



SLOVENSKI STANDARD
oSIST prEN IEC 60034-12:2023
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Električni rotacijski stroji - 12. del: Zagonska zmogljivost indukcijskih motorjev s trifazno kletko z eno hitrostjo

Rotating electrical machines - Part 12: Starting performance of single-speed three-phase cage induction motors

Drehende elektrische Maschinen - Teil 12: Anlaufverhalten von Drehstrommotoren mit Käfigläufer ausgenommen polumschaltbare Motoren

Machines électriques tournantes - Partie 12: Caractéristiques de démarrage des moteurs triphasés à induction à cage à une seule vitesse

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OF INTEREST TO THE FOLLOWING COMMITTEES: TC 9	PROPOSED HORIZONTAL STANDARD: <input type="checkbox"/> Other TC/SCs are requested to indicate their interest, if any, in this CDV to the secretary.
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TITLE: Rotating electrical machines – Part 12: Starting performance of single-speed three-phase cage induction motors

PROPOSED STABILITY DATE: 2026

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CONTENTS

FOREWORD	3
1 Scope	5
2 Normative references	5
3 Terms and definitions	6
4 Symbols	7
5 Designation	7
5.1 General.....	7
5.2 Design N.....	7
5.3 Design NE	8
5.4 Designs NY and NEY	8
5.5 Design H.....	8
5.6 Design HE	8
5.7 Designs HY and HEY	8
6 Design N requirements	8
6.1 Torque characteristics.....	8
6.2 Locked rotor current and apparent power	8
6.3 Starting requirements.....	9
7 Design NE starting requirements	9
8 Designs NY and NEY starting requirements	9
9 Design H requirements	9
9.1 Starting torque	9
9.2 Locked rotor current and apparent power	9
9.3 Starting requirements.....	10
10 Design HE starting requirements	10
11 Designs HY and HEY starting requirements	10
12 Determination of current and torque from measurement.....	10
12.1 Locked-rotor current and locked-rotor torque	10
12.2 Breakdown torque	10
12.3 Torque-speed curve and current-speed curve	11
12.3.1 Torque-speed and current-speed curves from direct measurement (method a).....	11
12.3.2 Torque-speed and current-speed curves from acceleration (method b)	11
12.3.3 Torque-speed and current-speed curves from measured input power (method c)	12
12.4 Correction of data for tests performed at reduced voltage and/or other than rated frequency.....	12
Annex A Current and torque characteristics with locked rotor (informative)	17
Annex B Correction method for test done on reduced voltage (informative).....	20
Table 1 – Minimum values of torques for design N	13
Table 2 – Maximum values of locked rotor apparent power for designs N and H	13
Table 3 – Maximum values of locked rotor apparent power for designs NE and HE.....	13
Table 4 – External moment of inertia (J).....	14
Table 5 – Minimum values of torques for design H	15
Table 6 – Minimum values of torques for design N motors with type of protection 'Ex eb – increased safety'	15
Table 7 – External moment of inertia (J) for motors with type of protection 'Ex eb – increased safety'	16

INTERNATIONAL ELECTROTECHNICAL COMMISSION

ROTATING ELECTRICAL MACHINES –**Part 12: Starting performance of single-speed
three-phase cage induction motors**

FOREWORD

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International Standard IEC 60034-12 has been prepared by IEC technical committee 2: Rotating machinery.

This fourth edition cancels and replaces the second edition, published in 2016. It constitutes a technical revision.

The main technical changes with regard to the previous edition are as follows:

Clause or subclause	Change
Table 6	Aligned with the requirements for explosion protected motors from TC31 WG27
12	New clause on methods for measuring locked-rotor current and torque
Annex A	New informative annex on the general current and torque characteristics with locked rotor
Annex B	New informative annex on correction of voltage and frequency

The text of this standard is based on the following documents:

CDV	Report on voting
2/1789/CDV	2/1821A/RVC

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts of the IEC 60034 series, published under the general title *Rotating electrical machines*, can be found on the IEC website.

NOTE A table of cross-references of all IEC TC 2 publications can be found in the IEC TC 2 dashboard on the IEC website.

The committee has decided that the contents of this publication will remain unchanged until the stability date indicated on the IEC website under "http://webstore.iec.ch" in the data related to the specific publication. At this date, the publication will be

- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

ROTATING ELECTRICAL MACHINES –

Part 12: Starting performance of single-speed three-phase cage induction motors

1 Scope

This part of IEC 60034 specifies the parameters for eight designs of starting performance of single-speed three-phase 50 Hz or 60 Hz cage induction motors in accordance with IEC 60034-1 that:

- have a rated voltage up to 1 000 V;
- are intended for direct-on-line or star-delta starting;
- are rated on the basis of duty type S1;
- are constructed to any degree of protection as defined in IEC 60034-5 and explosion protection.

This document also applies to dual voltage motors provided that the flux saturation level is the same for both voltages.

The values of torque, apparent power and current given in this document are limiting values (that is, minimum or maximum without tolerance).

NOTE 1 It is not expected that all manufacturers will produce machines for all eight designs. The selection of any specific design in accordance with this document will be a matter of agreement between the manufacturer and the purchaser.

NOTE 2 Designs other than the eight specified may be necessary for particular applications.

NOTE 3 It should be noted that values given in manufacturers' catalogues may include tolerances in accordance with IEC 60034-1.

NOTE 4 The values tabled for locked rotor apparent power are based on r.m.s. symmetrical steady state locked rotor currents. **The start of the motor leads to transient asymmetrical currents in the whole supply, so called inrush currents**, which may range from 1,8 to 2,8 times the steady state locked rotor value. The current peak and decay time are a function of the motor design and switching angle. **Similar effects can occur during the switchover from star to delta operation. A more detailed description is provided in Annex A.**

NOTE 5 **The application of the test methods described in clause 12 of this standard may be applied to cage induction motors outside the scope of this standard, as well. However, special care must be taken in such cases to prevent overheating of the stator or the rotor winding depending on the concrete method and parameters chosen.**

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60034-30-1, *Rotating electrical machines – Part 30-1: Efficiency classes of line-operated AC motors (IE-code)*

IEC 60079-7:2015, *Explosive atmospheres – Part 7: Equipment protection by increased safety "e"*

44 3 Terms and definitions

45 For the purposes of this document, the following terms and definitions apply.

46 ISO and IEC maintain terminological databases for use in standardization at the following
47 addresses:

- 48 • IEC Electropedia: available at <http://www.electropedia.org/>
- 49 • ISO Online browsing platform: available at <http://www.iso.org/obp>

50 3.1

51 **rated torque**

52 T_N

53 torque the motor develops at its shaft end at rated output and speed

54 [SOURCE: IEC 60050-411:1996, 411-48-05]

55 3.2

56 **locked-rotor torque**

57 T_l

58 smallest measured torque the motor develops at its shaft end with the rotor locked, over all its
59 angular positions, at rated voltage and frequency

60 [SOURCE: IEC 60050-411:1996, 411-48-06]

61 3.3

62 **pull-up torque**

63 T_u

64 smallest steady-state asynchronous torque which the motor develops between zero speed
65 and the speed which corresponds to the breakdown torque, when the motor is supplied at the
66 rated voltage and frequency

67 Note 1 to entry: This definition does not apply to those motors whose torque continually decreases with increase
68 in speed.

69 Note 2 to entry: In addition to the steady-state asynchronous torques, harmonic synchronous torques, which are a
70 function of rotor load angle, will be present at specific speeds. At such speeds, the accelerating torque may be
71 negative for some rotor load angles. Experience and calculation show this to be an unstable operating condition
72 and therefore harmonic synchronous torques do not prevent motor acceleration and are excluded from this
73 definition.

74 3.4

75 **breakdown torque**

76 T_b

77 maximum steady-state asynchronous torque which the motor develops without an abrupt drop
78 in speed, when the motor is supplied at the rated voltage and frequency

79 Note 1 to entry: This definition does not apply to those motors whose torque continually decreases with increase
80 in speed.

81 3.5

82 **rated output**

83 P_N

84 value of the output included in the rating

85 3.6

86 **rated voltage**

87 U_N

88 value of the voltage included in the rating

89 **3.7**90 **locked rotor apparent power**91 S_l 92 apparent power input with the motor held at rest at rated voltage and frequency **after the**
93 **inrush currents have decayed to a symmetrical system of current**94 **3.8**95 **locked rotor current**96 I_l 97 current with the motor held at rest at rated voltage and frequency **after the inrush currents**
98 **have decayed to a symmetrical system of current**99 **4 Symbols**

Symbol	Quantity
I_l	Locked rotor current
J	External moment of inertia
J_M	Moment of inertia of motor under test
n	Rotational speed
p	Number of pole pairs
P_1	Power at the motor terminals during test method c)
$P_{1,g}$	Power at the generator terminals during test method a)
P_{Fe}	Motor iron losses during test method c)
P_L	Motor I ² R losses during test method c)
$P_{T,g}$	Total losses of the generator during test method a)
P_N	Rated output
S_l	Locked rotor apparent power
T_N	Rated torque
T_l	Locked rotor torque
T_u	Pull-up torque
T_b	Breakdown torque
T_{fw}	Motor friction and windage torque during test method c)
U_N	Rated voltage

100

101 **5 Designation**102 **5.1 General**103 Motors designed according to this document are classified according to 5.2 to 5.7. The letters
104 used to specify the different designs stand for:

105 N: normal starting torque

106 H: high starting torque

107 Y: star-delta starting

108 E: motors utilizing extended / higher locked rotor apparent power and current to achieve
109 **efficiency classes of IE3 or higher** according to IEC 60034-30-1110 **5.2 Design N**111 Normal starting torque three-phase cage induction motors, intended for direct-on-line starting,
112 having 2, 4, 6 or 8 poles, rated from 0,12 kW to 1 600 kW.

113 5.3 Design NE

114 Normal starting torque three-phase cage induction motors having higher locked rotor apparent
115 power than design N, intended for direct-on-line starting, having 2, 4, 6 or 8 poles, rated from
116 0,12 kW to 1 600 kW. '

117

118 5.4 Designs NY and NEY

119 Motors similar to designs N or NE, respectively, but intended for star-delta starting. For these
120 motors in star-connection, minimum values for T_l and T_u are 25 % of the values of design N or
121 NE, respectively, see Table 1.

122 5.5 Design H

123 High starting torque three-phase cage induction motors with 4, 6 or 8 poles, intended for
124 direct-online starting, rated from 0,12 kW to 160 kW at a frequency of 60 Hz.

125 5.6 Design HE

126 High starting torque three-phase cage induction motors having higher locked rotor apparent
127 power than design H, with 4, 6 or 8 poles, intended for direct-online starting, rated from
128 0,12 kW to 160 kW at a frequency of 60 Hz.

129 5.7 Designs HY and HEY

130 Motors similar to designs H or HE, respectively, but intended for star-delta starting. For these
131 motors in star-connection, minimum values for T_l and T_u are 25 % of the values of design H or
132 HE, respectively, see Table 5.

133 6 Design N requirements

134 6.1 Torque characteristics

135 The starting torque is represented by three characteristic features. These features shall be in
136 accordance with the appropriate values given in Table 1 or Table 6. The values in Table 1 and
137 Table 6 are minimum values at rated voltage. Higher values are allowed.

138 The motor torque at any speed between zero and that at which breakdown torque occurs shall
139 be not less than 1,3 times the torque obtained from a curve varying as the square of the
140 speed and being equal to rated torque at rated speed. However, for 2-pole motors with type of
141 protection 'Ex eb – increased safety' having a rated output greater than 100 kW, the motor
142 torque at any speed between zero and that at which breakdown torque occurs shall not be
143 less than 1,3 times the torque obtained from a curve varying as the square of the speed and
144 being equal to 70 % rated torque at rated speed. For motors with type of protection 'Ex eb',
145 the three characteristic torques shall be in accordance with the appropriate values given in
146 Table 6.

147 NOTE The factor 1,3 has been chosen with regard to an undervoltage of 10 % in relation to the rated voltage at
148 the motor terminals during the acceleration period.

149 6.2 Locked rotor current and apparent power

150 The locked rotor apparent power shall be not greater than the appropriate value given in
151 Table 2. The values given in Table 2 are independent of the number of poles and are
152 maximum values at rated voltage. For motors with type of protection 'e', locked rotor apparent
153 power shall be in accordance with the appropriate values specified in IEC 60079-7.

154 The locked rotor current is calculated from the locked rotor apparent power according to:

$$155 \quad I_1 = \frac{S_1}{P_N} \times \frac{P_N}{\sqrt{3}U_N} \quad (1)$$

156 NOTE The advantage of specifying S_1/P_N instead of I_1/I_N is that the locked rotor current can be calculated from
157 rated power and rated voltage only, not requiring to know the rated current which depends on quantities such as
158 power factor and efficiency that are usually not known in early stages of a project.

159 **6.3 Starting requirements**

160 Motors shall be capable of withstanding two starts in succession (coasting to rest between
161 starts) from cold conditions and one start from hot after running at rated conditions. The
162 retarding torque due to the driven load will be in each case proportional to the square of the
163 speed and equal to the rated torque at rated speed with the external moment of inertia given
164 in Table 4 or Table 7.

165 In each case, a further start is permissible only if the motor temperature before starting does
166 not exceed the steady temperature at rated load. However, for 2-pole motors with type of
167 protection 'Ex eb – increased safety' having a rated output greater than 100 kW, the retarding
168 torque due to the driven load is proportional to the square of the speed and equal to 70 %
169 rated torque at rated speed, with the external moment of inertia given in Table 7. After this
170 starting, load with rated torque is possible.

171 NOTE It should be recognized that the number of starts should be minimized since these affect the life of the
172 motor.

173 **7 Design NE starting requirements**

174 The starting requirements are as for design N, except that the limits for locked rotor apparent
175 power in Table 3 apply, as increasing efficiency values require physically increasing values
176 for locked rotor apparent power.

177 **8 Designs NY and NEY starting requirements**

178 The starting requirements are as for designs N or NE, respectively. In addition, however, a
179 reduced retarding torque is necessary as the starting torque in 'star connection' may be
180 insufficient to accelerate some loads to an acceptable speed.

181 NOTE It should be recognized that the number of starts should be minimized since these affect the life of the
182 motor.

183 **9 Design H requirements**

184 **9.1 Starting torque**

185 The starting torque is represented by three characteristic features. These features shall be in
186 accordance with the appropriate values given in Table 5. These values are minimum values at
187 rated voltage. Higher values are allowed.

188 **9.2 Locked rotor current and apparent power**

189 The locked rotor apparent power shall be not greater than the appropriate value given in
190 Table 2. The values in Table 2 are independent of the number of poles and are maximum
191 values at rated voltage.