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Mechanical joining of sheet materials — Destructive testing of joints — Specimen dimensions and procedure for mechanized peel testing of single joints

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Foreword

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This document was prepared by Technical Committee ISO/TC 44, Welding and allied processes, Subcommittee SC 6, Resistance welding and allied mechanical joining.

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Official interpretations of ISO/TC 44 documents, where they exist, are available from this page: <u>https://committee.iso.org/sites/tc44/home/interpretation.html</u>.

Mechanical joining of sheet materials — Destructive testing of joints — Specimen dimensions and procedure for mechanized peel testing of single joints

1 Scope

This document specifies the geometry of test specimens and the testing procedure for mechanized peel testing of single mechanical joints on single-lap test specimens up to a single sheet thickness of 4,5 mm.

The term "sheet", as used in this document, includes extrusions and cast materials.

The purpose of the mechanized peel tests is to determine the mechanical characteristics and the failure modes of the joints made with different joining methods.

This document does not apply to civil engineering applications such as metal buildings and steel constructions which are covered by other application standards.

NOTE For mechanized peel testing of resistance spot, seam and embossed projection welds, see ISO 14270

2 Normative references **STANDARD PREVIEW**

There are no normative references in this document teh.ai)

3 Terms and definitions

https://standards.iteh.ai/catalog/standards/sist/f46ad3c8-e4e6-4f21-8e0a-

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

— ISO Online browsing platform: available at <u>https://www.iso.org/obp</u>

— IEC Electropedia: available at <u>http://www.electropedia.org/</u>

3.1 mechanized peel strength MPS

F_{max}

maximum *peel force* (3.2) obtained from mechanized peel testing

3.2 peel force

force/load which is applied to the test specimen during mechanized peel testing

3.3

slippage force

 F_{sl} peel force (3.2)/load at which slippage occurs if the phenomenon is observed during testing

3.4 specimen deformation

specimen deformation

crosshead displacement during testing

3.5

specimen deformation at maximum load

 S_{Fmax} specimen deformation (3.4) at which the maximum peel force (3.2)/load F_{max} is recorded

Note 1 to entry: See Figure 4 and Figure 5

3.6

specimen deformation at 0,3 $F_{\rm max}$

 $s_{0,3Fmax}$ specimen deformation (<u>3.4</u>) at which $0,3F_{max}$ is recorded

Note 1 to entry: See Figure 4 and Figure 5

3.7

specimen deformation at fracture

 s_{fracture} specimen deformation (3.4) of at which fracture occurs

Note 1 to entry: See Figure 4 and Figure 5

3.8

dissipated energy

W

amount of energy dissipated until a displacement point under the load-crosshead displacement curve

[SOURCE: ISO 12161, 3.4.1] **iTeh STANDARD PREVIEW**

3.9

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dissipated energy up to F_{max} W_{Fmax}

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dissipated energy or work calculated by integrating the area under the crosshead displacement curve up to the point at which maximum peal load (MPS point) is recorded

$$W_{F\max} = \int_0^{s_{F\max}} F \, ds$$

3.10 dissipated energy up to 0,3 F_{max}

$W_{0.3Fmax}$

dissipated energy or work calculated by integrating the area under the crosshead displacement curve up to the point where the peel force drops to 30 % of the MPS value, F_{max}

$$W_{0,3F\max} = \int_0^{s_{0,3F\max}} F \, ds$$

Note 1 to entry: See <u>Clause 6</u>

3.11 dissipated energy up to fracture

W_{fracture}

dissipated energy calculated by integrating the crosshead displacement curve up to the point at which fracture occurs

$$W_{\text{fracture}} = \int_0^{s_{\text{fracture}}} F \, ds$$

4 Test pieces and test specimens

<u>Table 1</u> and <u>Figure 1</u> give the dimensions and form of test coupons and test specimens for mechanized peel testing, and the location of mechanical joint. The positional accuracy of the mechanical joints on the test specimen shall be ± 1 mm in every direction.

Table 1 — Test specimen dimensions and joint position

Dimensions in millimetres

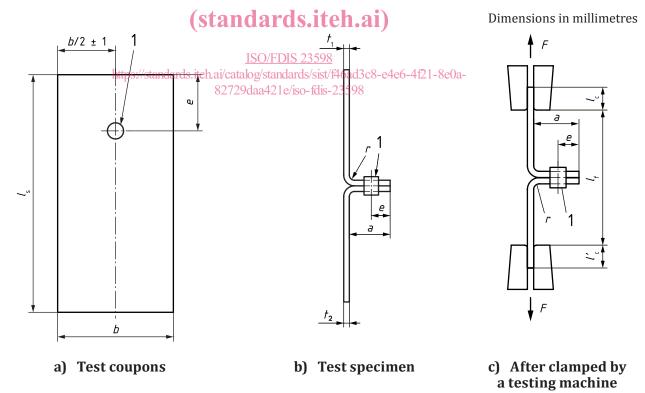
| Thickness | Flange length | Specimen width | Coupon length ^a | Free length be- tween clamps ^a | Edge distance |
|--|------------------|-------------------|-------------------------------|--|---------------|
| t | а | b | ls | $l_{\rm f}$ | е |
| | ≤ 4,5 50 | 50 | 100 | 30 | 25 |
| $0,5 < t \le 4,5$ | | | ≥160 | 105 | |
| The shorter coupon length (before joining) is preferred but a longer specimen can be needed based on joining process | | | | | |

limitations or for comparison with results from testing in accordance with ISO 14270.

The test specimen for mechanical joints shall be produced as a single joint specimen as shown in Figure 1 b), which is made of two coupons shown in Figure 1 a), and then the mechanized peel test specimen shall be mounted on a tensile test machine as shown in Figure 1 c).

In the case of unequal sheet thicknesses, the test specimen dimensions shall be based on the thinner sheet. Mechanized peel testing shall be made by the procedure specified in <u>Clause 5</u> and <u>Clause 6</u>.

The tolerances on the dimensions shall be in accordance with Table 2.



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| Key | | | |
|----------------------------------|----------------------------|---|-----------------------|
| 1 | joint/fastener | а | flange length |
| l _s | coupon length | r | bending radius |
| $l_{\rm f}$ | free length between clamps | b | coupon/specimen width |
| l _c , l' _c | clamping length | е | edge distance |
| F | applied force (load) | | |

Figure 1 — Test coupons, test specimens and the clamping state for mechanized peel testing

Table 2 — Tolerances on dimensions for mechanized peel test specimens

Dimensions in millimetres

| Flange length | Coupon/ specimen width | Edge distance | Coupon length | Free length be- tween clamps | Bend radius |
|--|---------------------------|------------------|------------------|---------------------------------|-----------------------------|
| а | b | е | l _s | $l_{\rm f}$ | r |
| +1,0 0 | +1 0 | +0,5 0 | 0 -1 | 0 -1 | ± 0,5 <i>t</i> ^a |
| ^a <i>t</i> is the sheet thickness of each coupon. | | | | | |

5 Preparation of mechanized peel test specimens

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5.1 General

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The mechanized peel test specimens for mechanical joints are recommended to be made in the following sequence, so that the test specimens can be tested using a tensile test machine;

 $Bending \rightarrow Mechanical joining \rightarrow Mechanized peel testing \\ 82/29 daa421e/iso-idis-2598$

The sequence is called "joining-after-bending process".

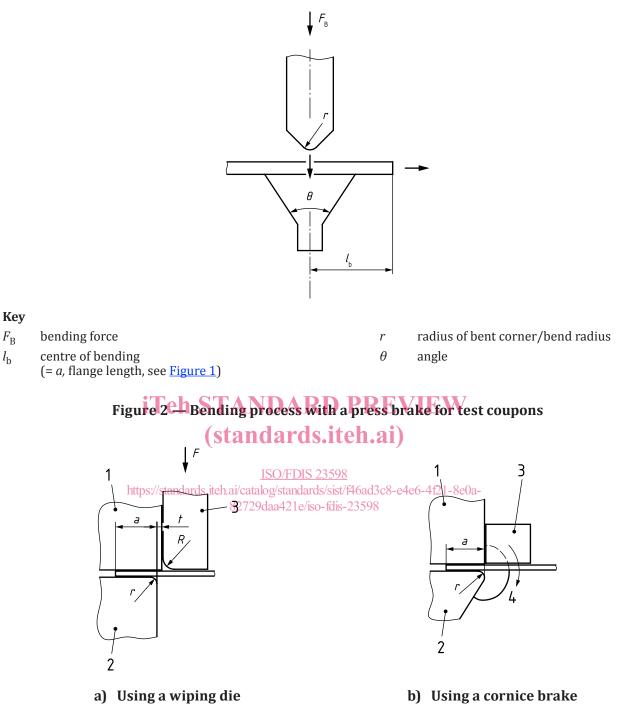
NOTE In resistance spot welding, the bending-after-welding process (Joining \rightarrow Bending \rightarrow Mechanized peel testing) can be used, but in the case of mechanical joining, some fasteners cannot be tested using this sequence as the fastener interferes with the clamping face for bending after joining, or the clamping device can influence the joint part properties.

5.2 Bending procedure for preparation of peel test specimens

The test coupons shall be bent before mechanical joining as shown in Figure 2.

The recommended set-up conditions of jigs for bending with a press brake are shown in **B.1**.

NOTE When setting the value $l_b = a$ as shown in Figure 2, the maximum error in the flange length is less than ±0,5 mm if r = 2t and $t \le 4,5$ mm (see detail in Annex C).





 $l_{\rm b}$

- 1 upper jaw
- 2 lower jaw
- 3 die
- 4 rotating

- F force r radius of bent corner R edge radius of die flange length а
- Figure 3 Examples of edge bending

A mechanized press brake system is generally recommended for the bending although a manual press brake can be used to bend test coupons for soft and thinner test pieces. Other bending tools shown in Figure 3 are also applicable to make the test coupons. The wiping die and cornice brake system can be used. An example of edge bending is shown in Annex B.

5.3 Dimensions and accuracy of bent radius

The value of the inner radius, *r*, shall be set so that no large and deep cracking occurs during bending on the inner or outer surfaces of the bent corner. The radius value tested shall be recorded. The inner radius *r*, equal to approximately 2*t* (*t*, plate thickness) is recommended. Tolerances shall be in accordance with Table 2.

If any cracks are visible, with up to $\times 5$ magnification, after bending in accordance with <u>5.2</u>, new test specimens/coupons with larger inner radii shall be made. The value of the inner radius shall be increased until no cracking occurs on the outer side of the bend.

6 Testing procedure and test equipment

The test specimen is clamped in a tensile testing machine which satisfies the requirements of ISO 7500-1, such that the clamps are at the required distance from one another as shown in Figure 1 c). Force and crosshead displacement shall be measured simultaneously during testing, and the measuring accuracy shall be ± 1 %. All tests shall be performed at room temperature until the joint fails.

If a special clamping device is used, the shape and size shall be specified in a joining procedure specification (JPS) document, and recorded.

The crosshead displacement rate of the testing machine shall be equal to 10 mm/min or less, and shall be kept constant during testing.

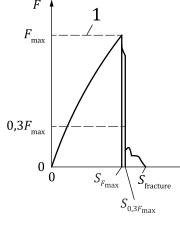
The specimen deformation shall be measured either as the crosshead displacement, or by using an appropriate displacement sensing device directly at the specimen. When using a signal from the crosshead position, it should be corrected for the stiffness of the testing machine. Results can only be compared when performed under similar displacement measuring conditions. The type of measurement and the initial measured length shall be noted in the test report.

The signals for load and specimen deformation during testing shall be recorded as shown in Figure 4, so that at least the peak value of the maximum force is recorded as the MPS in the test report.

NOTE 1 If required, further characteristic data, e.g. W_{Fmax} , $W_{0,3Fmax}$ and $W_{fracture}$, etc. can be determined from the load-elongation curve (see Figure 4).

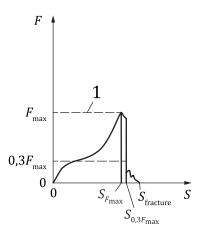
Test specimens for mechanized peel testing, as shown in <u>Figure 2b</u>), shall be made with a mechanical joining machine. The recommended set-up conditions of jigs for bending with a press brake are shown in <u>B.1</u>.

NOTE 2 When setting the value $l_b = a$ as shown in Figure 2, the maximum error in the flange length is less than ±0,5 mm if r = 2t and $t \le 4,5$ mm (see detail in Annex C).



b) Example 1

S

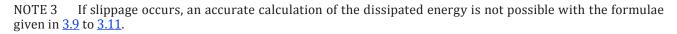


b) Example 2

| Key | | | |
|------------------|-----------------------------------|-----------------------|--|
| 1 | mechanized peel strength | $S_{F \max}$ | specimen deformation at maximum load |
| F | load /applied force | S _{0,3 Fmax} | specimen deformation at 0,3 $F_{\rm max}$ |
| S | elongation/crosshead displacement | S _{fracture} | specimen deformation of at which fracture occurs |
| F _{max} | mechanized peel strength | | |

Figure 4 — Examples of load-elongation/crosshead displacement curves without slippage (not to scale)

If slippage occurs during the mechanized peel test (See Figure 5), the slippage load is also recorded in the test report.



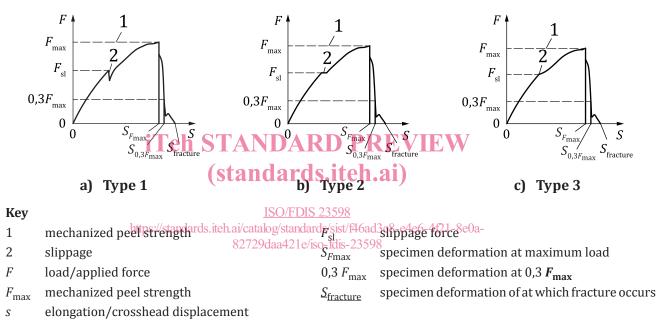


Figure 5 — Examples of possible slippage recorded on the load-elongation curves (not to scale)

7 Type of failure mode

The type of failure mode after mechanized peel testing shall be classified in accordance with <u>Annex A</u>, and recorded in the test report.

8 Re-test

If fracture occurs only from the bent corner of test specimens during mechanized peel testing in accordance with <u>Clause 6</u>, all mechanized test results shall be disregarded, and new test specimens with larger inner radius shall be made and tested. The value of the inner radius shall be increased until no fracture occurs from the bent part, especially the location of cracks appearing on the bent corner of test specimens. When using larger radii, the radius value tested shall be recorded.

If slippage occurs during the peel test and the slippage load is lower than the required value, re-tests are required with new test specimens after a re-design of the joints, re-selection of the joining technology and/or an improved joining process.