

Designation: D4485-11a Designation: D4485 - 11b

# Standard Specification for Performance of Active API Service Category Engine Oils<sup>1</sup>

This standard is issued under the fixed designation D4485; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense.

#### INTRODUCTION

This specification covers all the currently active American Petroleum Institute (API) engine oil performance categories that have been defined in accordance with the ASTM consensus process. There are organizations with specifications not subject to the ASTM consensus process, such as the International Lubricant Standardization and Approval Committee (ILSAC), American Petroleum Institute (API – SM, SN Specifications), and the Association des Constructeurs Europeans d' Automobiles (ACEA). Certain of these specifications, which have been defined primarily by the use of current ASTM test methods, have also been included in the Appendix of this document Appendixes for information.

In the ASTM system, a specific API designation is assigned to each category. The system is open-ended, that is, new designations are assigned for use with new categories as each new set of oil performance characteristics are defined. Oil categories may be referenced by engine builders in making lubricant recommendations, and used by lubricant suppliers and customers in identifying products for specific applications. Where applicable, candidate oil programs are conducted in accordance with the American Chemistry Council (ACC) Petroleum Additives Product Approval Code of Practice.

Other service categories not shown in this document have historically been used to describe engine oil performance (SA, SB, SC, SD, SE, SF, SG, SH and CA, CB, CC, CD, CD-II, CE, CF, CF-2, CF-4, CG-4) (see 3.1.2). SA is not included because it does not have specified engine performance requirements. SGSH is not included because it was a category that could not be licensed for gasoline engine oil use in the API Service Symbol after Dec. 31, 1995.2, 2010. (Note—The SH category has been included in Appendix X8 as relevant information in combination with "C" categories.) The others are not included because they are based on test methods for which engine parts, test fuel, or reference oils, or a combination thereof, are no longer available. Also, the ASTM 5-Car and Sequence VI Procedures are obsolete and have been deleted from the category Energy Conserving and Energy Conserving II (defined by Sequence VI). Information on excluded older categories and obsolete test requirements can be found in SAE J183.

#### 1. Scope

- 1.1 This specification covers engine oils for light-duty and heavy-duty internal combustion engines used under a variety of operating conditions in automobiles, trucks, vans, buses, and off-highway farm, industrial, and construction equipment.
- 1.2 This specification is not intended to cover engine oil applications such as outboard motors, snowmobiles, lawn mowers, motorcycles, railroad locomotives, or oceangoing vessels.
- 1.3 This specification is based on engine test results that generally have been correlated with results obtained on reference oils in actual service engines operating with gasoline or diesel fuel. As it pertains to the API SL engine oil category, it is based on engine test results that generally have been correlated with results obtained on reference oils run in gasoline engine Sequence Tests that defined engine oil categories prior to 2000. It should be recognized that not all aspects of engine oil performance are evaluated by the engine tests in this specification. In addition, when assessing oil performance, it is desirable that the oil be evaluated under actual operating conditions.

<sup>&</sup>lt;sup>1</sup> This specification is under the jurisdiction of ASTM Committee D02 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.B0 on Automotive Lubricants.

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- 1.4 This specification includes bench and chemical tests that help evaluate some aspects of engine oil performance not covered by the engine tests in this specification.
  - 1.5 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.
- 1.5.1 Exceptions—The roller follower shaft wear in Test Method D5966 is in mils. Appendix X2 descriptions are verbatim API language, which contains a few non-SI units. is in mils. Some of the appendixes are verbatim from other sources, and non-SI units are included.

### 2. Referenced Documents

2.1 ASTM Standards:<sup>2</sup>

D92 Test Method for Flash and Fire Points by Cleveland Open Cup Tester

D93 Test Methods for Flash Point by Pensky-Martens Closed Cup Tester

D130 Test Method for Corrosiveness to Copper from Petroleum Products by Copper Strip Test

D412 Test Methods for Vulcanized Rubber and Thermoplastic ElastomersTension

D471 Test Method for Rubber PropertyEffect of Liquids

D874 Test Method for Sulfated Ash from Lubricating Oils and Additives

D892 Test Method for Foaming Characteristics of Lubricating Oils

D2240 Test Method for Rubber PropertyDurometer Hardness

D2622 Test Method for Sulfur in Petroleum Products by Wavelength Dispersive X-ray Fluorescence Spectrometry

D2887 Test Method for Boiling Range Distribution of Petroleum Fractions by Gas Chromatography

D3244 Practice for Utilization of Test Data to Determine Conformance with Specifications

D4171 Specification for Fuel System Icing Inhibitors

D4683 Test Method for Measuring Viscosity of New and Used Engine Oils at High Shear Rate and High Temperature by Tapered Bearing Simulator Viscometer at 150 C

D4684 Test Method for Determination of Yield Stress and Apparent Viscosity of Engine Oils at Low Temperature

D4951 Test Method for Determination of Additive Elements in Lubricating Oils by Inductively Coupled Plasma Atomic **Emission Spectrometry** 

D5119 Test Method for Evaluation of Automotive Engine Oils in the CRC L-38 Spark-Ignition Engine

D5133 Test Method for Low Temperature, Low Shear Rate, Viscosity/Temperature Dependence of Lubricating Oils Using a Temperature-Scanning Technique

D5185 Test Method for Determination of Additive Elements, Wear Metals, and Contaminants in Used Lubricating Oils and Determination of Selected Elements in Base Oils by Inductively Coupled Plasma Atomic Emission Spectrometry (ICP-AES)

D5293 Test Method for Apparent Viscosity of Engine Oils and Base Stocks Between 5 and 35C Using Cold-Cranking Simulator

D5302 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Deposit Formation and Wear in a Spark-Ignition Internal Combustion Engine Fueled with Gasoline and Operated Under Low-Temperature, Light-Duty Conditions

D5480 Test Method for Engine Oil Volatility by Gas Chromatography

D5481 Test Method for Measuring Apparent Viscosity at High-Temperature and High-Shear Rate by Multicell Capillary

D5533 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIE, Spark-Ignition Engine

D5800 Test Method for Evaporation Loss of Lubricating Oils by the Noack Method

D5844 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Rusting (Sequence IID)

D5966 Test Method for Evaluation of Engine Oils for Roller Follower Wear in Light-Duty Diesel Engine

D5967 Test Method for Evaluation of Diesel Engine Oils in T-8 Diesel Engine

D6082 Test Method for High Temperature Foaming Characteristics of Lubricating Oils

D6202 Test Method for Automotive Engine Oils on the Fuel Economy of Passenger Cars and Light-Duty Trucks in the Sequence VIA Spark Ignition Engine

D6278 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus

D6335 Test Method for Determination of High Temperature Deposits by Thermo-Oxidation Engine Oil Simulation Test

D6417 Test Method for Estimation of Engine Oil Volatility by Capillary Gas Chromatography

D6483 Test Method for Evaluation of Diesel Engine Oils in T-9 Diesel Engine

D6557 Test Method for Evaluation of Rust Preventive Characteristics of Automotive Engine Oils

D6593 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Deposit Formation in a Spark-Ignition Internal Combustion Engine Fueled with Gasoline and Operated Under Low-Temperature, Light-Duty Conditions

D6594 Test Method for Evaluation of Corrosiveness of Diesel Engine Oil at 135C

D6681 Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel EngineCaterpillar 1P Test Procedure D6709 Test Method for Evaluation of Automotive Engine Oils in the Sequence VIII Spark-Ignition Engine (CLR Oil Test

Engine)

<sup>&</sup>lt;sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

D6750 Test Methods for Evaluation of Engine Oils in a High-Speed, Single-Cylinder Diesel Engine1K Procedure (0.4 % Fuel Sulfur) and 1N Procedure (0.04 % Fuel Sulfur)

D6794 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Various Amounts of Water and a Long (6-h) Heating Time

D6795 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Water and Dry Ice and a Short (30-min) Heating Time

D6837 Test Method for Measurement of Effects of Automotive Engine Oils on Fuel Economy of Passenger Cars and Light-Duty Trucks in Sequence VIB Spark Ignition Engine

D6838 Test Method for Cummins M11 High Soot Test

D6891 Test Method for Evaluation of Automotive Engine Oils in the Sequence IVA Spark-Ignition Engine

D6894 Test Method for Evaluation of Aeration Resistance of Engine Oils in Direct-Injected Turbocharged Automotive Diesel Engine

D6896 Test Method for Determination of Yield Stress and Apparent Viscosity of Used Engine Oils at Low Temperature

D6922 Test Method for Determination of Homogeneity and Miscibility in Automotive Engine Oils

D6923 Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel EngineCaterpillar 1R Test Procedure

D6975 Test Method for Cummins M11 EGR Test

D6984 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIF, Spark-Ignition Engine

D6987/D6987M Test Method for Evaluation of Diesel Engine Oils in T-10 Exhaust Gas Recirculation Diesel Engine

D7097 Test Method for Determination of Moderately High Temperature Piston Deposits by Thermo-Oxidation Engine Oil Simulation TestTEOST MHT

D7109 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus at 30 and 90 Cycles

D7156 Test Method for Evaluation of Diesel Engine Oils in the T-11 Exhaust Gas Recirculation Diesel Engine

D7216 Test Method for Determining Automotive Engine Oil Compatibility with Typical Seal Elastomers

D7320 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIG, Spark-Ignition Engine

D7422 Test Method for Evaluation of Diesel Engine Oils in T-12 Exhaust Gas Recirculation Diesel Engine

D7468 Test Method for Cummins ISM Test

D7484 Test Method for Evaluation of Automotive Engine Oils for Valve-Train Wear Performance in Cummins ISB Medium-Duty Diesel Engine

D7528 Test Method for Bench Oxidation of Engine Oils by ROBO Apparatus

D7549 Test Method for Evaluation of Heavy-Duty Engine Oils under High Output ConditionsCaterpillar C13 Test Procedure

D7563 Test Method for Evaluation of the Ability of Engine Oil to Emulsify Water and Simulated Ed85 Fuel

D7589 Test Method for Measurement of Effects of Automotive Engine Oils on Fuel Economy of Passenger Cars and Light-Duty
Trucks in Sequence VID Spark Ignition Engine ASTM D4485-11b

E29 Practice for Using Significant Digits in Test Data to Determine Conformance with Specifications Stm-d4485-11b E178 Practice for Dealing With Outlying Observations

2.2 Society of Automotive Engineers Standards:<sup>3</sup>

SAE J183 Engine Oil Performance and Engine Service Classification

SAE J300 Engine Oil Classification

SAE J1423 Passenger Car and Light-Duty Truck Energy-Conserving Engine Oil Classification

SAE <del>J2643Standard</del>J2643 Standard Reference Elastomers (SRE) for Characterizing the Effects on Vulcanized Rubber

2.3 American Petroleum Institute Publication:<sup>4</sup>

API 1509 Engine Oil Licensing and Certification System (EOLCS)

2.4 Government Standard:<sup>5</sup>

DOD CID A-A-52039A (SAE 5W-30, 10W-30, and <del>15W-40)</del>15W-40)

2.5 American Chemical Council Code:<sup>6</sup>

ACC Petroleum Additives Product Approval Code of Practice

## 3. Terminology

- 3.1 Definitions:
- 3.1.1 *automotive*, *adj*—descriptive of equipment associated with self-propelled machinery, usually vehicles driven by internal combustion engines.
- 3.1.2 *category*, *n*—*in engine oils*, a designation such as <del>SH,</del> SJ, SL, SM, <u>SN,</u> CH-4, CI-4, CJ-4, Energy <u>Conserving</u>, Resource Conserving, and so forth, for a given level of performance in specified engine and bench tests.

<sup>&</sup>lt;sup>3</sup> Available from Society of Automotive Engineers (SAE), 400 Commonwealth Dr., Warrendale, PA 15096–0001.

<sup>&</sup>lt;sup>4</sup> Available from American Petroleum Institute (API), 1220 L. St., NW, Washington, DC 20005-4070, http://www.api.org.

<sup>&</sup>lt;sup>5</sup> Available from U.S. Government Printing Office Superintendent of Documents, 732 N. Capitol St., NW, Mail Stop: SDE, Washington, DC 20401.

<sup>&</sup>lt;sup>6</sup> Available from American Chemical Council, 1300 Wilson Blvd., Arlington, VA 22209.

- 3.1.3 classification, n—in engine oils, the systematic arrangement into categories in accordance with different levels of performance in specified engine and bench tests.
- 3.1.4 *heavy duty, adj— in internal combustion engine operation*, characterized by average speeds, power output, and internal temperatures that are generally close to the potential maximums.
- 3.1.5 heavy-duty engine, n—in internal combustion engine types, one that is designed to allow operation continuous at or close to its peak output.
- 3.1.6 *light-duty*, *adj in internal combustion engine operation*, characterized by average speeds, power output, and internal temperatures that are generally much lower than the potential maximums.
- 3.1.7 *light-duty engine*, *n*—*in internal combustion engine types*, one that is designed to be normally operated at substantially less than its peak output.
  - 3.1.7.1 Discussion—This type of engine is typically installed in automobiles and small trucks, vans, and buses.
- 3.1.8 *lugging*, *adj—in internal combustion engine operation*, characterized by a combined mode of relatively low-speed and high-power output.
  - 3.2 Definitions of Terms Specific to This Standard:
  - 3.2.1 Ccategory, n—the group of engine oils that are intended primarily for use in diesel and certain gasoline-powered vehicles.
- 3.2.2 *Energy Conserving category*, *n*—the group of engine oils that have demonstrated fuel economy benefits and are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.
- 3.2.3 *engine oil*, *n*—a lubricating liquid with additives that reduces friction or wear, or both, between the moving parts within an engine; removes heat, serves as a combustion-gas sealant for piston rings; and reduces potentially harmful effects such as rusting, deposit formation, oil oxidation, and foaming resulting from engine operation.
- 3.2.4 *S category*, *n*—the group of engine oils that are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.

### 4. Performance Classification

4.1 Automotive engine oils are classified in three general arrangements, as defined in 3.2; that is, S, C, and Energy Conserving. These arrangements are further divided into categories with performance measured as follows:

4.1.1*SH* 

- 4.1.1 SJ—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.1.1 Test Method D5844, the Sequence IID, gasoline engine test, test has been correlated with vehicles used in short-trip service prior to 1978, 4.7 particularly with regard to rusting. (An alternative is Test Method D6557, the Ball Rust Test.)
- 4.1.1.2 Test Method D5533, the Sequence IIIE gasoline engine test, has been correlated with vehicles used in high-temperature service prior to 1988,<sup>8</sup> particularly with regard to oil thickening and valve train wear. (Alternatives are Test Method D6984, the Sequence IIIF test, or Test Method D7320, the Sequence IIIG test.)
- 4.1.1.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stop-and-go service prior to 1988, particularly with regard to sludge and valve train wear. (An alternative is the combination of Test Method D6593, the Sequence VG test, and Test Method D6891, the Sequence IVA test.)
- 4.1.1.4 Test Method D5119, the L-38 gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions. (An alternative is Test Method D6709, the Sequence VIII test.)
- (1) Test Method D5119 (or Test Method D6709) is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.1.5 In addition to passing performance in the engine tests, specific viscosity grades shall also meet bench test requirements (see Table 1), which are discussed in the following subsections:
- (1) The volatility of engine oils relates to engine oil consumption. ) The volatility of engine oils is one of several factors that relates to engine oil consumption.
- (2) Test Method D6795, the Engine Oil Filterability Test (EOFT) screens for the formation of precipitates that can cause oil filter plugging., the EOFT screens for the formation of precipitates and gels that form in the presence of water and can cause oil filter plugging.
- (3) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency.
  - (4) The flash point earnmay indicate if residual solvents and low-boiling fractions remain in the finished oil.
- (5) Foaming) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
  - (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- 4.1.1.6Licensing of the API SH eategory requires that candidate oils meet the performance requirements in this specification,

<sup>&</sup>lt;sup>7</sup> Available from ASTM International in STP 3151 (Part 1). Also available from the Society of Automotive Engineers as Technical Paper No. 780931.

<sup>&</sup>lt;sup>7</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1473.

<sup>8</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1225. RR:D02-1471.

<sup>9</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1226. RR:D02-1273.



## TABLE 1 S Engine Oil Categories

Engine Test Method	Rated or Me	asured Parameter	Primary P	erformance Criteria
D5844 <sup>A,B</sup> (Sequence IID)	Average engine rust r			<del>8.5</del>
	<ul> <li>Number stuck lifters</li> </ul>	3		none
or D6557 <sup>A</sup> (Ball Rust Test)	Average gray value, r	<del>nin</del>		<del>100</del>
D5533 <sup>B.D</sup> (Sequence IIIE)	Hours to 375 % kinen	natic viscosity		<del>64</del>
	increase at 40 °C, mil	7		
	Average engine sludg			<del>9.2</del>
	Average piston skirt v	<del>arnish rating,<sup>F</sup> min</del>		<del>8.9</del>
	Average oil ring land	<del>deposit rating,<sup>F</sup> min</del>		<del>3.5</del>
	Lifter sticking			none
	Scuffing and wear			
	<ul> <li>Cam or lifter scuffing</li> </ul>	<del>g</del>		none
	<ul> <li>Cam plus lifter wea</li> </ul>	<del>r, µm</del>		
	— Average, max			<del>30</del>
	— Maximum, max			<del>64</del>
_	Ring sticking (oil-relat			none
or D6984 (Sequence IIIF) <sup>D</sup>		<del>s increase at 40 °C, max</del>		325 <sup>H</sup>
	Average piston skirt v	<del>arnish rating,<sup>F</sup> min</del>		<del>8.5</del> ′
	Weighted piston depo	sit rating, <sup>J</sup> min		<del>3.2</del> /
	Screened average ca	m-plus-lifter wear, µm, max		<del>20<sup>I,K</sup></del>
	Hot stuck rings			none!
or D7320 (Sequence IIIG) <sup>L</sup>	Kinematic viscosity, %	s increase at 40 °C, max		<del>150</del>
	Weighted piston depo			<del>3.5</del>
	Cam-plus-lifter wear a	<del>ıvg, µm, max</del>		<del>60</del>
	Hot stuck rings			none
D5302 <sup>B,N</sup> (Sequence VE)	Average engine sludg	e rating, <sup>E</sup> min		9.0
	Rocker arm cover slu	<del>dge rating,<sup>E</sup> min</del>		<del>7.0</del>
	Average piston skirt v	arnish rating, F min		<del>6.5</del>
	Average engine varni	sh rating, <sup>F</sup> min		<del>5.0</del>
	Oil ring clogging, %			report
	Oil screen clogging, 9	<del>6, max</del>		<del>20.0</del>
	Compression ring stic			none
	Cam wear, µm	dards ita		
	Average, max			<del>127</del>
	- Maximum, max			<del>380</del>
or D6891 (Sequence IVA) <sup>N</sup>	Average cam wear, µ	m <sup>o</sup>		<del>120</del>
plus, D6593 <sup>N</sup> (Sequence VG)	Average engine sludg	e rating. E min		<del>7.8</del>
p , , , ,	Rocker arm cover sludge rating, Emin			8.0
	Average piston skirt varnish rating, min			<del>7.5</del>
	Average engine varnish rating, min			8.9
	Oil screen clogging, %, max			<del>20</del>
	Hot stuck compression			none
nttp <sub>D51190</sub> (L 38) ls. iteh.ai/catalog/stand	Bearing weight loss, r	ng, max		Str <sub>40</sub> 04483-11
,				
	Shear stability			R
or D6709 <sup>©</sup> (Sequence VIII)	Shear stability Bearing weight loss, r	<del>ng, max</del>		# <del>26.4</del>
or D6709 <sup>©</sup> (Sequence VIII)	Shear stability Bearing weight loss, r Shear stability	<del>ng, max</del>		
o <del>r D6709<sup>©</sup> (Sequence VIII)</del>	Bearing weight loss, r		coity Crade Perfermance Cri	26.4 #
er D6709 <sup>©</sup> (Sequence VIII)  Bench Test and Measured Parameter (effective J	Bearing weight loss, r Shear stability	Vise	osity Grade Performance Cri	26:4 # teria <sup>S</sup>
Bench Test and Measured Parameter (effective J	Bearing weight loss, r Shear stability	Vise	SAE 10W-30	26.4 # teria <sup>S</sup> SAE 15W-40
Bench Test and Measured Parameter (effective $J$ )  Test Method D5800 volatility loss, $\%$ max $^T$	Bearing weight loss, r Shear stability	Vise SAE 5W-30 25	SAE 10W-30 20	26.4 # teria <sup>S</sup> SAE 15W 40
Bench Test and Measured Parameter (effective J	Bearing weight loss, r Shear stability lanuary 1, 1992)	SAE 5W-30 25 20	SAE-10W-30 20 17	26.4 # teria <sup>S</sup> SAE 15W 40  18 15
Bench Test and Measured Parameter (effective Jates Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m	Bearing weight loss, is Shear stability  January 1, 1992)	SAE 5W-30  25 20 50	SAE 10W-30 20 17 50	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup>
Bench Test and Measured Parameter (effective of the test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho	Bearing weight loss, is Shear stability  lanuary 1, 1992)  hax <sup>I</sup> hax sphorus %, max	SAE 5W-30  25 20 50 0.12	SAE 10W-30 20 17 50 0.12	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup> NR
Bench Test and Measured Parameter (effective July Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho	Bearing weight loss, is Shear stability  lanuary 1, 1992)  hax <sup>I</sup> hax sphorus %, max	SAE 5W-30  25 20 50	SAE 10W-30 20 17 50	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup>
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction photest Method D4	Bearing weight loss, I Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12	SAE 10W-30 20 17 50 0.12	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup> NR
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades) (unless valid passing Test Method D5302 resul	Bearing weight loss, I Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30 20 17 50 0.12 0.06	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup> NR 0.06
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades) — (unless valid passing Test Method D5302 resul Test Method D92 flash point, °C, min <sup>V</sup>	Bearing weight loss, I Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30 20 17 50 0.12 0.06	26.4 # teria <sup>S</sup> SAE 15W-40  18 15 NR <sup>U</sup> NR 0.06
Bench Test and Measured Parameter (effective July 1988)  Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades) — (unless valid passing Test Method D5302 resul Test Method D92 flash point, °C, min <sup>V</sup> Test Method D93 flash point, °C, min <sup>V</sup>	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30 20 17 50 0.12 0.06	26.4 # teria <sup>S</sup> SAE 15W 40 18 15 NR <sup>U</sup> NR 0.06
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades)  — (unless valid passing Test Method D5302 resul Test Method D92 flash point, °C, min V Test Method D93 flash point, °C, min V Test Method D93 flash point, °C, min V Test Method D892 foaming tendency (Option A)	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30  20 17 50 0.12 0.06	26.4 # Retria <sup>S</sup> SAE 15W 40  18 15 NR NR 0.06
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades) — (unless valid passing Test Method D5302 resul Test Method D92 flash point, °C, min <sup>V</sup> Test Method D93 flash point, °C, min <sup>V</sup> Test Method D802 foaming tendency (Option A) — Sequence I, max, foaming/settling <sup>W</sup>	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W 30 20 17 50 0.12 0.06 205 190	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR <sup>U</sup> NR 0.06  215 200  10/0
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction pho Test Method D4951 or D5185, mass fraction pho (all viscosity grades) — (unless valid passing Test Method D5302 resultest Method D92 flash point, °C, min V Test Method D93 flash point, °C, min V Test Method D802 foaming tendency (Option A) — Sequence II, max, foaming/settling W — Sequence II, max, foaming/settling W	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30 20 17 50 0.12 0.06 205 190 10/0 50/0	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR NR 0.06  215 200  10/0 50/0
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % mast Method D4951 or D5185, mass fraction photest Method D92 flash point, °C, min Test Method D92 flash point, °C, min Test Method D892 foaming tendency (Option A)—Sequence II, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Sequence III, max, foaming/settling Method D892 foaming tendency (Option A)—Se	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06  200 185 10/0 50/0 10/0	SAE 10W 30 20 17 50 0.12 0.06 205 190	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR <sup>U</sup> NR 0.06  215 200  10/0 50/0 10/0
Bench Test and Measured Parameter (effective July 1988)  Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction photest Method D4951 or D5185, mass fraction photest Method D4951 or D5185, mass fraction photest Method D9951 point, °C, min Test Method D9951 point, °C, min Test Method D9951 point, °C, min Test Method D892 floaming tendency (Option A) Sequence II, max, foaming/settling Test Method D8951 point, °C, min Test Method D8951 point, °C, min Test Method D8952 foaming tendency (Option A) Sequence II, max, foaming/settling Test Method D6082 (optional blending required)	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min	SAE 5W-30  25 20 50 0.12 0.06	SAE 10W-30 20 17 50 0.12 0.06 205 190 10/0 50/0	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR NR 0.06  215 200  10/0 50/0
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % mast Method D4951 or D5185, mass fraction photest Method D92 flash point, °C, min Test Method D92 flash point, °C, min Test Method D892 foaming tendency (Option A)—Sequence II, max, foaming/settling Sequence III, max, foaming/sequence I	Bearing weight loss, is Shear stability  January 1, 1992)  hax <sup>I</sup> hax sphorus %, max sphorus %, min  Its are obtained)	SAE 5W-30  25 20 50 0.12 0.06  200 185  10/0 50/0 10/0 report <sup>X</sup> *	SAE 10W-30 20 17 50 0.12 0.06 205 190 10/0 50/0 10/0	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR <sup>U</sup> NR 0.06  215 200  10/0 50/0 10/0
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max <sup>T</sup> Test Method D2887 volatility loss at 371 °C, % m Test Method D6795 (EOFT), % flow reduction, m Test Method D4951 or D5185, mass fraction photest Method D92 flash point, °C, min <sup>V</sup> Test Method D92 flash point, °C, min <sup>V</sup> Test Method D802 foaming tendency (Option A) Sequence II, max, foaming/settling <sup>W</sup> Sequence II, max, foaming/settling <sup>W</sup> Sequence III, max, foaming/settling Test Method D6082 (optional blending required) Test Method D6082 homogeneity and miseibility	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>I</sup> max sphorus %, max sphorus %, min- lits are obtained)	SAE 5W-30  25 20 50 0.12 0.06  200 185 10/0 50/0 10/0 report <sup>X</sup> *	20 17 50 0.12 0.06 205 190 10/0 50/0 10/0 report <sup>×</sup>	26.4 # Heria <sup>S</sup> SAE 15W 40  18 15 NR 0.06  215 200  10/0 50/0 10/0 report <sup>X</sup> *
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % mast Method D6795 (EOFT), % flow reduction, mast Method D4951 or D5185, mass fraction photest Method D992 flash point, °C, min Vacet Method D992 flash point, °C, min Vacet Method D892 foaming tendency (Option A)—Sequence II, max, foaming/settling Vacet Sequence III, max, foaming/settling Vacet Method D6082 (optional blending required) Test Method D6082 (optional blending required) Test Method D6092 homogeneity and miscibility	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>T</sup> max sphorus %, max sphorus %, min- lits are obtained)  API S Rated or Mea	### SAE 5W-30  25 20 50 0.12 0.06  200 185 10/0 50/0 10/0 report **  **  **  **  **  **  **  **  **  **	20 17 50 0.12 0.06 205 190 10/0 50/0 10/0 report <sup>×</sup>	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR <sup>U</sup> NR 0.06  215 200  10/0 50/0 10/0 report <sup>X</sup> **  Performance Criteria
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % mast Method D6795 (EOFT), % flow reduction, mast Method D4951 or D5185, mass fraction photest Method D996 flash point, °C, min Vacet Method D996 flash point, °C, min Vacet Method D892 flash point, °C, min Vace	Bearing weight loss, is Shear stability  January 1, 1992)  MAXI HAVE SPHORE TO SHEAR SPHORE WITH SHEAR SPHORE SHEAR SPHORE SHEAR SHE	### SAE 5W-30  25 20 50 0.12 0.06  200 185 10/0 50/0 10/0 report **  **  **  **  **  **  **  **  **  **	20 17 50 0.12 0.06 205 190 10/0 50/0 10/0 report <sup>×</sup>	26.4 # teria S SAE 15W 40  18 15 NR U NR 0.06  215 200  10/0 50/0 10/0 report X Y  Performance Criteria 8.5
Bench Test and Measured Parameter (effective of Test Method D5800 volatility loss, % max Test Method D2887 volatility loss at 371 °C, % mast Method D6795 (EOFT), % flow reduction, mast Method D4951 or D5185, mass fraction photest Method D996 flash point, °C, min Vacet Method D996 flash point, °C, min Vacet Method D892 flash point, °C, min Vace	Bearing weight loss, is Shear stability  lanuary 1, 1992)  max <sup>T</sup> max sphorus %, max sphorus %, min- lits are obtained)  API S Rated or Mea	### SAE 5W-30  25 20 50 0.12 0.06  200 185 10/0 50/0 10/0 report **  **  **  **  **  **  **  **  **  **	20 17 50 0.12 0.06 205 190 10/0 50/0 10/0 report <sup>×</sup>	26.4 # teria <sup>S</sup> SAE 15W 40  18 15 NR <sup>U</sup> NR 0.06  215 200  10/0 50/0 10/0 report <sup>X</sup> **  Performance Criteria



## TABLE 1 Continued

	API SJ Category	
Engine Test Method	Rated or Measured Parameter	Primary Performance Criteria
	Average engine sludge rating, <sup>E</sup> min	<del>9.2</del>
	Average engine sludge rating, <sup>C</sup> min	9.2
	Average piston skirt varnish rating, F min	<del>8.9</del>
	Average piston skirt varnish rating, min	8.9
	Average oil ring land deposit rating, F min	<del>3.5</del>
	Average oil ring land deposit rating, min	3.5
	Lifter sticking	none
	Scuffing and wear	
	Cam or lifter scuffing	none
	Cam plus lifter wear, µm	
	Average, max	30
	Maximum, max	64
	Ring sticking (oil-related) <sup>G</sup>	none
	Ring sticking (oil-related) <sup>E</sup>	none
or D6984 (Sequence	Kinematic viscosity, % increase at 40 °C, max	325 <sup>H</sup>
HIF) <sup>D</sup>	Minematic viscosity, 70 increase at 40 0, max	023
,	Kinamatia viaccaity 9/ ingrance at 40 °C may	20EF
or D6984 (Sequence	Kinematic viscosity, % increase at 40 °C, max	<u>325<sup>F</sup></u>
IIIF) <sup>D</sup>	Average pieten ekint vernieh neting F i-	0.5/
	Average piston skirt varnish rating, Fmin	8.5 <sup>1</sup>
	Average piston skirt varnish rating, min	8.5 <sup>G</sup>
	Weighted piston deposit rating, <sup>J</sup> min	3.2 <sup>1</sup>
	Weighted piston deposit rating, H min	3.2 <sup>G</sup>
	Screened average cam-plus-lifter wear, µm, max	<del>20<sup><i>l</i>,K</sup></del>
	Screened average cam-plus-lifter wear, µm, max	20 <sup><i>G,I</i></sup>
	Hot stuck rings	none <sup>1</sup>
	Hot stuck rings	none <sup>G</sup>
or D7320 (Sequence	Kinematic viscosity, % increase at 40 °C, max	150 150
HIG) <sup>L</sup>		100
or D7320 (Sequence	Kinematic viscosity, % increase at 40 °C, max	150
IIIG) <sup>J</sup>	Tanismans viologity, 75 morotood at 40 O, max	100
ma <sub>j</sub>	Weighted piston deposit rating, M min	2.5
	Weighted pictor deposit rating, mill	<del>3.5</del> 3.5
	Weighted piston deposit rating, <sup>K</sup> min	3.5
	Cam-plus-lifter wear avg, µm, max	60
Barra B.N. (B.	Hot stuck rings	none
D5302 <sup>B,N</sup> (Sequence VE)	Average engine sludge rating, Emin	9.0
D5302 <sup>B,L</sup> (Sequence VE)	Average engine sludge rating, min	9.0
	Rocker arm cover sludge rating, Emin	<del>7.0</del>
	Rocker arm cover sludge rating, C min	7.0
	Average piston skirt varnish rating, Fmin	<del>6.5</del>
	Average piston skirt varnish rating, min	6.5
	Average engine varnish rating, F min	<del>5.0</del>
	Average engine varnish rating, $^{c}$ min $747-4670-803b-b8512c$	7997ed/as5.0-d4485-1
	Oil ring clogging, %	report
	Oil screen clogging, %, max	20.0
	Compression ring sticking (hot stuck)	none
	Cam wear, µm	
	Average, max	
		127
	Maximum, max	380
<del>IVA)^</del>	Maximum, max <del>Average cam wear, µm</del> <sup>Q</sup>	380 <del>120</del>
<del>IVA)</del> <sup>∆</sup> or D6891 (Sequence	Maximum, max	380
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup>	Maximum, max Average cam wear, μm <sup>Q</sup> Average cam wear, μm <sup>M</sup>	380 <del>120</del>
<del>IVA)<sup>N</sup></del> or D6891 (Sequence IVA) <sup>L</sup>	Maximum, max <del>Average cam wear, µm</del> <sup>Q</sup>	380 <del>120</del>
<del>IVA)<sup>N</sup></del> or D6891 (Sequence <u>IVA)<sup>L</sup></u> <del>plus, D6593<sup>N</sup></del>	Maximum, max  Average cam wear, µm <sup>Q</sup> Average cam wear, µm <sup>M</sup> Average engine sludge rating, Emin  Average engine sludge rating, omin	380 <del>120</del> <u>7-8</u> 7.8
<u>IVA)<sup>N</sup></u> or D6891 (Sequence <u>IVA)<sup>L</sup></u> <del>plus, D6593<sup>N</sup></del> plus, D6593 <sup>L</sup>	Maximum, max  Average cam wear, µm <sup>Q</sup> Average cam wear, µm <sup>M</sup> Average engine sludge rating, Emin  Average engine sludge rating, omin	380 <del>120</del> <u>7-8</u> 7.8
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, µm <sup>D</sup> Average engine sludge rating, min  Average engine sludge rating, min  Rocker arm cover sludge rating, min	380 <del>120</del> <u>7-8</u> 7.8 8.0
<u>IVA)<sup>N</sup></u> or D6891 (Sequence <u>IVA)<sup>L</sup></u> <del>plus, D6593<sup>N</sup></del> plus, D6593 <sup>L</sup>	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min	380 <del>120</del> <u>7-8</u> 7.8 8.0
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, µm <sup>D</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>F</sup> min	380 <del>120</del> <u>7-8</u> 7-8 8-0 8.0 7-5
or D6891 (Sequence IVA) <sup>L</sup> <del>plus, D6593<sup>N</sup></del> plus, D6593 <sup>L</sup> <del>(Sequence VG)</del>	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min	380 <del>120</del> <u>7-8</u> 7-8 8-0 8.0 7-5
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>F</sup> min  Average piston skirt varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>C</sup> min	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>7.5</del> <del>7.5</del> <del>8.9</del>
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>ε</sup> min  Average engine sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>7.5</del> <del>7.5</del> <del>8.9</del> 8.9
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Oil screen clogging, <sup>C</sup> , max	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>8.0</del> <del>7.5</del> <del>7.5</del> <del>8.9</del> <del>20</del>
rva) <sup>N</sup> or D6891 (Sequence rva) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>ε</sup> min  Average engine sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>7.5</del> <del>7.5</del> <del>8.9</del> 8.9
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Oil screen clogging, <sup>C</sup> , max	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>7.5</del> <u>7.5</u> <del>8.9</del> 20 none
IVA) <sup>M</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>M</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)	Maximum, max  Average cam wear, µm <sup>\(\overline{D}\)</sup> Average engine sludge rating, \(\verline{E}\) min  Average engine sludge rating, \(\verline{C}\) min  Rocker arm cover sludge rating, \(\verline{C}\) min  Rocker arm cover sludge rating, \(\verline{C}\) min  Average piston skirt varnish rating, \(\verline{E}\) min  Average engine varnish rating, \(\verline{C}\) min  Average engine varnish rating, \(\verline{C}\) min  Average engine varnish rating, \(\verline{D}\) min  Oil screen clogging, \(\verline{C}\), max  Hot stuck compression rings	380 120 7.8 7.8 8.0 7.5 7.5 8.9 20 none
IVA) <sup>M</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>M</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>E</sup> min  Rocker arm cover sludge rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>F</sup> min  Average engine varnish rating, <sup>F</sup> min  Average engine varnish rating, <sup>N</sup> min  Oil screen clogging, %, max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability	380 120 7.8 7.8 8.0 7.5 7.5 9.9 20 none
VA) <sup>N</sup> or D6891 (Sequence  IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>N</sup> min  Oil screen clogging, <sup>N</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max	380 <del>120</del> <del>7.8</del> <del>7.8</del> <del>8.0</del> <del>7.5</del> <u>7.5</u> <del>8.9</del> 20 none
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG) (Sequence VG)  D5119 <sup>O</sup> (L-38)	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>ε</sup> min  Average engine sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Oil screen clogging, <sup>ε</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Shear stability	380 120 7.8 7.8 8.0 8.0 7.5 7.5 8.9 20 none 40 8
WA) <sup>№</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)  D5119 <sup>O</sup> (L-38)  Or D6709 <sup>O</sup> (Sequence	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average cam wear, μm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>C</sup> min  Average engine varnish rating, <sup>N</sup> min  Oil screen clogging, <sup>N</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max	380 120 7.8 7.8 8.0 7.5 7.5 9.9 20 none
VA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)  D5119 <sup>Q</sup> (L-38)  or D6709 <sup>Q</sup> (Sequence VIII)	Maximum, max  Average cam wear, µm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>M</sup> min  Oil screen clogging, <sup>M</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max	380 120 7-8 7-8 7-8 8-0 8-0 8-0 7-5 7-5 8-9 20 none 40 8 40 8 26-4
IVA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)  D5119 <sup>O</sup> (L-38)  er D6709 <sup>O</sup> (Sequence VIII) or D6709 <sup>O</sup> (Sequence	Maximum, max  Average cam wear, μm <sup>Δ</sup> Average engine sludge rating, <sup>ε</sup> min  Average engine sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Rocker arm cover sludge rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average piston skirt varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Average engine varnish rating, <sup>ε</sup> min  Oil screen clogging, <sup>ε</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Shear stability	380 120 7.8 7.8 8.0 8.0 7.5 7.5 8.9 20 none 40 8
VA) <sup>N</sup> or D6891 (Sequence IVA) <sup>L</sup> plus, D6593 <sup>N</sup> plus, D6593 <sup>L</sup> (Sequence VG) (Sequence VG)  D5119 <sup>Q</sup> (L-38)  or D6709 <sup>Q</sup> (Sequence VIII)	Maximum, max  Average cam wear, µm <sup>M</sup> Average engine sludge rating, <sup>E</sup> min  Average engine sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Rocker arm cover sludge rating, <sup>C</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average piston skirt varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>E</sup> min  Average engine varnish rating, <sup>M</sup> min  Oil screen clogging, <sup>M</sup> , max  Hot stuck compression rings  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max  Shear stability  Bearing weight loss, mg, max	380 120 7-8 7-8 7-8 8-0 8-0 8-0 7-5 7-5 8-9 20 none 40 8 40 8 26-4



## TABLE 1 Continued

Bench Test and Measured Parameter  SAE 0W-20, SAE 5W-20, SAE 5W-30, SAE 10W-30  Test Method D5800 volatility loss, % max <sup>2</sup> 22  Test Method D5800 volatility loss, % max <sup>2</sup> Test Method D6417 volatility loss at 371 °C, % max <sup>2</sup> Test Method D6417 volatility loss at 371 °C, % max <sup>2</sup> Test Method D5480 volatility loss at 371 °C, % max <sup>2</sup> Test Method D5480 volatility loss at 371 °C, % max <sup>2</sup> Test Method D5480 volatility loss at 371 °C, % max <sup>2</sup> Test Method D6795 (EOFT), % flow reduction, max  Test Method D6794 (EOWTT), % flow reduction, max  with 0.6 % H <sub>2</sub> 0  with 1.0 % H <sub>2</sub> 0  report with 2.0 % H <sub>2</sub> 0  report with 3.0 % H <sub>2</sub> 0  report Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, min (unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min ½  2000	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	All Others
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	<del>20^</del> AA
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20 <sup>R</sup>
Test Method D5480 volatility loss at 371 °C, % max O  Test Method D6795 (EOFT), % flow reduction, max  Test Method D6794 (EOWTT), % flow reduction, max  with 0.6 % H <sub>2</sub> 0  with 1.0 % H <sub>2</sub> 0  report  with 2.0 % H <sub>2</sub> 0  report  with 3.0 % H <sub>2</sub> 0  report  repor	<del>15<sup>AA</sup></del>
Test Method D5480 volatility loss at 371 °C, % max O  Test Method D6795 (EOFT), % flow reduction, max  Test Method D6794 (EOWTT), % flow reduction, max  with 0.6 % H <sub>2</sub> 0  with 1.0 % H <sub>2</sub> 0  report  with 2.0 % H <sub>2</sub> 0  report  with 3.0 % H <sub>2</sub> 0  report  repor	15 <sup>R</sup>
Test Method D6794 (EOWTT), % flow reduction, max with $0.6 \% H_20$ report with $1.0 \% H_20$ report with $1.0 \% H_20$ report with $2.0 \% H_20$ report report with $3.0 \% H_20$ report report rest Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{AB}$ Test Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{S}$ Test Method D4951 or D5185, mass fraction phosphorus, %, min $0.06$ (unless valid passing Test Method D5302 results are obtained) $0.06$	15 <sup>AA</sup>
Test Method D6794 (EOWTT), % flow reduction, max with $0.6 \% H_20$ report with $1.0 \% H_20$ report with $1.0 \% H_20$ report with $2.0 \% H_20$ report report with $3.0 \% H_20$ report report rest Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{AB}$ Test Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{S}$ Test Method D4951 or D5185, mass fraction phosphorus, %, min $0.06$ (unless valid passing Test Method D5302 results are obtained) $0.06$	$\frac{15^{R}}{50}$
Test Method D6794 (EOWTT), % flow reduction, max with $0.6 \% H_20$ report with $1.0 \% H_20$ report with $2.0 \% H_20$ report with $3.0 \% H_20$ report report with $3.0 \% H_20$ report report rest Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{AB}$ Test Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{S}$ Test Method D4951 or D5185, mass fraction phosphorus, %, min $0.06$ (unless valid passing Test Method D5302 results are obtained) $0.06$	50
$\begin{array}{c} \text{with } 0.6 \% \ \text{H}_20 \\ \text{with } 1.0 \% \ \text{H}_20 \\ \text{with } 2.0 \% \ \text{H}_20 \\ \text{with } 2.0 \% \ \text{H}_20 \\ \text{with } 3.0 \% \ \text{H}_20 \\ \text{Test Method D4951 or D5185, mass fraction phosphorus, \%, max} \\ \text{Test Method D4951 or D5185, mass fraction phosphorus, \%, max} \\ \text{Test Method D4951 or D5185, mass fraction phosphorus, \%, min} \\ \text{(unless valid passing Test Method D5302 results are obtained)} \\ \text{Test Method D92 flash point, } ^{\circ}\text{C, min}^{\vee} \\ \text{200} \\ \end{array}$	
$\begin{array}{c} \text{with } 1.0 \% \ \text{H}_2^{0}0 \\ \text{with } 2.0 \% \ \text{H}_2^{0}0 \\ \text{with } 3.0 \% \ \text{H}_2^{0}0 \\ \text{with } 3.0 \% \ \text{H}_2^{0}0 \\ \text{report} \\ repor$	report
with 2.0 % $H_2^0$ report with 3.0 % $H_2^0$ report $0.10^{AB}$ report report $0.10^{AB}$ rest Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{AB}$ rest Method D4951 or D5185, mass fraction phosphorus, %, max $0.10^{S}$ rest Method D4951 or D5185, mass fraction phosphorus, %, min $0.06$ (unless valid passing Test Method D5302 results are obtained) $0.06$ rest Method D92 flash point, $0.06$ rest Method D92 flash point $0.06$ rest Method D92 flash poi	report
with 3.0 % H <sub>2</sub> 0 report  Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, max  O.10 <sup>S</sup> Test Method D4951 or D5185, mass fraction phosphorus, %, min  (unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min <sup>V</sup> 200	report
Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, min  (unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min 2000	report
Test Method D4951 or D5185, mass fraction phosphorus, %, max  Test Method D4951 or D5185, mass fraction phosphorus, %, min  (unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min 2000	NR <sup>U</sup>
(unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min <sup>V</sup> 200	$NR^{\mathcal{T}}$
(unless valid passing Test Method D5302 results are obtained)  Test Method D92 flash point, °C, min <sup>V</sup> 200	0.06
Test Method D92 flash point, °C, min <sup>™</sup> 200	
	NR <sup>U</sup>
Test Method D92 flash point, °C, min <sup>U</sup> 200	$NR^{ au}$
Test Method D93 flash point, °C, min <sup>V</sup> 185	<del>NR</del> <sup>U</sup>
Test Method D93 flash point, °C, min <sup>U</sup> 185	$NR^{ au}$
Test Method D892 foaming tendency (Option A)	
— Sequence I, max, foaming/settling <sup>AC</sup> 10/0	<del>10/0</del>
Sequence I, max, foaming/settling <sup>V</sup> 10/0	10/0
Sequence II, max, foaming/settling <sup>AC</sup> 50/0	<del>50/0</del>
Sequence II, max, foaming/settling <sup>V</sup> 50/0	50/0
Sequence III, max, foaming/settling <sup>AC</sup>	<del>10/0</del>
Sequence III, max, foaming/settling 10/0	10/0
Test Method D6082 (optional blending required) Static foam, max, 200/50 <sup>AD</sup>	<del>20</del> 0/50 <sup>AD</sup>
tendency/stability	
Test Method D6082 (optional blending required) Static foam, max, 200/50 <sup>W</sup>	200/50 <sup>W</sup>
tendency/stability	
Test Method D6922 homogeneity and miscibility	¥
Test Method D6922 homogeneity and miscibility  Test Method D6335 High temperature deposits (TEOST 33), deposit  60	X
Test Method D6335 High temperature deposits (TEOST 33), deposit 60	60
wt, mg, max	
Test Method D5133 Gelation Index, max  Test Method D5133 Gelation Index, max  12  12	NR <sup>U</sup> NR <sup>™</sup>

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Engine Test Method	Rated or Measured Parameter	Primary Performance Criteria
D6984 (Sequence IIIF)	Kinematic viscosity, % increase at 40 °C, max	275
	Average piston skirt varnish rating, F min	9.0
	Average piston skirt varnish rating, min	9.0
	Weighted piston deposit rating, min	9.0 4.0
	Weighted piston deposit rating, H min	4.0
	Screened average cam-plus-lifter wear, µm, max	4.0 <del>20</del> <sup>K</sup>
	Screened average cam-plus-lifter wear, µm, max	<u>20'</u>
	Hot Stuck Rings	none
	Low temperature viscosity performance <sup>AE</sup>	report
	Low temperature viscosity performance Y	report
or D7320 (Sequence IIIG) <sup>L</sup>	Kinematic viscosity, % increase at 40 °C, max	<del>150</del>
or D7320 (Sequence IIIG) <sup>J</sup>	Kinematic viscosity, % increase at 40 °C, max	150
	Weighted piston deposit rating, min	<del>3.5</del>
	Weighted piston deposit rating, min	3.5 60
	Cam-plus-lifter wear avg, µm, max	60
	Hot stuck rings	none
	Low temperature viscosity performance <sup>AF</sup>	<del>report</del>
	Low temperature viscosity performance <sup>Z</sup>	report
D6891 (Sequence IVA)	Cam wear average, µm, o max	<del>120</del>
D6891 (Sequence IVA)	Cam wear average, µm, <sup>M</sup> max	120 127
D5302 <sup>B</sup>	Cam wear average, µm, max	127
(Sequence VE <sup>AG</sup> )	Cam wear max, µm, max	<del>380</del>
(Sequence VE <sup>AA</sup> )	Cam wear max, µm, max	<u>380</u>
D6593		
(Sequence VG)	Average engine sludge rating, Emin	<del>7.8</del>
(Sequence VG)	Average engine sludge rating, min	7.8 8.0
	Rocker arm cover sludge rating, Emin	
	Rocker arm cover sludge rating, min	8.0 <del>7.5</del>
	Average piston skirt varnish rating, F min	<del>7.5</del>



7.5
<del>8.9</del>
8.9 20
20
none
report
report
report
26.4
<del>R</del>
P

Bench Test and Measured Parameter Pe	erformance Criteria
Test Method D6557 (Ball Rust Test), average gray value, min	100
Test Method D5800 volatility loss, % max	15
Test Method D6417 volatility loss at 371 °C, % max	10
D6795 (EOFT), % flow reduction, max	50
D6794 (EOWTT), % flow reduction, max	
With 0.6 % H <sub>2</sub> O	50
With 1.0 % $H_2^{\circ}O$	50
With 2.0 % H <sub>2</sub> O	50
With 3.0 % H <sub>2</sub> O	50
Test Method D4951 or D5185, mass fraction phosphorus %, max <sup>AH</sup>	0.10 <sup>AB</sup>
Test Method D4951 or D5185, mass fraction phosphorus %, max <sup>AB</sup>	0.10 <sup>S</sup>
Test Method D4951 or D5185, mass fraction phosphorus %, min	0.06
(unless valid passing Test Method D5302 results are obtained)	
Test Method D892 foaming tendency (Option A)	
Sequence I, max, foaming/settling <sup>AC</sup>	<del>10/0</del>
Sequence I, max, foaming/settling <sup>v</sup>	10/0
Sequence II, max, foaming/settling <sup>AC</sup>	<del>50/0</del>
Sequence II, max, foaming/settling $^{ m V}$	50/0
Sequence III, max, foaming/settling <sup>AC</sup>	<del>10/0</del>
Sequence III, max, foaming/settling <sup>v</sup>	10/0
Test Method D6082 (optional blending required) static foam max;	100/0 <sup>AD</sup>
— tendency/stability	
Test Method D6082 (optional blending required) static foam max,	100/0 <sup>W</sup>
tendency/stability	<del></del>
Test Method D6922 homogeneity and miscibility	¥
Test Method D6922 homogeneity and miscibility	X
Test Method D7097 high temperature deposits (TEOST MHT-4),	<del>-</del>
deposit wt, mg, max	45
Test Method D5133 (Gelation Index), max <sup>AH</sup>	<del>12<sup>AI</sup></del>
Test Method D5133 (Gelation Index), max <sup>AB</sup>	<u>12<sup>AC</sup></u>

<sup>A</sup> Demonstrate passing performance in either Test Method D5844 or D6557.

D6709 (Sequence VIII) (Sequence VIII)

- <sup>B</sup> Monitoring of this test method was discontinued in June 20, 2001. Valid test results shall predate the end of the last calibration period for the test stand in which this test method was conducted.
- <sup>C</sup> CRC RuASTM Deposit Rating Manual-No. 7 20, available from ASTM Custoomerdin Relationg Res, ASTM Intearch Councational, 2 19 Pe00 Barr Harbor Drimeyet, Werst Ceonter Pshohockwy., Atlaenta, G PA-303 194628-2959.
- Demonstrate passing performance in either Test Method D5533 or D6984. However, an oil passing Test Method D6984 and containing less than 0.08 % mass phosphorus in the form of ZDDP shall also pass the wear limits in Test Method D5302 (see also footnote <sup>£</sup>\_2).
- EGRC SAn olludg-re Riated stuck ring Man occual Nrs o. 12:n ava pilable frstom Goordina with an ing Resedividuareh Gl ouncil, 219 Pe rimeter Genter Pkwy., Atg land deposit ra, GA 3034ting <2.6.
  - F CRC Varnish RaDeting Manual No. 14, available from Goordinating Rese arch Council, 219 Perimeter Center Pkwy., Atlanta, GA 3034 60 h.
  - G An oil-rDelated stuckrming occurs on a piston with an individual oil ring land deposit r ating <2.6 80 h.
- H Determine weighted piston deposits by rat-6ing the following piston areas and applying the corresponding weightings: undercrown, 10 %; second land, 15 %; third land, 30 %; piston skirt, 10 %; first groove, 5 %; second groove, 10 %; and third groove, 20 %. Use ASTM Deposit Rating Manual 20 for all ratings.
- DCalculate by eliminating the highest and lowest cam-plus-lifter wear results and then calculate by eliminating the highest and lowest cam-plus-lifter wear results and then calculate by eliminating the remaining ten rating positions.
- Determine weighted piston deposits by rating the following piston areas and applying the corresponding weightings: undercrown, 10%; second land, 15%; third land, 30%; piston skirt, 10%; first groove, 5%; second groove, 10%; and third groove, 20%. Use CRC Varnish Rating Manual No. 14 for all ratings.
  - \*Calculate by eliminating the highest and lowest cam-plus-lifter wear results and then calculating an average based on the remaining ten rating positions.
- <sup>±</sup> For oils containing at least 0.06 % mass phosphorus in the form of ZDDP, demonstrating passing performance in the Sequence IIIG test obviates the need to also conduct Test Method D5302 (Sequence VE), which was previously required for oils with less than 0.08 % mass phosphorus.
  - MY Unlike the Sequence IIIF test, piston skirt varnish rating is not required in the Sequence IIIG test.
  - № Demonstrate passing performance in Test Method D5302, or alternatively, in both Test Method D6891 and Test Method D6593.
- <sup>6M</sup> Determine cam wear according to Test Method D6891. Seven wear measurements are made on each cam lobe and the seven measured values are added to obtain an individual cam lobe wear result. The overall cam wear value is the average of the twelve individual cam lobe wear results.
- PN Determine the average engine varnish rating by averaging the piston skirt, right rocker arm cover, and left rocker arm cover varnish ratings. Use th ASTM De CRC Varniposhit Rating Manual-No. 14 20 for all ratings.
- Demonstrate passing performance in either Test Method D5119 or D6709.
- Pro-hour stripped kinematic viscosity (oil shall remain in original viscosity grade).
- <sup>€</sup> Passing bMench test p therf vormlancetis onlity required for SAE 5W-30, SAE 10W-30, amend SAE 15W-40 vt iscosn eity gherad Tes as dt Mefinethod in SAE J300 D5800-
  - Theet either Test Method , D54800, or Test Method D2886417-volatility requirement.
  - \*\*\* NR stPassindg volatility los fs only r-Not Required for SAE 15W-40 oils.
  - WeeThis is a noncritical specificathion as descr-Fibesd in Pract-Micethod-D93244 or Test Method D93 flash point requirement.
  - \*\*T DetermineNR settliang vds folume ar Not 5 m Requinred.
  - \*U Report kinetic foam volume (mL), static foam volume (mL), and collapse time, s.



- YHomogeneous with SAE reference oils.
- <sup>-2</sup>Meet-th e-volatility requirement in either Test Method D<del>5800</del>92, or Test Method D<del>5480</del>93, flash point r<del>D6417</del>equirement.
- PaDetermine ssettling volatility loss only requirmed for SAE, in mL, at 15W-40-o milsn.
- ABW This is a noneDetermiticalne specificattlion as dg volumeser, ibed in Pr mL, aet 1 mice D3244n.
- AGX DeterHominoge-settling-veolume,s win mL, at 10 min SAE reference oils.
- ADY Determine settling volume, in mL, at 1 min.
- AEEvaluate the 80- h test oil sample by Test Method D4684 at the temperature indicated by the low temperature grade of oil as determined on the 80- h sample by Test Method D5293
- AFZ Measure the viscosity of the EOT oil sample by Test Method D4684. The measured viscosity shall meet the requirements of the original grade or the next higher grade. The EOT sample can be either from a Sequence IIIG or a Sequence IIIGA test. (A Sequence IIIGA test is identical to a Sequence IIIG test, except only low temperature viscosity performance is measured.) Additional details are provided in the Sequence IIIG test method, in Section 13.6.
  - AGA Not required for oils containing a minimum of 0.08 % mass phosphorus in the form of ZDDP.
  - AHB Requirement applies only to SAE 0W-20, 5W-20, 0W-30, 5W-30, and 10W-30 viscosity grades.
  - AG For gelation temperatures at or above the W grade pumpability temperature as defined in SAE J300.

and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification. (See Appendix X3 for more information.)

- 4.1.2SJ—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.2.1Test Method D5844, the Sequence IID, gasoline engine test has been correlated with vehicles used in short-trip service prior to 1978, particularly with regard to rusting. (An alternative is Test Method D6557, the Ball Rust Test.)
- 4.1.2.2Test Method D5533, the Sequence IIIE gasoline engine test, has been correlated with vehicles used in high-temperature service prior to 1988, particularly with regard to oil thickening and valve train wear. (Alternatives are Test Method D6984, the Sequence IIIF test, or Test Method D7320, the Sequence IIIG test.)
- 4.1.2.3Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stop-and-go service prior to 1988, particularly with regard to sludge and valve train wear. (An alternative is the combination of Test Method D6593, the Sequence VG test, and Test Method D6891, the Sequence IVA test.)
- 4.1.2.4Test Method D5119, the L-38 gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions. (An alternative is Test Method D6709, the Sequence VIII test.)
- (1)Test Method D5119 (or Test Method D6709) is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.2.5In addition to passing performance in the engine tests, specific viscosity grades shall also meet bench test requirements (see Table 1), which are discussed in the following subsections:
  - (1) The volatility of engine oils is one of several factors that relates to engine oil consumption.
- (2) Test Method D6795, the EOFT screens for the formation of precipitates and gels that form in the presence of water and can cause oil filter plugging.
- (3) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency.
  - (4) The flash point may indicate if residual solvents and low-boiling fractions remain in the finished oil.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
  - (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test Method D6335, the TEOST test, may be useful in determining the deposit control of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low temperature protection not adequately measured by the Test Method D4684.
- 4.1.21.6 Licensing of the API SJ category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification. (See Appendix X3 for more information.)
  - 4.1.34.1.2 SL—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests: 4.1.3.1Test Method D6984
- 4.1.2.1 Test Method D6984, the Sequence IIIF gasoline engine test, is used to measure oil thickening and piston deposits under high temperature conditions and provides information about valve train wear.<sup>10</sup> (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.32.2 Test Method D6891, the Sequence IVA gasoline engine test, has been correlated with the Sequence VE gasoline engine test in terms of overhead cam and slider follower wear control.<sup>7</sup>
- 4.1.32.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stop-and-go service prior to 1988, with regard to valve train wear. It is included in the SL performance specification to augment assessment of the wear control performance of oils containing less than 0.08 % mass of phosphorus from ZDDP additive.

<sup>&</sup>lt;sup>10</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1391.

Note1—Prior to May 2004, the API SH, SJ, and SL categories required that oils with passing Test Method D6984 (Sequence IIIF) results, and containing less than 0.08% mass phosphorus in the form of ZDDP, also demonstrate passing performance in Test Method- 1—Prior to May 2004, the API SH, SJ, and SL categories required that oils with passing Test Method D6984 (Sequence IIIF) results, and containing less than 0.08 % mass phosphorus in the form of ZDDP, also demonstrate passing performance in Test Method D5302 (Sequence VE). This requirement was included to address concerns over adequate wear protection with low levels of ZDDP. However, Test Method D5302 (Sequence VE). This requirement was included to address concerns over adequate wear protection with low levels of ZDDP. However, Test Method D5302 has not been available to industry for some time; and an alternative method was needed. In a related activity, the next level of gasoline engine oil performance, the ILSAC GF-4 standard, was developed outside the normal ASTM consensus process. Deliberations during the GF-4 development process included careful consideration of the suitability of Test Method-has not been available to industry for some time, and an alternative method was needed. In a related activity, the next level of gasoline engine oil performance, the ILSAC GF-4 standard, was developed outside the normal ASTM consensus process. Deliberations during the GF-4 development process included careful consideration of the suitability of Test Method D7320, the Sequence IIIG, a new test, to evaluate the wear protection of oils with less than 0.08 % mass phosphorus. Data on oils with less than 0.08 % mass phosphorus in the form of ZDDP were reviewed by members of the D02.B0 Passenger Car Engine Oil Classification Panel (PCEOCP). These data were from Test Method D7320, the Sequence HIG, a new test, to evaluate the wear protection of oils with less than 0.08% mass phosphorus. Data on oils with less than 0.08% mass phosphorus in the form of ZDDP were reviewed by members of the D02.B0 Passenger Car Engine Oil Classification Panel (PCEOCP). These data were from Test Method (Sequence IIIG) tests and from field tests on large populations of older vehicles with different engine types. Based on these data, the PCEOCP recommended a ballot to allow the use of Test Method D7320 (Sequence HIG) tests and from field tests on large populations of older vehicles with different engine types. Based on these data; the PCEOCP recommended a ballot to allow the use of Test Method D7320 (Sequence IIIG) as an alternative to Test Method D6984 (Sequence IIIF) plus Test Method D5302-(Sequence IIIG) as an alternative to Test Method D6984 (Sequence IIIF) plus Test Method D5302 (Sequence VE) for demonstration of acceptable API SH, SJ, and SL performance on low phosphorus oils, establishing at least the mass fraction of phosphorus is 0.06 % as the minimum level. That ballot was approved by Subcommittee D02.B0 in May 2004.

#### 4.1.3.4Test Method D6593

- 4.1.2.4 Test Method D6593, the Sequence VG gasoline engine test, has been correlated with the Sequence VE gasoline engine test and with vehicles used in stop-and-go service prior to 2000, with regard to sludge and varnish deposit control.
- 4.1.32.5 Test Method D6709, the Sequence VIII gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions and has been shown to correlate with the L-38 gasoline engine test.<sup>8</sup>
  - (1) The Sequence VIII gasoline engine test is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.32.6 In addition to passing performance in the engine tests, oils shall also meet bench test requirements (see Table 1), which are discussed in the following subsections:
  - (1) Test Method D6557(Ball Rust Test), was developed to replace the Sequence IID gasoline engine test, and evaluates the ability of an oil to prevent the formation of rust under short-trip service conditions.
  - (2) The volatility of engine oils is one of several factors that relates to engine oil consumption. For this engine oil category, volatility is measured by Test Methods D5800 and D6417.
  - (3) Test Method D6795, the Engine Oil Filterability Test (EOFT) and Test Method D6794, the Engine Oil Water Tolerance Test (EOWTT) screen for the formation of precipitates and gels which form in the presence of water and can cause oil filter plugging.
- (4) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency. For this engine oil category, phosphorus content is measured by either Test Method D4951 or D5185.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082empirically rate the foaming tendency and stability of oils.
  - (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test Method D7097, the TEOST MHT-4 test may be useful in determining the piston deposit control capability of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low-temperature protection not adequately measured by Test Method D4684.
- 4.1.32.7 Licensing of the API SL category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Codewill help ensure that an engine oil meets its intended performance specification.

#### 4.1.4

4.1.3 CH-4—Oil meeting the performance requirements measured in the following diesel and gasoline engine tests and bench tests.

#### 4.1.4.1Test Method

- <u>4.1.3.1 Test Method</u> D6750, the 1K diesel engine test, has been correlated with vehicles equipped with engines used in high speed operation prior to 1989, particularly with respect to aluminum piston deposits and oil consumption when the mass fraction of sulfur content is nominally 0.4 %.
- 4.1.4.24.1.3.2 Test Method D6681, the 1P diesel engine test, has been used to predict iron piston deposit formation and oil consumption in four-stroke-cycle, direct injection, diesel engines that have been calibrated to meet 1998 U.S. federal exhaust

emissions requirements for heavy duty engines operated on fuel containing the mass fraction of sulfur less than  $0.05\,\%$ .

4.1.4.3Test Method-11

<u>4.1.3.3 Test Method</u> D6483, the T-9 diesel engine test, has been correlated with vehicles equipped with engines used in high speed operation prior to 1998, particularly in regard to ring and liner wear and used oil lead content.<sup>12</sup> (Alternatives are Test Method D6987/D6987M, the T-10 diesel engine test—see <u>4.1.5.24.1.4.2</u>, and Test Method D7422, the T-12 diesel engine test—see <u>4.1.4.24.1.3.2</u>.)

### 4.1.4.4Test Method

<u>4.1.3.4 Test Method</u> D5967 extended, the T-8E engine test, has been shown to generate soot-related oil thickening in a manner similar to 1998 emissions-controlled heavy duty diesel engines using electronic injection control systems.

#### 4.1.4.5Test Method

4.1.3.5 Test Method D6838, The M11 High Soot diesel engine test has been correlated with vehicles equipped with four-stroke-cycle diesel engines used in high speed operations prior to 1998, particularly with regard to soot related valve train wear, filter plugging, and sludge control. (An alternative is Test Method D7468, the Cummins ISM diesel engine test. See 4.1.6.54.1.5.5.)

#### 4.1.4.6Test Method

- 4.1.3.6 Test Method D5966, the Roller Follower Wear Test, has been correlated with hydraulic roller cam follower pin wear in medium-duty indirect injection diesel engines used in broadly based field operations.
- 4.1.43.7 Test Method D6984, the Sequence IIIF test, is used to measure bulk oil viscosity increase, which indicates an oil's ability to withstand the higher temperatures found in modern diesel engines. (An alternative is Test Method D7320, the Sequence IIIG test.)

#### 4.1.4.8Test Method

4.1.3.8 Test Method D6894, the EOAT has been correlated with oil aeration in diesel engines equipped with HEUI used in medium-duty diesel engines.

## 4.1.4.9Test Method D892<sup>14</sup>

4.1.3.9 Test Method D892, a foaming test, Sequences I, II and III, has been shown to predict foaming of engine oils in diesel engines.

## 4.1.4.10Test Method

4.1.3.10 Test Method D6594 operated at 135 °C, a High Temperature Corrosion Bench Test (HTCBT), has been shown to predict the corrosion of engine oil-lubricated copper and lead containing components used in diesel engines.

#### 4.1.4.11Test Method

4.1.3.11 Test Method D6278, the Diesel Injector Shear Test, has been shown to correlate with permanent shear loss of engine oils in medium-duty direct injection diesel engines used in broadly based field operations.

## 4.1.4.12Test Method

- 4.1.3.12 Test Method D5800, Noack Volatility or, alternatively, Test Method D6417, are used to measure engine oil volatility loss under high temperature operating conditions.
- 4.1.43.13 Licensing of the API CH-4 category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Codewill help ensure that an engine oil meets its intended performance specification.

4.1.5

<u>4.1.4</u> *CI-4*—Oil meeting the performance requirements measured in the following diesel and gasoline engine tests and bench tests.

#### 4.1.5.1Test Method

<u>4.1.4.1 Test Method</u> D6923, the 1R single cylinder diesel engine test is used to measure engine oil performance with respect to piston deposits, oil consumption, piston and piston ring scuffing, and ring sticking using a two-piece iron/aluminum piston similar to that used in modern, production heavy-duty diesel engines. (An alternative is Test Method D6681, the 1P diesel engine test, see <u>4.1.4.24.1.3.2</u>.

4.1.5.2

4.1.4.2 Test Method D6987/D6987M, the T-10 diesel engine test, is used to measure engine oil performance with respect to piston ring and cylinder liner wear, bearing lead corrosion, and oil consumption in an electronically governed, open chamber, in-line six-cylinder, four-stroke cycle, turbocharged, compression-ignition engine with exhaust gas recirculation. (An alternative is Test Method D7422, the T-12 diesel engine test, see 4.1.6.24.1.5.2.)

#### 4.1.5.3Test Method

4.1.4.3 Test Method D6975, the M11 EGR heavy-duty diesel engine test, is used to evaluate oil performance with respect to

<sup>11</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1473. RR:D02-1441.

<sup>&</sup>lt;sup>12</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1471. RR:D02-1440.

<sup>&</sup>lt;sup>13</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1273. RR:D02-1439.

<sup>14</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1441. RR:D02-1379.