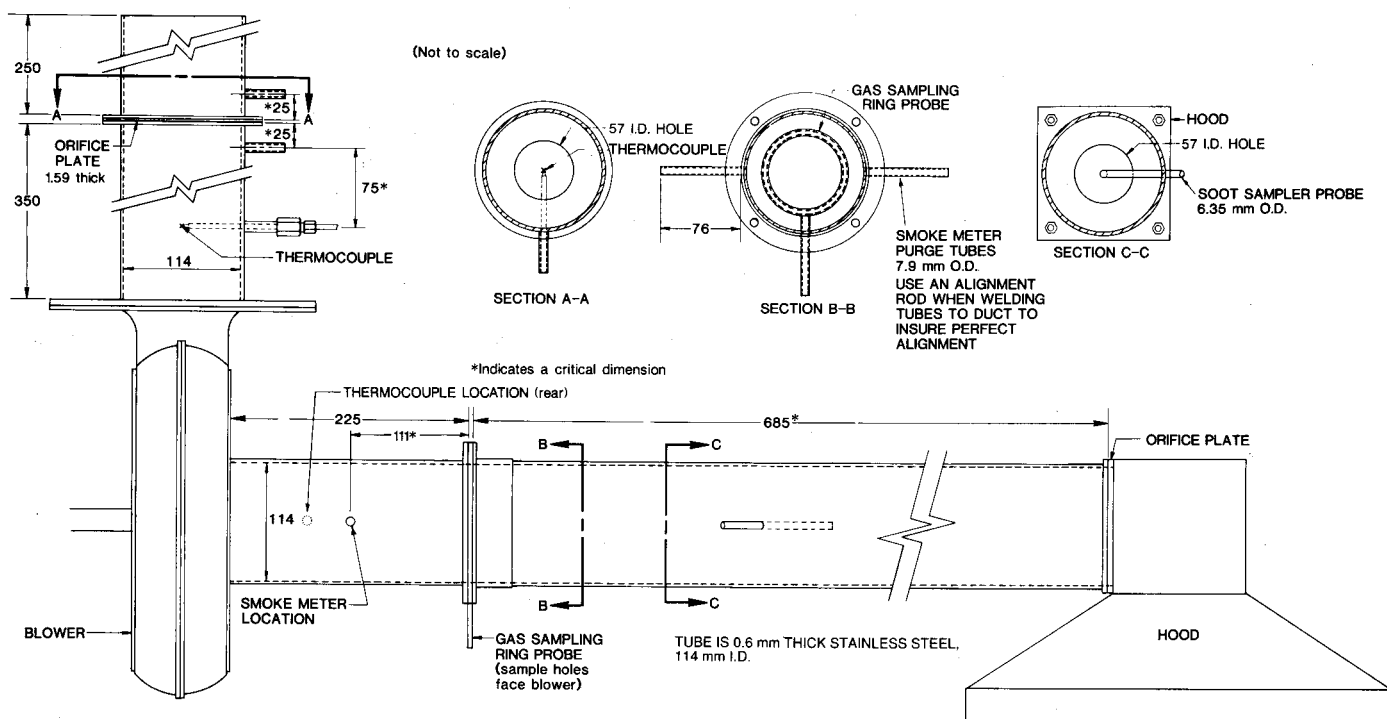
6.4.2 A restrictive orifice (57 mm inside diameter) shall be located between the hood and the duct to promote mixing.

6.4.3 A ring sampler shall be located in the fan intake duct for gas sampling, 685 mm from the hood (Fig. 1). The ring sampler shall contain twelve holes to average the stream composition with the holes facing away from the flow to avoid soot clogging.

6.4.4 The temperature of the gas stream shall be measured using a 1.0 to 1.6 mm outside diameter sheathed-junction thermocouple or a 3 mm outside diameter exposed junction thermocouple positioned in the exhaust stack on the centerline and 100 mm upstream from the measuring orifice plate.

6.4.5 The flow rate shall be determined by measuring the differential pressure across a sharp-edged orifice (57 mm inside diameter) in the exhaust stack, at least 350 mm downstream from the fan when the latter is located as shown in Fig. 5.

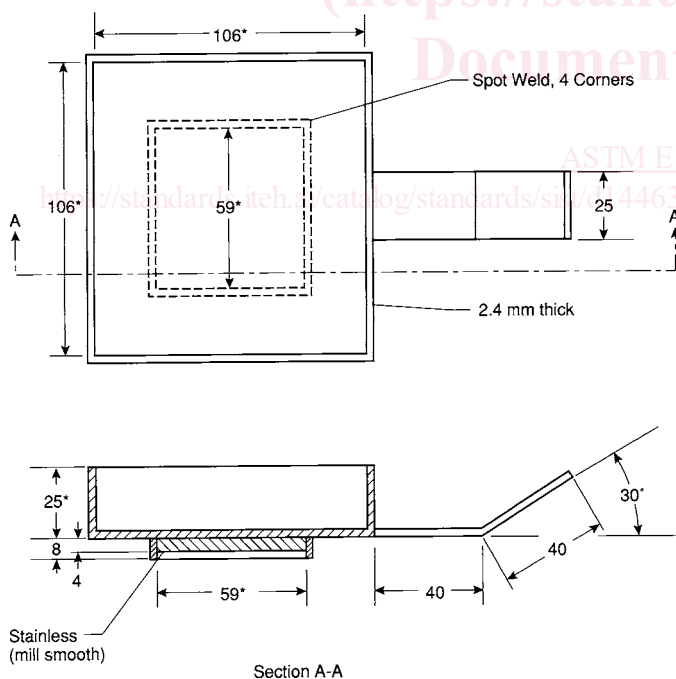
6.4.6 In other details, the geometry of the exhaust system is not critical. Where necessary, small deviations from the recommended dimensions given in Fig. 5 shall be permitted to be made. The inner diameter of the duct and the orifice plates is not a critical dimension. Also the fan does not need to be at the exact location as indicated on Fig. 5, but shall be permitted to be further downstream, allowing for a more common type of fan to be used. In this case, sufficient undisturbed inflow



NOTE—All dimensions are in millimetres (not to scale).

NOTE 1—All dimensions are in millimetres (not to scale).

FIG. 5 Exhaust System



NOTE 1—All dimensions are in millimetres.

NOTE 2—\* Indicates a critical dimension.

FIG. 6 Horizontal Specimen Holder

distances to the gas sampling probe and the measuring orifice shall be provided for the flow to be uniformly mixed.

6.5 *Load Cell*—The general arrangement of the specimen holders on the load cell is indicated in Fig. 3 and Fig. 4. The load cell shall have an accuracy of 0.1 g, and shall have a total weighing range of at least 3.5 kg of which at least 500 g shall be available for direct monitoring during any single test.

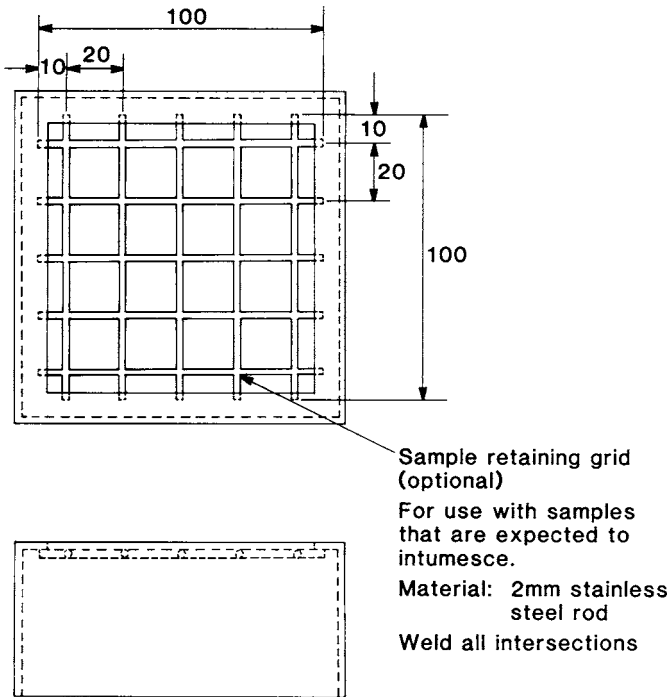
6.6 *Specimen Mounting*:

6.6.1 The horizontal specimen holder is shown in Fig. 6.

6.6.2 The bottom of the horizontal specimen holder shall be lined with a layer of low density (nominal density 65 kg/m<sup>3</sup>) refractory fiber blanket with a thickness of at least 13 mm. The distance between the bottom surface of the cone heater and the top of the specimen shall be adjusted to be 25 mm except as indicated in 6.6.2.1. For mechanisms constructed according to the drawing in Fig. 2, this is accomplished by using the sliding cone height adjustment.

6.6.2.1 Materials that intumesce or deform to such an extent that they make physical contact with either (a) the spark plug before ignition or (b) the underside of the cone heater after ignition shall be tested by adjusting the distance between the bottom surface of the cone heater and the top of the specimen to 60 mm, or as described in 6.6.4.

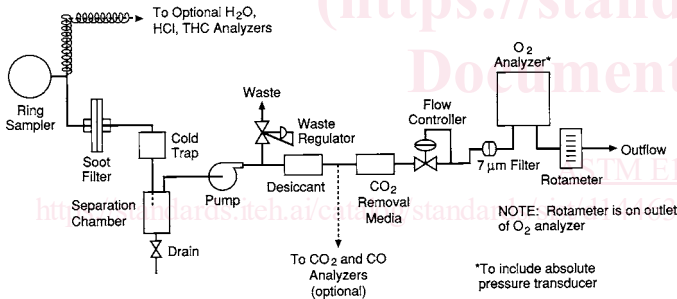




Material: Stainless steel, 1.9 mm thick

NOTE 1—All dimensions are in millimetres.

FIG. 8 Optional Wire Grid (For Horizontal or Vertical Orientation)



NOTE 1—Rotameter is on outlet of the oxygen (O<sub>2</sub>) analyzer.

FIG. 9 Gas Analyzer Instrumentation

6.6.4.2 Use a wire grid (Fig. 8), whether testing is conducted in the horizontal or in the vertical orientations.

NOTE 2—The wire grid is used for retaining specimens prone to delamination and is suitable for several types of intumescent specimens.

6.6.4.3 Use a separation distance between the cone base plate and the upper specimen surface of 60 mm instead of 25 mm. Use this technique for those dimensionally unstable materials that have the potential to intumesce or deform to such an extent that they are likely to make physical contact with either (a) the spark plug before ignition or (b) the underside of the cone heater after ignition.

6.6.4.4 Use a special mounting procedure suitable for the specimen to be tested.

6.6.5 Unstable materials that warp so that the exposed surface of the test specimen is not flat during testing shall be restrained to maintain the surface in a flat orientation. This

shall be accomplished with four tie wires, as described in 6.6.5.1 through 6.6.5.4.

6.6.5.1 The four tie wires shall be metal wires,  $1.0 \pm 0.1$  mm in diameter and at least 350 mm long.

6.6.5.2 The test specimen shall be prepared as described in Section 8 and then tied with the metal wires.

6.6.5.3 A tie wire shall be looped around the specimen holder assembly so that it is parallel to and  $20 \pm 2$  mm away from any of the four sides of the assembly. The ends of the tie wire shall be twisted together such that the wire is pulled firmly against the specimen holder assembly. Trim excess wire from the twisted section before testing.

6.6.5.4 Fit the other three tie wires around the specimen holder assembly in a similar manner, so that each one is parallel to one of the sides of the assembly.

6.6.6 Melting Materials:

6.6.6.1 Materials that melt and overflow the aluminum foil wrapping (see 8.1.1) during testing shall be tested using aluminum foil that extends above the specimen surface level.

The aluminum foil extension above the specimen surface shall be such that melt overflow is contained, without interfering with the combustion process. A height of 2-3 mm is recommended.

6.6.6.2 If a test has been conducted as indicated in 8.1.1 without using the special technique described in 6.6.6.1 and melt overflow has occurred, that test shall be deemed invalid and the technique in 6.6.6.1 shall be used for future tests.

6.7 Radiation Shield—The cone heater shall be provided with a removable radiation shield to protect the specimen from the initial test heat flux prior to the start of a test. The shield shall be made of noncombustible material with a total thickness not to exceed 12 mm. The shield shall be one of the following:

- (a) water cooled and coated with a durable matte black finish of surface emissivity  $e = 0.95 \pm 0.05$  or
- (b) not water cooled with a metallic reflective top surface to minimize radiation transfer.

(c) not water-cooled, with a ceramic, non-metallic, surface that minimizes radiation transfer to the specimen surface.

The shield shall be equipped with a handle or other suitable means for quick insertion and removal. The cone heater base plate shall be equipped with the means for holding the shield in position and allowing its easy and quick removal.

6.8 Ignition Circuit—External ignition is accomplished by a 10-kV discharge across a 3-mm spark gap located 13 mm above the center of the specimen in the horizontal location; in the vertical orientation the gap is located in the specimen face plane and 5 mm above the top of the holder. A suitable power source is a transformer designed for spark-ignition use or a spark generator. The high voltage connections to the spark electrodes shall not be grounded to the chassis in order to minimize interference with the data-transmission lines. For testing with electric spark ignition, spark discharge shall be continuously operating at 50 to 60 Hz until sustained flaming is achieved. The ignitor shall be removed when sustained flaming is achieved.

6.9 Ignition Timer—The timing device for measuring time to sustained flaming shall be capable of recording elapsed time to the nearest second and shall be accurate to within 1 s in 1 h.

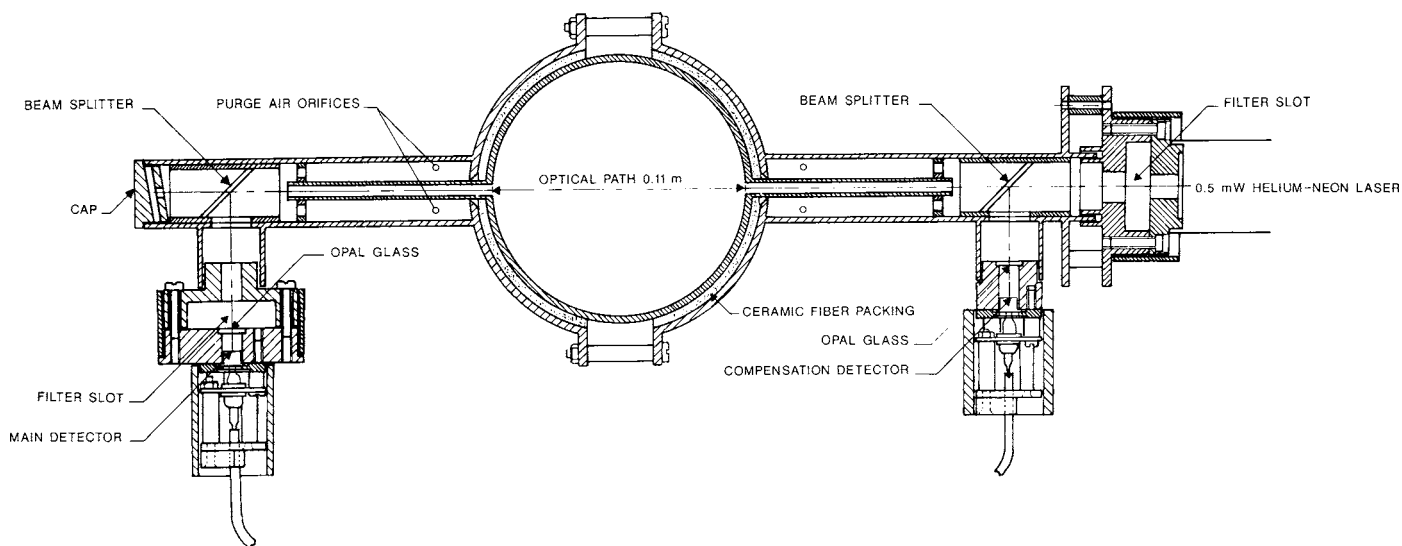
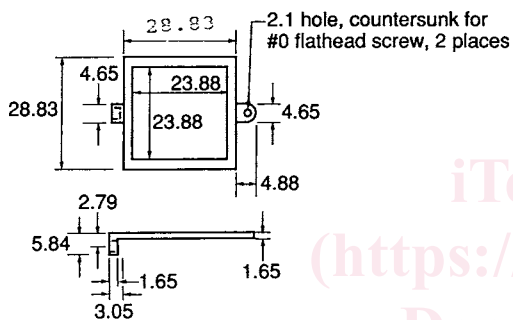
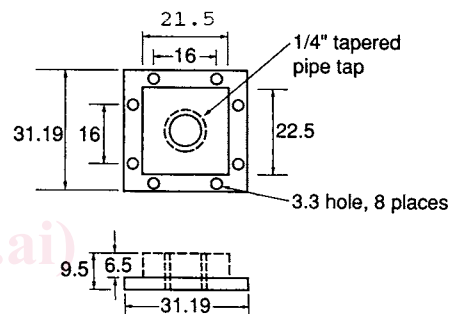


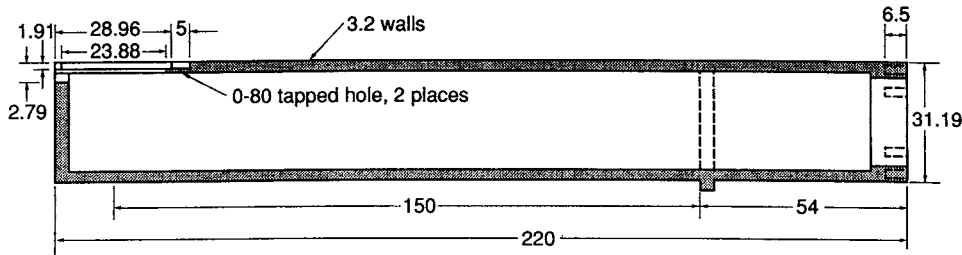
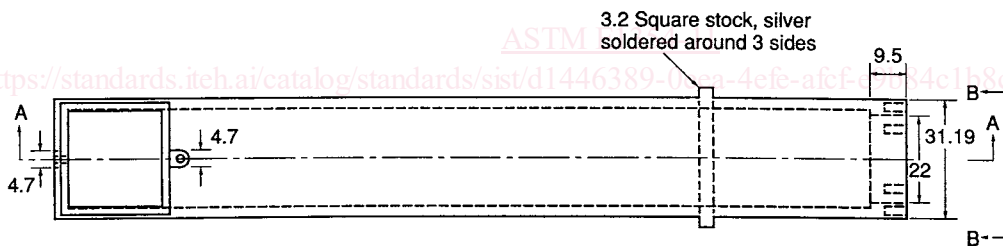
FIG. 10 Smoke Obscuration Measuring System



SCREEN RETAINING RING (brass)

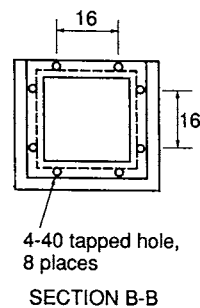


END CAP (brass)



BURNER MAIN BODY (brass)

Pack burner with ceramic fiber batting



SECTION B-B

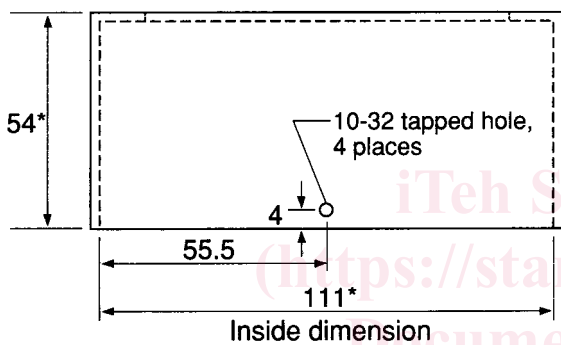
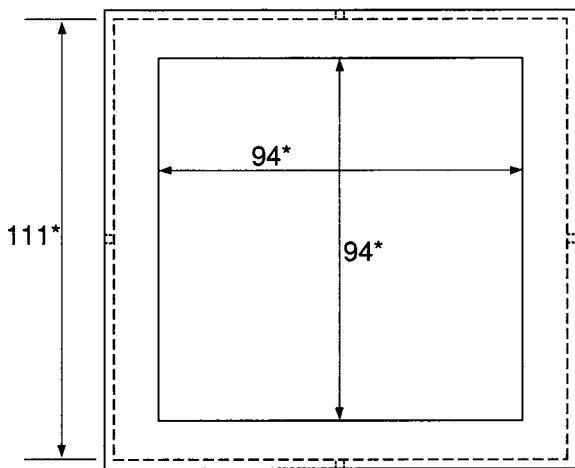
NOTE 1—All dimensions are in millimetres except where noted.

FIG. 11 Calibration Burner

6.10 Gas Sampling—Gas sampling arrangements are shown in Fig. 9. They shall incorporate a pump, a filter to prevent

entry of soot, a cold trap to remove most of the moisture, a bypass system set to divert all flow except that required for the





(stainless steel, 1.9 mm thick)

NOTE 1—All dimensions are in millimetres.

NOTE 2—\* Indicates a critical dimension.

FIG. 12 Optional Retainer Frame for Horizontal Orientation Testing

oxygen analyzer, a further moisture trap, and a trap for carbon dioxide (CO<sub>2</sub>) removal; the latter if CO<sub>2</sub> is not measured. When a CO<sub>2</sub> trap is used, the sample stream entering the oxygen analyzer must be fully dry; some designs of CO<sub>2</sub> traps require an additional moisture trap downstream of the CO<sub>2</sub> trap.

NOTE 3—If an optional CO<sub>2</sub> analyzer is used instead of removing CO<sub>2</sub> from the oxygen analyzer stream, the equations to calculate the rate of heat release will be different from those for the standard case (Section 12) and are, instead, given in Annex A1.

6.11 *Oxygen Analyzer*—The analyzer shall be of the paramagnetic type with a range from 0 to 25 % oxygen. The analyzer shall exhibit a linear response and drift of not more than ±50 ppm of oxygen over a period of 30 min, and noise of not more than 50 ppm of oxygen (root-mean-square value) during this same 30 min period. Since oxygen analyzers are sensitive to stream pressures, the stream pressure shall be regulated (upstream of the analyzer) to allow for flow fluctuations, and the readings from the analyzer compensated with an absolute pressure regulator to allow for atmospheric pressure

variations. The analyzer and the absolute pressure regulator shall be located in a constant-temperature environment. The oxygen analyzer shall have a 10 to 90 % response time of less than 12 s.

6.12 *Smoke Obscuration Measuring System*—The smoke measuring system (Fig. 10) comprises a helium-neon laser, silicon photodiodes as main beam and reference detectors, and appropriate electronics to derive the extinction coefficient and to set the zero reading. The system is designed to be resiliently attached to the exhaust duct by means of refractory gasketing, at the location shown in Fig. 5. This shall be achieved by one of the following options: (a) the use of an optical bench, or (b) the use of a split yoke mounting comprising two pieces that are rigidly screwed together. The meter is located in place by means of two small-diameter tubes welded onto each side of the exhaust duct. These serve as part of the light baffling for the air purging and also serve to aid in the desposition on the tube walls of any smoke that enters despite the purge flow, so that it does not reach the optical elements.

6.13 *Heat Flux Meter:*

6.13.1 The total heat fluxmeter shall be of the Gardon (foil) or Schmidt-Boelter (thermopile) type with a design range of about 100 kW/m<sup>2</sup>. The sensing surface of the fluxmeter shall be flat, circular, approximately 12.5 mm in diameter, and coated with a durable matte-black finish. The fluxmeter shall be water cooled. Radiation shall not pass through any window before reaching the sensing surface. The instrument shall be robust, simple to set up and use, and stable in calibration. The instrument shall have an accuracy of within ±3 %.

6.13.2 The calibration of the heat fluxmeter shall be checked whenever a recalibration of the apparatus is carried out by comparison with an instrument (of the same type as the working heat fluxmeter and of similar range) held as a reference standard and not used for any other purpose. The reference standard shall be fully calibrated at a standardizing laboratory at yearly intervals.

6.13.3 This meter shall be used to calibrate the heater temperature controller (Fig. 3 and Fig. 4). It shall be positioned at a location equivalent to the center of the specimen face in either orientation during this calibration.

6.14 *Calibration Burner*—To calibrate the rate of heat release apparatus, a burner is used (Fig. 3 and Fig. 4). The burner is constructed from a square-section brass tube with a square orifice covered with wire gauze through which the methane diffuses (Fig. 11). The tube is packed with ceramic fiber to improve uniformity of flow. The calibration burner is suitably connected to a metered supply of methane of at least 99.5 % purity.

6.15 *Optical Calibration Filters*—Glass neutral density filters, of at least two different values accurately calibrated at the laser wavelength of 0.6328 μm, are required.

6.16 *Digital Data Collection*—The data collection system used must have facilities for the recording of the output from the oxygen analyzer, the orifice meter, the thermocouples, the load cell, and the smoke measuring system. The data collection system shall have an accuracy corresponding to at least 50 ppm oxygen for the oxygen channel, 0.5°C for the temperature measuring channels, and 0.01 % of full-scale instrument output

for all other instrument channels. The system shall be capable of recording data at intervals not exceeding 5 s.

## 7. Hazards

7.1 The test procedures involve high temperatures and combustion processes. Therefore, hazards exist for burns, ignition of extraneous objects or clothing, and for inhalation of combustion products. The operator shall use protective gloves for insertion and removal of test specimens. Neither the cone heater nor the associated fixtures shall be touched while hot except with the use of protective gloves. The possibility of the violent ejection of molten hot material or sharp fragments from some kinds of specimens when irradiated cannot totally be discounted and eye protection shall be worn.

7.2 The exhaust system shall be checked for proper operation before testing and must discharge into a building exhaust system with adequate capacity. Provision shall be made for collecting and venting any combustion products that are not collected by the normal exhaust system of the apparatus.

## 8. Test Specimens

### 8.1 Size and Preparation:

8.1.1 Test specimens shall be 100 by 100 mm in area, up to 50-mm thick, and cut to be representative of the construction of the end-use product. For products of normal thickness greater than 50 mm, the requisite specimens shall be obtained by cutting away the unexposed face to reduce the thickness to 50 mm. For testing, wrap specimens in a single layer of aluminum foil, shiny side toward the specimen, covering the sides and bottom. Foil thickness shall be 0.025 to 0.04 mm.

8.1.2 Expose composite specimens in a manner typical of the end-use condition. Prepare them so the sides are covered with the outer layer(s) or otherwise protected.

8.1.3 Some materials, including composites, intumescent materials, other dimensionally unstable materials, materials that warp during testing and materials that melt and overflow the aluminum foil (8.1.1) during testing, require special mounting and retaining techniques to retain them adequately within the specimen holder during combustion. Section 6.6 describes some of the key techniques. The exact mounting and retaining method used shall be specified in the test report. Additional specialized guidance to the operator is provided in Ref (2).

8.1.4 Assemblies shall be tested as specified in 8.1.2 or 8.1.3 as appropriate. However, where thin materials or composites are used in the fabrication of an assembly, the presence of an air gap or the nature of any underlying construction often significantly affects the ignition and burning characteristics of the exposed surface. The influence of the underlying layers must be understood and care taken to ensure that the test result obtained on any assembly is relevant to its use in practice. When the product is a material or composite that is normally attached to a well defined substrate, it shall be tested in conjunction with that substrate, using the recommended fixing technique, for example, bonded with the appropriate adhesive or mechanically fixed.

8.1.5 Products that are thinner than 6 mm shall be tested with a substrate representative of end use conditions, such that the total specimen thickness is 6 mm or more. In the case of specimens of less than 6 mm in thickness and that are used with

an air space adjacent to the unexposed face, the specimens shall be mounted so that there is an air space of at least 12 mm between its unexposed face and the refractory fibre blanket. This is achieved by the use of a metal spacer frame.

8.2 *Conditioning*—Specimens shall be conditioned to moisture equilibrium (constant weight) at an ambient temperature of  $23 \pm 3^\circ\text{C}$  and a relative humidity of  $50 \pm 5\%$ .

## 9. Test Environment

9.1 The apparatus shall be located in a draft-free environment in an atmosphere of relative humidity of between 20 and 80 % and a temperature between 15 and  $30^\circ\text{C}$ .

## 10. Calibration of Apparatus

10.1 *Heater Flux Calibration*—Set the temperature controller to the required flux by using the heat fluxmeter at the start of the test day, after changing to a new flux level, or when the cone-heater orientation or the distance between the cone heater and the top of the specimen is changed. Do not use a specimen holder when the heat fluxmeter is inserted into the calibration position. Operate the cone heater for at least 10 min and ensure that the controller is within its proportional band before beginning this calibration.

10.1.1 Calibrate the heat flux by placing the heat fluxmeter at the same distance from the base plate of the cone heater as the upper surface of the specimen will be placed during testing. This will normally be a distance of 25 mm. However, under certain circumstances, this distance will be different, depending on the specimen mounting (see 6.6).

10.1.2 Note that times to sustained flaming measured with different distances between the base plate of the cone heater and the upper surface of the specimen are likely to be different.

### 10.2 Oxygen Analyzer Calibration:

#### 10.2.1 Preliminary Calibrations:

10.2.1.1 The oxygen analyzer delay time must be determined. This is done by arranging for a methane flow rate equivalent to 5 kW to the calibration burner. The heater shall not be turned on for this calibration. Record the output of the analyzer as the methane supply, turned on and ignited, reaches a steady value, and then returns to baseline after the supply is cut off. Record the temperature for the exhaust-orifice meter at the same time. Determine the turn-on delay as the time difference between the time when the temperature reading reaches 50 % of its ultimate deflection and the time when the oxygen reading reaches 50 % of its ultimate deflection. Determine the turn-off delay similarly at turn-off. Take the delay time as the average of the turn-on delay and turn-off delay. Use this value,  $t_d$ , subsequently to time-shift all the oxygen readings.

10.2.1.2 If the oxygen analyzer is equipped with an electric response-time adjustment, set it so that at turn-off there is just a trace of overshoot when switching rapidly between two different calibration gases.

10.2.1.3 The timing of the scans by the data collection system shall be calibrated with a timer accurate to within 1 s in 1 h. The data output shall show event times correct to 3 s.

10.2.2 *Operating Calibrations*—At the start of testing each day, the oxygen analyzer shall be zeroed and calibrated. For zeroing, the analyzer shall be fed with nitrogen gas with the