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Thermal insulation products — Vacuum insulation panels (VIPs) — Specification

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Foreword

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The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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This document was prepared by Technical Committee ISO/TC 163, *Thermal performance and energy use in the built environment*, Subcommittee SC 3, *Thermal insulation products, components and systems*.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Thermal insulation products — Vacuum insulation panels (VIPs) — Specification

1 Scope

This document:

- defines requirements for vacuum insulation panels (VIPs) with silica or glass fibre core, which are used for thermal insulation of buildings;
- outlines required product properties, their performance, test methods and rules for conformity evaluations, identification and labelling;
- provides a test method to determine ageing factors and the influence of the linear thermal bridges at the edges.

This document is applicable to all types of silica and glass fibre core VIPs, independent of the type of envelope. In the case of a glass fibre core VIP, it is only applicable to VIPs with desiccants whose service life is ≥ 25 years.

This document is not applicable to:

- any specific installation and application requirements;
- products intended to be used for the insulation of building equipment and industrial installations.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 1182, Reaction to fire tests for products — Non-combustibility test

ISO 1716, Reaction to fire tests for products — Determination of the gross heat of combustion (calorific value)

ISO 3529-1, Vacuum technology — Vocabulary — Part 1: General terms

ISO 3529-2, Vacuum technology — Vocabulary — Part 2: Vacuum pumps and related terms

ISO 3529-3, Vacuum technology — Vocabulary — Part 3: Total and partial pressure vacuum gauges

ISO 8301, Thermal insulation — Determination of steady-state thermal resistance and related properties — Heat flow meter apparatus

ISO 8302, Thermal insulation — Determination of steady-state thermal resistance and related properties — Guarded hot plate apparatus

ISO 8990, Thermal insulation — Determination of steady-state thermal transmission properties — Calibrated and guarded hot box

 ${\it ISO~10211, Thermal~bridges~in~building~construction-Heat~flows~and~surface~temperatures-Detailed~calculations}$

ISO 10456, Building materials and products — Hygrothermal properties — Tabulated design values and procedures for determining declared and design thermal values

ISO 11925-2, Reaction to fire tests — Ignitability of products subjected to direct impingement of flame — Part 2: Single-flame source test

ISO 12136, Reaction to fire tests — Measurement of material properties using a fire propagation apparatus

ISO 12567-1, Thermal performance of windows and doors — Determination of thermal transmittance by the hot-box method — Part 1: Complete windows and doors

ISO 12576-1:2001, Thermal insulation — Insulating materials and products for buildings — Conformity control systems — Part 1: Factory-made products

ISO 29465, Thermal insulating products for building applications — Determination of length and width

ISO 29466, Thermal insulating products for building applications — Determination of thickness

ISO 29467, Thermal insulating products for building applications — Determination of squareness

ISO 29468, Thermal insulating products for building applications — Determination of flatness

ISO 29472, Thermal insulating products for building applications — Determination of dimensional stability under specified temperature and humidity conditions

EN 13501-1, Fire classification (Euroclasses) of construction products and building elements — Classification using test data from reaction to fire tests

EN 13823, Reaction to fire tests for building products — Building products excluding floorings exposed to the thermal attack by a single burning item

3 Terms, definitions, symbols and units and ard safety and are safety.

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at https://www.iso.org/obp
- IEC Electropedia: available at https://www.electropedia.org/

3.1 Terms and definitions

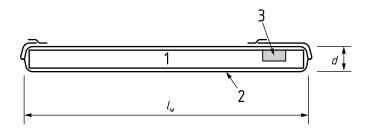
3.1.1

vacuum insulation panel VIP

insulation element containing open porous *core material* (3.1.4) and an *adsorbent* (3.1.8) within an *envelope* (3.1.5), where the *inner pressure* (3.1.10) inside the envelope is significantly lower, close to the vacuum (i.e. zero pressure), than the ambient air pressure

Note 1 to entry: A schematic view of a VIP is shown in Figure 1.

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Key

- 1 core material
- 2 envelope
- 3 adsorbent
- d thickness (3.1.17)
- working length (3.1.11)

Figure 1 — Schematic view of VIP

3.1.2

silica core VIP

vacuum insulation panel (VIP) (3.1.1) using fumed silica or other comparable silica powders as core material(3.1.4)

3.1.3

glass fibre core VIP

vacuum insulation panel (VIP) (3.1.1) using glass fibre as core material (3.1.4), and generally containing an adsorbent (3.1.8)

3.1.4

core material

open porous insulation material constituting the main component inside the vacuum insulation panel (VIP) (3.1.1) envelope (3.1.5)

3.1.5

envelope

barrier layer(s) of the *vacuum insulation panel (VIP)* (3.1.1) resisting gas or vapour permeation into and securing the vacuum inside the VIP

3.1.6

metallized film

laminated film containing a high barrier performance metallic thin layer produced by chemical/ physical deposition

3.1.7

aluminium foil laminated film

laminated film containing aluminium foil as a gas barrier layer

3.1.8

adsorbent

material adsorbing either water vapour or dry air, or both, physically or chemically

3.1.9

desiccant

material added inside the *envelope* (3.1.5) for the purpose of adsorbing water vapour

EXAMPLE CaO.

3.1.10

inner pressure

total gas pressure within the *vacuum insulation panel (VIP)* (3.1.1)

3.1.11

working length

I_w

longer linear dimension of the major surface of the test specimen

Note 1 to entry: See Figure 2.

3.1.12

working width

 w_{w}

shorter linear dimension of the major surface of the test specimen, measured at right angles to the working length (3.1.11)

Note 1 to entry: See Figure 2.

3.1.13

core length

 $l_{\rm c}$

longer linear dimension of the *core material* (3.1.4) of the test specimen

Note 1 to entry: See Figure 2.

3.1.14

core width

 $w_{\rm c}$

shorter linear dimension of the *core material* (3.1.4) of the test specimen, measured at right angles to the *core length* (3.1.13)

3.1.15

length of edge seal

 I_2

longer linear dimension of the edge seal of the test specimen 648-4421-a56b-d178ea8c8362/iso-

Note 1 to entry: See Figure 2.

3.1.16

width of edge seal

 w_2

shorter linear dimension of the edge seal of the test specimen, measured at right angles to the *edge seal* length (3.1.19)

Note 1 to entry: See Figure 2.

3.1.17

thickness

d

linear dimension measured perpendicularly to the length and width plane

3.1.18

surface area

 A_{c}

area of gas permeation plane of the test specimen

Note 1 to entry A_{sur} shall be determined by Formulae (1) or (2).

metallized film (MF) (3.1.6) on both sides:

$$A_{\text{sur}} = l_2 \times w_2 \times 2 \tag{1}$$

MF on single side:

$$A_{\rm sur} = l_2 \times w_2 \tag{2}$$

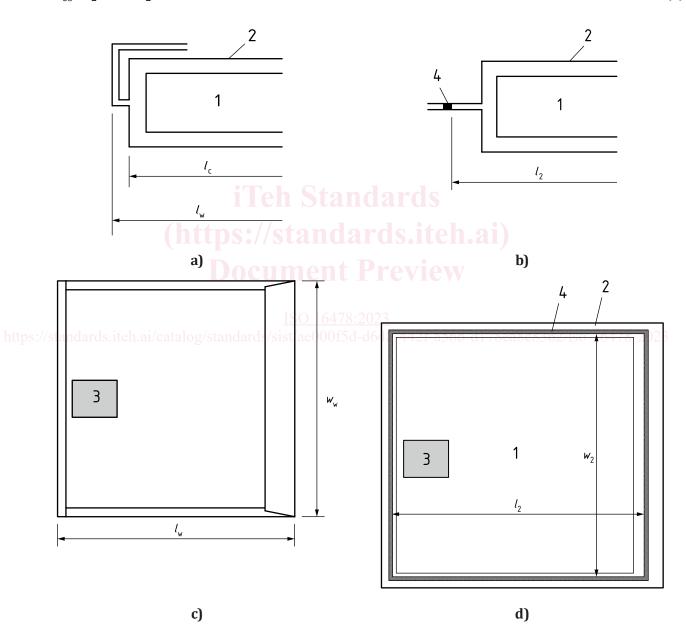
3.1.19

edge seal length

 $\emph{\emph{l}}_{es}$ total length of the edge seal of the test specimen

Note 1 to entry: $l_{\rm es}$ shall be determined by Formula (3).

$$l_{\rm es} = l_2 \times 2 + w_2 \times 2 \tag{3}$$



Key 1 core material (3.1.4)2 envelope (3.1.5)3 adsorbent or desiccant 4 edge seal l_c core length (3.1.13) l_w working length (3.1.11) l_2 length of edge seal (3.1.15) w_w working width (3.1.12) w_2 width of edge seal (3.1.16)

Figure 2 — Dimensions of a VIP

3.1.20

centre of panel

COP

area of the vacuum insulation panel (VIP) (3.1.1) not affected by the edge effect (3.1.21)

3.1.21

edge effect

thermal bridging along the edge due to higher thermal conductivity of the outer *envelope* (3.1.5) compared to the *core material* (3.1.4)

3.1.22

aged value

expected mean thermal conductivity value at 25 years in specified laboratory conditions

3.2 Symbols and units

A https://standards.	surface area of the VIP	m ² c8362/iso-16478-2023
A_{m}	metering area of the GHP or HFM apparatus used for measurement	m^2
$A_{ m N}$	nominal surface area of the VIP	m^2
$A_{\rm sp}$	area of the specimen measured by hot box method	m^2
$A_{\rm sur}$	surface area of gas permeation plane of the product	m^2
$A_{\rm sur,sp}$	surface area of gas permeation plane of the specimen	m^2
$C_{ m des}$	capacity of the desiccant	g/g
$C_{ m des,20\%}$	capacity of the desiccant including a safety margin of 20 $\%$	g/g
d	thickness	m
$d_{ m ambient}$	thickness of the ventilated VIP	m
$d_{ m N}$	nominal thickness of the product	m
$d_{ m VIP}$	thickness of the VIP	m
$f_{ m air}$	acceleration factor for dry air of the envelope	-

N number of test results - P_{air} air permeability of the VIP envelope m³··l $P_{air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RH $P_{air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, $p/(d)$			
l_c core lengthm l_c core lengthm l_c length of edge sealm l_w working lengthm l_ψ length of the joints within the metering aream m_1 initial water amount of core materialg m_2 amount of adsorbed water vapourg m_{25a} water vapour amount adsorbed over 25 yearsg m_{des} mass of desiccantg $m_{des,1a}$ mass of the desiccant after testg $m_{des,1d}$ sufficient amount of desiccantg $m_{des,2a}$ mass of the desiccant before acceleration testg $m_{des,0}$ mass of the desiccant after acceleration testg $m_{des,0}$ mass of the saturated desiccantg $m_{des,0}$ mass of the saturated desiccantg $m_{t,air,23/50}$ inner dry air mass increase rate at 23 °C, 50 % relative humidityg/de $m_{t,air,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/de $m_{t,air,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/de $m_{t,air,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/de $m_{t,air,23/50}$ air permeability of the VIP envelopem³-1 $m_{t,air,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RHg/(m²-1) $m_{t,air,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(m²-1) $m_{t,air,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(m²-1) $m_{t,air,23/50}$ <td>$f_{ m v}$</td> <td>acceleration factor for water vapour of the VIP envelope</td> <td>-</td>	$f_{ m v}$	acceleration factor for water vapour of the VIP envelope	-
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$m_{ m des,1d}$ sufficient amount of desiccant $m_{ m des,2a}$ mass of the desiccant before acceleration test $m_{ m des,2c}$ mass of the desiccant after acceleration test $m_{ m des,2c}$ mass of the fully dried desiccant $m_{ m des,sat}$ mass of the saturated desiccant $m_{ m des,sat}$ mass of the saturated desiccant $m_{ m des,sat}$ inner dry air mass increase rate at 23 °C, 50 % relative humidity $m_{ m t,v}^2$ (RH) $m_{ m t,v}^2$ water vapour mass increase rate at 23 °C, 50 % RH $m_{ m t,v}^2$ air permeability of the VIP envelope $m_{ m t,v}^3$ air permeability of the VIP envelope of the product at 23 °C, $m_{ m t,v}^2$ $m_$	$m_{ m des}$	mass of desiccant	g
$m_{\rm des,2a}$ mass of the desiccant before acceleration testg $m_{\rm des,2c}$ mass of the desiccant after acceleration testg $m_{\rm des,0}$ mass of the fully dried desiccantg $m_{\rm des,sat}$ mass of the saturated desiccantg $m'_{\rm t,air,23/50}$ inner dry air mass increase rate at 23 °C, 50 % relative humidityg/da $m'_{\rm t,v,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/da N number of test results- $P_{\rm air}$ air permeability of the VIP envelopem³·l $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RHg/(d $P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RHg/(n $P_{\rm air,l,23/50}$ air permeability of the film surface at 23 °C, 50 % RHg/(n $P_{\rm air,l,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(n $P_{\rm v}$ water intake rate of the VIP envelopekg/(n $P_{\rm air,atm}$ atmospheric pressurePa $P_{\rm lim}$ maximum value of the inner pressure measured at leastPa	$m_{\rm des,1a}$	mass of the desiccant after test	g
$m_{\rm des,2c}$ mass of the desiccant after acceleration testg $m_{\rm des,0}$ mass of the fully dried desiccantg $m_{\rm des,sat}$ mass of the saturated desiccantg $m'_{\rm t,air,23/50}$ inner dry air mass increase rate at 23 °C, 50 % relative humidityg/da $m'_{\rm t,v,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/da N number of test results- $P_{\rm air}$ air permeability of the VIP envelopem³-1 $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RHg/(d $P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RHg/(n $P_{\rm air,1,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(n $P_{\rm air,1,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(n $P_{\rm air,1,23/50}$ air permeability of the VIP envelopekg/(n $P_{\rm air,1,23/50}$ air perssure inside the VIPPa $P_{\rm air,1,23/50}$ air pressure inside the VIPPa $P_{\rm air,1,23/50}$ air perssure inside the VIPPa	$m_{\rm des,1d}$	sufficient amount of desiccant	g
$m_{\rm des,0}$ mass of the fully dried desiccantg $m_{\rm des,sat}$ mass of the saturated desiccantg $m'_{\rm t,air,23/50}$ inner dry air mass increase rate at 23 °C, 50 % relative humidityg/da $m'_{\rm t,v,23/50}$ water vapour mass increase rate at 23 °C, 50 % RHg/da N number of test results- $P_{\rm air}$ air permeability of the VIP envelopem³-1 $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RHg/da $P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RHg/da $P_{\rm air,A,23/50}$ air permeability of the film surface at 23 °C, 50 % RHg/(n $P_{\rm air,1,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(n $P_{\rm v}$ water intake rate of the VIP envelopekg/(n $P_{\rm air,atm}$ air pressure inside the VIPPa $P_{\rm air,atm}$ atmospheric pressurePa $P_{\rm lim}$ maximum value of the inner pressure measured at leastPa	$m_{\rm des,2a}$	mass of the desiccant before acceleration test	g
$m_{\rm des,sat}$ mass of the saturated desiccant g inner dry air mass increase rate at 23 °C, 50 % relative humidity g/dz (RH) standards six accounted at 23 °C, 50 % RH g/dz	$m_{ m des,2c}$	mass of the desiccant after acceleration test	g
$m'_{\rm t,air,23/50}$ inner dry air mass increase rate at 23 °C, 50 % relative humidity g/days/standards. Inch ai/ (RH) standards six action 13 °C, 50 % RH g/days are vapour mass increase rate at 23 °C, 50 % RH g/days air permeability of the VIP envelope m³-1 air permeability of the VIP envelope of the product at 23 °C, 50 % RH $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RH $P_{\rm air,total,50/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RH $P_{\rm air,4.23/50}$ air permeability of the film surface at 23 °C, 50 % RH g/(n) $P_{\rm air,1.23/50}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) $P_{\rm air,1.23/50}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) $P_{\rm air,1.23/50}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope kg/(n) $P_{\rm air,1.23/50}$ air permeability of the VIP envelope	$m_{\mathrm{des},0}$	mass of the fully dried desiccant	g
ps.//standards.iteh.ai/c (RH) g/standards/sist/ae000f5d-d648-442f-a56b-d178ea8c8362/iso-160 $m'_{\rm t,v,23/50}$ water vapour mass increase rate at 23 °C, 50 % RH g/da N number of test results - air permeability of the VIP envelope $m^{3\text{-}1}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RH $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, m^{2} $m^$	$m_{ m des,sat}$	mass of the saturated desiccant	g
Nnumber of test results- P_{air} air permeability of the VIP envelope $m^3 \cdot N$ $P_{\text{air,total,23/50}}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,total,sp,23/50}}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,A,23/50}}$ air permeability of the film surface at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,1,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,1,23/50}}$ water intake rate of the VIP envelope $g/(d^3 \cdot N)$ $P_{\text{air,1,23/50}}$ air pressure inside the VIP $g/(d^3 \cdot N)$ $P_{\text{air,1,23/50}}$ air pressure inside the VIP $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air pressure inside the VIP $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ $P_{\text{air,2,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH $g/(d^3 \cdot N)$ <td>m'_{t,air, 23/50} s://standards.iteh.ai/o</td> <td></td> <td>g/day so-16478-2023</td>	m' _{t,air, 23/50} s://standards.iteh.ai/o		g/day so-16478-2023
$P_{\rm air}$ air permeability of the VIP envelopem³-l $P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RHg/(d $P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RHg/(d $P_{\rm air,A,23/50}$ air permeability of the film surface at 23 °C, 50 % RHg/(n $P_{\rm air,1,23/50}$ air permeability of the edge seal at 23 °C, 50 % RHg/(n $P_{\rm v}$ water intake rate of the VIP envelopekg/(n $P_{\rm air}$ air pressure inside the VIPPa $P_{\rm air,atm}$ atmospheric pressurePa $P_{\rm lim}$ maximum value of the inner pressure measured at leastPa	$m'_{\rm t,v,23/50}$	water vapour mass increase rate at 23 °C, 50 % RH	g/day
$P_{\rm air,total,23/50}$ air permeability of the VIP envelope of the product at 23 °C, 50 % RH $P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, 50 % RH $P_{\rm air,A,23/50}$ air permeability of the film surface at 23 °C, 50 % RH g/(n) $P_{\rm air,A,23/50}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) $P_{\rm v}$ water intake rate of the VIP envelope kg/(n) $P_{\rm v}$ air pressure inside the VIP $P_{\rm v}$ atmospheric pressure $P_{\rm lim}$ maximum value of the inner pressure measured at least $P_{\rm air,atm}$ pair maximum value of the inner pressure measured at least $P_{\rm air}$	N	number of test results	-
$P_{\rm air,total,sp,23/50}$ air permeability of the VIP envelope of the specimen at 23 °C, $p/(d)$ $p_{\rm air,A,23/50}$ air permeability of the film surface at 23 °C, 50 % RH $p_{\rm air,1,23/50}$ air permeability of the edge seal at 23 °C, 50 % RH $p_{\rm air,1,23/50}$ water intake rate of the VIP envelope $p_{\rm air}$ air pressure inside the VIP $p_{\rm air,atm}$ atmospheric pressure $p_{\rm air,atm}$ maximum value of the inner pressure measured at least $p_{\rm air}$	P_{air}	air permeability of the VIP envelope	m^3 ·Pa/(m^2 ·s)
$50 \% \mathrm{RH}$ $P_{\mathrm{air,A,23/50}}$ air permeability of the film surface at 23 °C, 50 % RH g/(n) $P_{\mathrm{air,l,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) P_{v} water intake rate of the VIP envelope kg/(n) P_{air} air pressure inside the VIP Pa $P_{\mathrm{air,atm}}$ atmospheric pressure Pa P_{lim} maximum value of the inner pressure measured at least Pa	$P_{\rm air,total,23/50}$		g/(day·Pa)
$P_{\mathrm{air,l,23/50}}$ air permeability of the edge seal at 23 °C, 50 % RH g/(n) P_{v} water intake rate of the VIP envelope kg/(n) p_{air} air pressure inside the VIP Pa $p_{\mathrm{air,atm}}$ atmospheric pressure p_{lim} maximum value of the inner pressure measured at least Pa	$P_{\rm air,total,sp,23/50}$		g/(day·Pa)
$P_{ m v}$ water intake rate of the VIP envelope kg/($p_{ m air}$ air pressure inside the VIP Pa $p_{ m air,atm}$ atmospheric pressure Pa $p_{ m lim}$ maximum value of the inner pressure measured at least Pa	$P_{\text{air,A,23/50}}$	air permeability of the film surface at 23 °C, 50 $\%$ RH	g/(m²·day·Pa)
$p_{ m air}$ air pressure inside the VIP Pa $p_{ m air,atm}$ atmospheric pressure Pa $p_{ m lim}$ maximum value of the inner pressure measured at least Pa	$P_{\rm air,l,23/50}$	air permeability of the edge seal at 23 °C, 50 $\%$ RH	g/(m·day·Pa)
$p_{ m air,atm}$ atmospheric pressure Pa $p_{ m lim}$ maximum value of the inner pressure measured at least Pa	$P_{\rm v}$	water intake rate of the VIP envelope	$kg/(m^2 \cdot s)$
$p_{ m lim}$ maximum value of the inner pressure measured at least Pa	p_{air}	air pressure inside the VIP	Pa
	$p_{\rm air,atm}$	atmospheric pressure	Pa
	$p_{ m lim}$		Pa

$p_{ m v}$	water vapour pressure inside the VIP	Pa
$p_{ m v,out}$	atmospheric water vapour pressure	Pa
p_0	initial value of the inner pressure	Pa
$p_{1/2}$	inner pressure of VIP, where λ increases by 1/2 of the thermal conductivity of still air	Pa
$p'_{\mathrm{t,air,23/50}}$	inner pressure increase rate at 23 °C, 50 % RH	Pa/day
$p'_{\rm t,air,40}$	inner pressure increase rate at 40 $^{\circ}\text{C}$	Pa/day
$p'_{\rm t,air,60}$	inner pressure increase rate at 60 °C	Pa/day
$p'_{\rm t,air,80}$	inner pressure increase rate at 80 $^{\circ}\text{C}$	Pa/day
$R_{\rm aux}$	thermal resistance of the auxiliary material	m²⋅K/W
R_{D}	declared thermal resistance	m²⋅K/W
$R_{ m eq}$	thermal resistance obtained by assuming the entire surface to be homogeneous calculated by the thermal transmittance	m²⋅K/W
$R_{s,t}$	total surface thermal resistance	m²⋅K/W
R_{mean}	mean thermal resistance 1 Standards	m²⋅K/W
R_{tot}	thermal resistance of VIP plus auxiliary material	m²⋅K/W
$R_{90/90}$	90 % fractile with a confidence level of 90 % for the thermal resistance	m²⋅K/W
S	top surface area (working length x working width) of the VIP	m^2
S_b https://standards	deviation from squareness on width or length 42f-a56b-d178ea8	mm/m 0-16478-2023
$S_{ ext{MAX}}$	deviation from flatness	mm
$S_{ m N}$	nominal perimeter of the product	m
s_{λ}	estimate of the standard deviation of the thermal conductivity	W/(m·K)
T	temperature	K
t	time	S
$t_{ m des}$	lifetime of desiccant	a
U	thermal transmittance	W/(m²⋅K)
V	core volume of the product	m^3
$V_{\rm sp}$	core volume of the specimen	m^3
$V_{ m void}$	void volume of core	m^3
W	width	m
$w_{\rm c}$	core width	m
w_2	width of edge seal	

$W_{\rm W}$	working width	m
X	water content inside the VIP	mass-%
$\lambda_{ m air}$	thermal conductivity of still air	W/(m·K)
$\lambda_{ambient}$	thermal conductivity of a ventilated VIP at centre of the panel	W/(m⋅K)
λ_{cop}	thermal conductivity for centre of panel	W/(m⋅K)
$\lambda_{\text{cop,mean}}$ (25 years)	average value of thermal conductivity over 25 years in use at centre of panel	W/(m·K)
$\lambda_{ m cop,90/90,aged}$	$\lambda_{90/90}$ at centre of panel plus ageing	W/(m·K)
λ_{D}	declared thermal conductivity	W/(m⋅K)
$\lambda_{ m eq}$	thermal conductivity including edge effect	W/(m⋅K)
$\lambda_{ m eq,ja}$	equivalent thermal conductivity including edge effect	W/(m⋅K)
$\lambda_{ ext{mean}}$	mean value of thermal conductivity	W/(m⋅K)
λ_{i}	one test result of thermal conductivity	W/(m⋅K)
λ_0	thermal conductivity in the evacuated state	W/(m⋅K)
λ_{p}'	change of thermal conductivity with pressure	W/(m·K·Pa)
λ_{t}'	change of thermal conductivity with time	W/(m·K·s)
$\lambda_{ m VIP}$	thermal conductivity of the VIP review	W/(m⋅K)
λ'_{X}	change of thermal conductivity with humidity	W/(m·K)/mass-%
$\lambda_{90/90}$ dards.iteh.ai/	90 % fractile with a confidence level of 90 % of thermal 808362/1 conductivity	W/(m⋅K) 2023
$\lambda'_{\rm t,23/50}$	change of thermal conductivity with time at 23 °C 50 % RH	W/(m·K·s)
$\lambda'_{\rm t,50/70}$	change of thermal conductivity with time at 50 °C 70 % RH	W/(m·K·s)
$\lambda_{\text{cop}}(t)$	time-dependent thermal conductivity value	W/(m⋅K)
$\lambda(t)_{,23/50}$	time-dependent value of thermal conductivity at 23 °C 50 % RH $$	W/(m·K·s)
$\lambda(t)_{,50/70}$	time-dependent value of thermal conductivity at 50 °C 70 % RH $$	W/(m·K·s)
$\lambda^*(t=0)$	interpolated initial thermal conductivity	W/(m⋅K)
$\sigma_{ m mt}$	tensile strength perpendicular to faces	kPa
σ_{10}	compressive stress at 10 % deformation	kPa
φ	RH inside the VIP	%
$arphi_{ m x}'$	change of RH inside the VIP as function of water content	(rel. humidity-%) /(mass-%)
$\Phi_{ m in}$	quantity of heat generated in the hot box	W

$\Phi_{ m l}$	quantity of heat loss from the hot box	W
$\Phi_{ m sur}$	quantity of heat flow through the surround panel	W
ψ	linear thermal transmittance	W/(m⋅K)
$\psi_{ m m}$	linear thermal transmittance for the joints in the metering area	W/(m⋅K)
$\Delta\theta_{\mathrm{n}}$	environmental temperature difference between both sides of the specimen	K

4 Requirements

4.1 General

Products shall be assessed in accordance with $\underline{\text{Clause 6}}$ and meet the requirements as outlined in $\underline{\text{Clause 4}}$.

All characteristics defined in <u>Clause 4</u>, if declared, shall be subject to product type determination (PTD) in accordance with <u>Annex E</u>. The minimum frequencies of tests in the factory production control (FPC) shall be in accordance with <u>Annex E</u>.

NOTE The manufacturer can choose to give information for additional properties (see Annex F).

4.2 Thermal resistance and thermal conductivity

4.2.1 General

Requirements of thermal resistance and thermal conductivity are given in Table 1.

Table 1 — Thermal resistance and thermal conductivity

https://standards.iteh.ai/catalog/standards/sist/ae0001	Thermal resistance	Thermal conductivity	023
Property	R	λ	
	m ²⁺ K/W	W/(m⋅K)	
Initial value of centre of panel (COP) $(\lambda_{cop,90/90}, R_{cop,90/90})$	> 1,6	< 0,005	
Initial value including thermal bridging (λ_D)	_	Declare	
Aged value of COP ($\lambda_{\text{cop,90/90,aged}}$, $R_{\text{cop,90/90,aged}}$)	> 0,8	< 0,010	
Aged value including thermal bridging ($\lambda_{90/90,aged}$)	-	Declare	

4.2.2 Initial COP thermal properties

The initial value of COP, $R_{\text{cop},90/90}$ and $\lambda_{\text{cop},90/90}$ shall be determined by using Formulae (4) and (5) and shall not exceed the limits given in Table 1.

$$\lambda_{\text{cop},90/90} = \lambda_{\text{mean}} + k \times s_{\lambda} \tag{4}$$

$$R_{\text{cop,90/90}} = \frac{d_N}{\lambda_{\text{cop,90/90}}} \tag{5}$$

4.2.3 Size dependent value

4.2.3.1 **General**

Edge effect and ageing effect depends on the size of VIP.