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Plastics - Determination of thermal conductivity and thermal diffusivity - Part 1: General principles (ISO/DIS 22007-1:2023)

Kunststoffe - Bestimmung der Wärmeleitfähigkeit und der Temperaturleitfähigkeit - Teil 1: Allgemeine Grundlagen (ISO/DIS 22007-1:2023)

Plastiques - Détermination de la conductivité thermique et de la diffusivité thermique - Partie 1: Principes généraux (ISO/DIS 22007-1:2023)

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Part 1:

General principles

Plastiques — Détermination de la conductivité thermique et de la diffusivité thermique — Partie 1: Principes généraux

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Foreword

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The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 61, *Plastics*, Subcommittee SC 5, *Physical-chemical properties*.

This third edition cancels and replaces the second edition (ISO 22007-1:2017), which has been technically revised.

The main changes are as follows:

- terms and definitions which are not used in the document have been deleted from Clause 3:
- new term <u>3.7</u> contact resistance has been added;
- laser flash method has been changed to light flash method;
- the document has been editorially revised.

A list of all parts in the ISO 22007 series can be found on the ISO website

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Plastics — Determination of thermal conductivity and thermal diffusivity —

Part 1:

General principles

SAFETY STATEMENT — Persons using this document should be familiar with normal laboratory practice, if applicable. This document does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user to establish appropriate safety and health practices and to ensure compliance with any regulatory requirements.

1 Scope

This document describes the background to methods for the determination of the thermal conductivity and thermal diffusivity of polymeric materials. Different techniques are available for these measurements and some may be better suited than others for a particular type, state and form of material. This document provides a broad overview of these techniques. Standards specific to these techniques, as referenced in this document, are used to carry out the actual test method.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 472, Plastics — Vocabulary 85e7c8fe/osist-pren-iso-22007-1-2023

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 472 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at https://www.iso.org/obp
- EC Electropedia: available at https://www.electropedia.org/

3.1

heat pulse

heat change in the form of a pulse produced by a heat source

3.2

heat source

heater in the form of a wire, strip, plate or foil embedded within or attached to a test specimen or an area irradiated by incident light, e.g. a laser

3.3

heat flux

q

heat source output produced by a planar source per unit time and unit area

Note 1 to entry: It is expressed in watts per square metre (W/m^2) .

3.4

temperature transient

temporary perturbation of temperature in a system initially at a uniform temperature due to a heat pulse for a period during which the system does not attain equilibrium

3.5

volumetric heat capacity

product of the density and the specific heat capacity

Note 1 to entry: It is expressed in joules per cubic metre kelvin $[J/(m^3 \cdot K)]$.

3.6

thermal effusivity

h

heat transport property given by the square root of the product of thermal conductivity and volumetric heat capacity:

$$b = \sqrt{\lambda \cdot \rho \cdot c_p}$$

where

- λ is the thermal conductivity in watt per metre kelvin [W/(m · K)];
- ρ is the density in kilogram per cubic metre [kg/m³];
- $c_{\rm p}$ is the specific heat capacity in joule per kelvin kilogram [J/(K · kg)]

Note 1 to entry: It is expressed in joules per square metre kelvin square root second $[J/(m^2 \cdot K \cdot s^{1/2})]$.

3.7

contact resistance

surface thermal resistance (STR) sitch ai/catalog/standards/sist/3436f415-48a1-426b-b05b-

thermal resistance due to the conditions of contact of solids

Note 1 to entry: The amount of heat that passes through a unit heat transfer area is proportional to the temperature difference between its two sides and inversely proportional to the thermal resistance *R*.

The thermal resistance R of a material of thickness d and thermal conductivity λ is defined as

$$R = \frac{d}{\lambda}$$

If heat passes in series through different materials, the overall thermal resistance is found as the sum of the individual materials.

Note 2 to entry: It is expressed in square meter kelvin per watt $[(m^2 \cdot K)/W]$.

4 Principles

Thermal conductivity refers specifically to the mode of heat transfer via conduction. In thermal conductivity measurements, other modes of heat transfer, such as convection, radiation and mass transfer, may occur. Where these modes are significant, the measured property is usually referred to as apparent or effective thermal conductivity. Thermal conductivity is affected by the conditions under which it is measured, such as temperature and pressure, as well as compositional variation of the material and orientation of the specimen since some materials are not isotropic.

In steady-state methods, an appropriately sized specimen of simple geometry in contact with a heat source, together with one or more temperature sensors, which may be combined with the heat source or separate from it, is allowed to equilibrate at a given temperature. Transient methods may be contact

or non-contact. A thermal transient is produced by a heat pulse to generate a dynamic temperature field within the specimen. The temperature change with time (temperature response) is measured by one or more sensors which may be combined with the heat source, placed at a fixed distance from the source or, as in the case of the light flash method, located on the other side of the specimen. For measuring very thin films (with thicknesses in the nm range), the thermal reflectance method – an ultra-fast variant of the laser flash analysis – is well suited. Two modes are available: rear heating/front detection and front heating/front detection. [16] In any case the response is analysed in accordance with a model, and a set of solutions developed for the representative set-up and designed for the specific geometry and the assumed boundary conditions. Depending upon the geometry of the specimen and source and the means of generating the temperature field, one or more thermo-physical properties can be obtained, either separately or simultaneously. Table 1 contains a summary of the characteristics of different types of transient methods and the properties that may be determined by their use.

NOTE 1 Most unfilled plastics fall into the category of materials of intermediate thermal conductivity $(0.1 \text{ W/m} \cdot \text{K to } 1 \text{ W/m} \cdot \text{K})$.

NOTE 2 Poly (methyl methacrylate) and glass fibre board IRMM-440 and glass ceramic BCR-724 $^{1)}$ have a thermal conductivity which is in the same range as those of most polymer and polymer-filled materials. Polydimethylsiloxane and glycerol are well characterized fluid reference materials with thermal conductivities in the same range as those of plastics.

NOTE 3 The thermal conductivity λ can be obtained by multiplying the thermal diffusivity α with the specific heat capacity at constant pressure c_p and the density ρ , i.e. $\lambda = \alpha \cdot c_p \cdot \rho$.

Type of method	Heat source/ heat source geometry	Mode of heat generation	Heat source/tempera- ture sensor configura- tion	Measured and/or de- rived parameters
Hot wire/line source /hot strip	Contact/Line, strip	Step-wise	Combined ^a or separate ^b	λ , α (c_p and b in some versions of the method)
Pulse transient	Plane	Pulse	Separate	α , $c_{\rm p}$, λ
Transient plane source	Contact/Plane	Pulse, step- wise	Combined	α , $c_{\rm p}$, λ
Laser or light flash	Laser, Xenon lamp/Plane	Pulse	Separate	α , $c_{\rm p}$, λ

Table 1 — Basic characteristics of transient methods

<u>Annex A</u> provides information on sources of uncertainty on measuring thermal transport properties.

5 Test methods

5.1 General

A number of test methods have been developed to provide a means of measuring thermal conductivity and thermal diffusivity based upon the basic principle outlined above. An overview of these methods is given in the following subclauses. Some of the contact methods are summarized in $\underline{\text{Table 2}}$ and then further explained in more detail. Complete details of the contact and non-contact test methods described in $\underline{5.4}$ to $\underline{5.6}$ can be found in other parts of the ISO 22007 series.

3

 $[\]lambda$ = thermal conductivity; α = thermal diffusivity; b = thermal effusivity; c_p = specific heat capacity

a One sensor

b Two sensors

¹⁾ Glass fibre board IRMM-440 and glass ceramic BCR-724 are products supplied by the Joint Research Centre (JRC) of the European Commission. This information is given for the convenience of users of this document and does not constitute an endorsement by ISO of the products named.

In contact methods, the accuracy of the measurement result depends strongly on a good thermal contact between the sensor and the sample. Enough uniaxial pressure should therefore be applied to press the various parts of the specimen and the heat source together.

NOTE In some cases heat sink pastes are used to improve thermal contact.

Table 2 — Schematic diagrams of various transient experimental methods showing critical dimensions

Method	Specimen set-up	Characteristic parameters	Ideal model
Hot wire ^a		$l = \text{specimen length}$ $w = \text{specimen width,}$ thickness $d_p = \text{wire probe diameter}$	200d _p < w l > 4w
Line source ^a	i leh STANI AF	w_s = active zone l_p = probe length d_p = probe diameter d_s = specimen diameter 22007-1:2023 rds/sist/3436f415-48a1-	$W_{s} > 1.5l_{p}$ $l_{p} > 33d_{p}$ $d_{s} > 6d_{p}$ $426b-b05b-$
Hot plate ^b	W d _s	$w = $ width, thickness $h = $ height $d_s = $ specimen diameter	w , h , d_s > $3\sqrt{\alpha t_{\max}}$ where t_{\max} is the maximum measurement time

Unless the specimen is a liquid, a suitable groove or hole has to be made for the hot wire or line source.

b Good thermal contact has to be established between the strip or disc and the specimen.

c Round or rectangular sample geometries are possible.

Method	Specimen set-up	Characteristic parameters	Ideal model
Transient plane source ^b	d _p d _p	$d_{\rm p}$ = heat source diameter $d_{\rm s}$ = specimen diameter w = specimen thickness	$d_{\rm s}-d_{\rm p}>4\sqrt{\alpha t_{\rm max}}$ where $t_{\rm max}$ is the maximum measurement time
Laser or light flash ^c	Teh STA2NDARD	$h = { m specimen\ thickness}$ $d_s/h = { m ratio\ between\ specimen\ diameter\ } (d_s)$ and thickness (h) $1 = { m IR\ detector\ }$ $2 = { m power\ source\ } ({ m laser\ }$ or xenon lamp)	$d_{\rm s}/h > 5$ The diameter $d_{\rm s}$ or side length of the sample shall be $> 10~{\rm mm}$

Table 2 (continued)

- ^a Unless the specimen is a liquid, a suitable groove or hole has to be made for the hot wire or line source.
- b Good thermal contact has to be established between the strip or disc and the specimen.
- Round or rectangular sample geometries are possible.

5.2 Hot-wire method

This method can be used to determine the thermal conductivity of polymers as a function of temperature. A wire heater is placed in a test specimen or between two test specimens of the same material. The temperature rise is measured either by the wire itself acting as a platinum resistance temperature detector or by a thermocouple placed in close proximity to the wire. The heater current is switched on and the temperature rise is measured by the thermocouple as a function of time.

Starting with the Fourier differential equation, it is possible to describe the transient heat flow for an infinitely long wire as follows:

$$\Delta T(r,t) = -\frac{\phi}{4\pi L\lambda} \operatorname{Ei}\left(-\frac{r^2}{4\alpha t}\right) \tag{1}$$

where

- t is the time, in s;
- ϕ is the rate of heat flow generated by the wire, in W;
- *r* is the distance between the heater and the thermocouple, in m;
- L is the length of the wire, in m;
- λ is the thermal conductivity, in W/(m·K);
- α is the thermal diffusivity, in m²/s ($\alpha = \lambda/\rho C_n$);
- Ei(x) is the exponential integral, given by: