

Designation: D4485 - 11c

StandardSpecification for Performance of Active API Service Category Engine Oils¹

This standard is issued under the fixed designation D4485; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

INTRODUCTION

This specification covers all the currently active American Petroleum Institute (API) engine oil performance categories that have been defined in accordance with the ASTM consensus process. There are organizations with specifications not subject to the ASTM consensus process, such as the International Lubricant Standardization and Approval Committee (ILSAC), American Petroleum Institute (API – SM, SN Specifications), and the Association des Constructeurs Europeans d' Automobiles (ACEA). Certain of these specifications, which have been defined primarily by the use of current ASTM test methods, have also been included in the Appendixes for information.

In the ASTM system, a specific API designation is assigned to each category. The system is open-ended, that is, new designations are assigned for use with new categories as each new set of oil performance characteristics are defined. Oil categories may be referenced by engine builders in making lubricant recommendations, and used by lubricant suppliers and customers in identifying products for specific applications. Where applicable, candidate oil programs are conducted in accordance with the American Chemistry Council (ACC) Petroleum Additives Product Approval Code of Practice.

Other service categories not shown in this document have historically been used to describe engine oil performance (SA, SB, SC, SD, SE, SF, SG, SH and CA, CB, CC, CD, CD-II, CE, CF, CF-2, CF-4, CG-4) (see 3.1.2). SA is not included because it does not have specified engine performance requirements. SH is not included because it was a category that could not be licensed for gasoline engine oil use in the API Service Symbol after Dec. 2, 2010. (Note—The SH category has been included in Appendix X8 as relevant information in combination with "C" categories.) The others are not included because they are based on test methods for which engine parts, test fuel, or reference oils, or a combination thereof, are no longer available. Also, the ASTM 5-Car and Sequence VI Procedures are obsolete and have been deleted from the category Energy Conserving and Energy Conserving II (defined by Sequence VI). Information on excluded older categories and obsolete test requirements can be found in SAE J183.

1. Scope*

- 1.1 This specification covers engine oils for light-duty and heavy-duty internal combustion engines used under a variety of operating conditions in automobiles, trucks, vans, buses, and off-highway farm, industrial, and construction equipment.
- 1.2 This specification is not intended to cover engine oil applications such as outboard motors, snowmobiles, lawn mowers, motorcycles, railroad locomotives, or oceangoing vessels.
- ¹ This specification is under the jurisdiction of ASTM Committee D02 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.B0 on Automotive Lubricants.

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- 1.3 This specification is based on engine test results that generally have been correlated with results obtained on reference oils in actual service engines operating with gasoline or diesel fuel. As it pertains to the API SL engine oil category, it is based on engine test results that generally have been correlated with results obtained on reference oils run in gasoline engine Sequence Tests that defined engine oil categories prior to 2000. It should be recognized that not all aspects of engine oil performance are evaluated by the engine tests in this specification. In addition, when assessing oil performance, it is desirable that the oil be evaluated under actual operating conditions.
- 1.4 This specification includes bench and chemical tests that help evaluate some aspects of engine oil performance not covered by the engine tests in this specification.



- 1.5 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.
- 1.5.1 *Exceptions*—The roller follower shaft wear in Test Method D5966 is in mils. Some of the appendixes are verbatim from other sources, and non-SI units are included.

2. Referenced Documents

- 2.1 ASTM Standards:²
- D92 Test Method for Flash and Fire Points by Cleveland Open Cup Tester
- D93 Test Methods for Flash Point by Pensky-Martens Closed Cup Tester
- D130 Test Method for Corrosiveness to Copper from Petroleum Products by Copper Strip Test
- D412 Test Methods for Vulcanized Rubber and Thermoplastic Elastomers—Tension
- D471 Test Method for Rubber Property—Effect of Liquids
- D874 Test Method for Sulfated Ash from Lubricating Oils and Additives
- D892 Test Method for Foaming Characteristics of Lubricating Oils
- D2240 Test Method for Rubber Property—Durometer Hardness
- D2622 Test Method for Sulfur in Petroleum Products by Wavelength Dispersive X-ray Fluorescence Spectrometry
- D2887 Test Method for Boiling Range Distribution of Petroleum Fractions by Gas Chromatography
- D3244 Practice for Utilization of Test Data to Determine Conformance with Specifications
- D4171 Specification for Fuel System Icing Inhibitors
- D4683 Test Method for Measuring Viscosity of New and Used Engine Oils at High Shear Rate and High Temperature by Tapered Bearing Simulator Viscometer at 150 °C
- D4684 Test Method for Determination of Yield Stress and Apparent Viscosity of Engine Oils at Low Temperature
- D4951 Test Method for Determination of Additive Elements in Lubricating Oils by Inductively Coupled Plasma Atomic Emission Spectrometry
- D5119 Test Method for Evaluation of Automotive Engine
 Oils in the CRC L-38 Spark-Ignition Engine (Withdrawn
 2003)³
- D5133 Test Method for Low Temperature, Low Shear Rate, Viscosity/Temperature Dependence of Lubricating Oils Using a Temperature-Scanning Technique
- D5185 Test Method for Multielement Determination of Used and Unused Lubricating Oils and Base Oils by Inductively Coupled Plasma Atomic Emission Spectrometry (ICP-AES)
- D5293 Test Method for Apparent Viscosity of Engine Oils and Base Stocks Between -5 and -35°C Using Cold-Cranking Simulator

- D5302 Test Method for Evaluation of Automotive Engine
 Oils for Inhibition of Deposit Formation and Wear in a
 Spark-Ignition Internal Combustion Engine Fueled with
 Gasoline and Operated Under Low-Temperature, LightDuty Conditions (Withdrawn 2003)³
- D5480 Test Method for Engine Oil Volatility by Gas Chromatography (Withdrawn 2003)³
- D5481 Test Method for Measuring Apparent Viscosity at High-Temperature and High-Shear Rate by Multicell Capillary Viscometer
- D5533 Test Method for Evaluation of Automotive Engine
 Oils in the Sequence IIIE, Spark-Ignition Engine (Withdrawn 2003)³
- D5800 Test Method for Evaporation Loss of Lubricating Oils by the Noack Method
- D5844 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Rusting (Sequence IID) (Withdrawn 2003)³
- D5966 Test Method for Evaluation of Engine Oils for Roller Follower Wear in Light-Duty Diesel Engine
- D5967 Test Method for Evaluation of Diesel Engine Oils in T-8 Diesel Engine
- D6082 Test Method for High Temperature Foaming Characteristics of Lubricating Oils
- D6202 Test Method for Automotive Engine Oils on the Fuel Economy of Passenger Cars and Light-Duty Trucks in the Sequence VIA Spark Ignition Engine (Withdrawn 2009)³
- D6278 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus
- D6335 Test Method for Determination of High Temperature Deposits by Thermo-Oxidation Engine Oil Simulation Test
- D6417 Test Method for Estimation of Engine Oil Volatility by Capillary Gas Chromatography
- D6483 Test Method for Evaluation of Diesel Engine Oils in T-9 Diesel Engine (Withdrawn 2009)³
- D6557 Test Method for Evaluation of Rust Preventive Characteristics of Automotive Engine Oils
- D6593 Test Method for Evaluation of Automotive Engine Oils for Inhibition of Deposit Formation in a Spark-Ignition Internal Combustion Engine Fueled with Gasoline and Operated Under Low-Temperature, Light-Duty Conditions
- D6594 Test Method for Evaluation of Corrosiveness of Diesel Engine Oil at 135 °C
- D6681 Test Method for Evaluation of Engine Oils in a High
 Speed, Single-Cylinder Diesel Engine—Caterpillar 1P
 Test Procedure
- D6709 Test Method for Evaluation of Automotive Engine Oils in the Sequence VIII Spark-Ignition Engine (CLR Oil Test Engine)
- D6750 Test Methods for Evaluation of Engine Oils in a High-Speed, Single-Cylinder Diesel Engine—1K Procedure (0.4 % Fuel Sulfur) and 1N Procedure (0.04 % Fuel Sulfur)
- D6794 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Various Amounts of Water and a Long (6 h) Heating Time

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ The last approved version of this historical standard is referenced on www.astm.org.



- D6795 Test Method for Measuring the Effect on Filterability of Engine Oils After Treatment with Water and Dry Ice and a Short (30 min) Heating Time
- D6837 Test Method for Measurement of Effects of Automotive Engine Oils on Fuel Economy of Passenger Cars and Light-Duty Trucks in Sequence VIB Spark Ignition Engine
- D6838 Test Method for Cummins M11 High Soot Test
- D6891 Test Method for Evaluation of Automotive Engine
 Oils in the Sequence IVA Spark-Ignition Engine
- D6894 Test Method for Evaluation of Aeration Resistance of Engine Oils in Direct-Injected Turbocharged Automotive Diesel Engine
- D6896 Test Method for Determination of Yield Stress and Apparent Viscosity of Used Engine Oils at Low Temperature
- D6922 Test Method for Determination of Homogeneity and Miscibility in Automotive Engine Oils
- D6923 Test Method for Evaluation of Engine Oils in a High Speed, Single-Cylinder Diesel Engine—Caterpillar 1R Test Procedure
- D6975 Test Method for Cummins M11 EGR Test
- D6984 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIF, Spark-Ignition Engine
- D6987/D6987M Test Method for Evaluation of Diesel Engine Oils in T-10 Exhaust Gas Recirculation Diesel Engine
- D7097 Test Method for Determination of Moderately High Temperature Piston Deposits by Thermo-Oxidation Engine Oil Simulation Test—TEOST MHT
- D7109 Test Method for Shear Stability of Polymer Containing Fluids Using a European Diesel Injector Apparatus at 30 and 90 Cycles
- D7156 Test Method for Evaluation of Diesel Engine Oils in the T-11 Exhaust Gas Recirculation Diesel Engine
- D7216 Test Method for Determining Automotive Engine Oil Compatibility with Typical Seal Elastomers
- D7320 Test Method for Evaluation of Automotive Engine Oils in the Sequence IIIG, Spark-Ignition Engine
- D7422 Test Method for Evaluation of Diesel Engine Oils in T-12 Exhaust Gas Recirculation Diesel Engine
- D7468 Test Method for Cummins ISM Test
- D7484 Test Method for Evaluation of Automotive Engine Oils for Valve-Train Wear Performance in Cummins ISB Medium-Duty Diesel Engine
- D7528 Test Method for Bench Oxidation of Engine Oils by ROBO Apparatus
- D7549 Test Method for Evaluation of Heavy-Duty Engine Oils under High Output Conditions—Caterpillar C13 Test Procedure
- D7563 Test Method for Evaluation of the Ability of Engine Oil to Emulsify Water and Simulated Ed85 Fuel
- D7589 Test Method for Measurement of Effects of Automotive Engine Oils on Fuel Economy of Passenger Cars and Light-Duty Trucks in Sequence VID Spark Ignition Engine
- E29 Practice for Using Significant Digits in Test Data to Determine Conformance with Specifications

- E178 Practice for Dealing With Outlying Observations
- 2.2 Society of Automotive Engineers Standards:⁴
- SAE J183 Engine Oil Performance and Engine Service Classification
- SAE J300 Engine Oil Classification
- SAE J1423 Passenger Car and Light-Duty Truck Energy-Conserving Engine Oil Classification
- SAE J2643 Standard Reference Elastomers (SRE) for Characterizing the Effects on Vulcanized Rubber
- 2.3 American Petroleum Institute Publication:⁵
- API 1509 Engine Oil Licensing and Certification System (EOLCS)
- 2.4 Government Standard:⁶
- DOD CID A-A-52039A (SAE 5W-30, 10W-30, and 15W-40)
- 2.5 American Chemical Council Code:⁷
- ACC Petroleum Additives Product Approval Code of Practice

3. Terminology

- 3.1 Definitions:
- 3.1.1 *automotive, adj*—descriptive of equipment associated with self-propelled machinery, usually vehicles driven by internal combustion engines.
- 3.1.2 *category, n—in engine oils*, a designation such as SJ, SL, SM, SN, CH-4, CI-4, CJ-4, Energy Conserving, Resource Conserving, and so forth, for a given level of performance in specified engine and bench tests.
- 3.1.3 *classification*, *n*—*in engine oils*, the systematic arrangement into categories in accordance with different levels of performance in specified engine and bench tests.
- 3.1.4 heavy duty, adj— in internal combustion engine operation, characterized by average speeds, power output, and internal temperatures that are generally close to the potential maximums.
- 3.1.5 *heavy-duty engine*, *n*—*in internal combustion engine types*, one that is designed to allow operation continuous at or close to its peak output.
- 3.1.6 *light-duty, adj— in internal combustion engine operation*, characterized by average speeds, power output, and internal temperatures that are generally much lower than the potential maximums.
- 3.1.7 *light-duty engine*, *n*—*in internal combustion engine types*, one that is designed to be normally operated at substantially less than its peak output.
- 3.1.7.1 *Discussion*—This type of engine is typically installed in automobiles and small trucks, vans, and buses.

⁴ Available from Society of Automotive Engineers (SAE), 400 Commonwealth Dr., Warrendale, PA 15096–0001.

⁵ Available from American Petroleum Institute (API), 1220 L. St., NW, Washington, DC 20005-4070, http://www.api.org.

⁶ Available from U.S. Government Printing Office Superintendent of Documents, 732 N. Capitol St., NW, Mail Stop: SDE, Washington, DC 20401.

⁷ Available from American Chemical Council, 1300 Wilson Blvd., Arlington, VA 22209.

- 3.1.8 *lugging*, *adj—in internal combustion engine operation*, characterized by a combined mode of relatively low-speed and high-power output.
 - 3.2 Definitions of Terms Specific to This Standard:
- 3.2.1 *C category*, *n*—the group of engine oils that are intended primarily for use in diesel and certain gasoline-powered vehicles.
- 3.2.2 Energy Conserving category, n—the group of engine oils that have demonstrated fuel economy benefits and are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.
- 3.2.3 *engine oil*, *n*—a lubricating liquid with additives that reduces friction or wear, or both, between the moving parts within an engine; removes heat, serves as a combustion-gas sealant for piston rings; and reduces potentially harmful effects such as rusting, deposit formation, oil oxidation, and foaming resulting from engine operation.
- 3.2.4 *S category*, *n*—the group of engine oils that are intended primarily for use in automotive gasoline engine applications, such as passenger cars, light-duty trucks, and vans.

4. Performance Classification

- 4.1 Automotive engine oils are classified in three general arrangements, as defined in 3.2; that is, S, C, and Energy Conserving. These arrangements are further divided into categories with performance measured as follows:
- 4.1.1 *SJ*—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.1.1 Test Method D5844, the Sequence IID, gasoline engine test has been correlated with vehicles used in short-trip service prior to 1978, ^{5,8} particularly with regard to rusting. (An alternative is Test Method D6557, the Ball Rust Test.)
- 4.1.1.2 Test Method D5533, the Sequence IIIE gasoline engine test, has been correlated with vehicles used in high-temperature service prior to 1988, particularly with regard to oil thickening and valve train wear. (Alternatives are Test Method D6984, the Sequence IIIF test, or Test Method D7320, the Sequence IIIG test.)
- 4.1.1.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stop-and-go service prior to 1988, ¹⁰ particularly with regard to sludge and valve train wear. (An alternative is the combination of Test Method D6593, the Sequence VG test, and Test Method D6891, the Sequence IVA test.)
- 4.1.1.4 Test Method D5119, the L-38 gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions. (An alternative is Test Method D6709, the Sequence VIII test.)
- ⁸ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1473.
- ⁹ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1471.
- ¹⁰ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1273.

- (1) Test Method D5119 (or Test Method D6709) is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.1.5 In addition to passing performance in the engine tests, specific viscosity grades shall also meet bench test requirements (see Table 1), which are discussed in the following subsections:
- (1) The volatility of engine oils is one of several factors that relates to engine oil consumption.
- (2) Test Method D6795, the EOFT screens for the formation of precipitates and gels that form in the presence of water and can cause oil filter plugging.
- (3) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency.
- (4) The flash point may indicate if residual solvents and low-boiling fractions remain in the finished oil.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
- (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test Method D6335, the TEOST test, may be useful in determining the deposit control of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low temperature protection not adequately measured by the Test Method D4684.
- 4.1.1.6 Licensing of the API SJ category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification. (See Appendix X3 for more information.)
- 4.1.2 *SL*—Oil meeting the performance requirements measured in the following gasoline engine tests and bench tests:
- 4.1.2.1 Test Method D6984, the Sequence IIIF gasoline engine test, is used to measure oil thickening and piston deposits under high temperature conditions and provides information about valve train wear. (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.2.2 Test Method D6891, the Sequence IVA gasoline engine test, has been correlated with the Sequence VE gasoline engine test in terms of overhead cam and slider follower wear control.⁸
- 4.1.2.3 Test Method D5302, the Sequence VE gasoline engine test, has been correlated with vehicles used in stopand-go service prior to 1988, with regard to valve train wear. It

¹¹ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1391.



TABLE 1 S Engine Oil Categories

	7.11	I SJ Category	
Engine Test Method	I Rated or Mea	sured Parameter	Primary Performance Criteria
05844 ^{A,B} (Sequence IID)	Average engine rust rating		8.5
(20400.002)	Number stuck lifters	,	none
r D6557 ^A (Ball Rust Test)	Average gray value, min		100
5533 ^{B,D} (Sequence IIIE)	0 0 1	viscosity increase at 40 °C,	64
(======================================	min	,	
	Average engine sludge rati	ina. ^C min	9.2
	Average piston skirt varnis		8.9
	Average oil ring land depos		3.5
	Lifter sticking	3,	none
	Scuffing and wear		
	Cam or lifter scuffing		none
	Cam plus lifter wear, µm		
	Average, max		30
	Maximum, max		64
	Ring sticking (oil-related) ^E		none
or D6984 (Sequence IIIF) ^D	Kinematic viscosity, % incr	ease at 40 °C. max	325 ^F
	Average piston skirt varnis		8.5^G
	Weighted piston deposit ra		3.2^G
	Screened average cam-plu		20 ^{G,I}
	Hot stuck rings	inter wear, pm, max	none ^G
D7320 (Sequence IIIG) ^J	Kinematic viscosity, % incr	ose at 40 °C may	150
Oequence ma)	Weighted piston deposit ra		3.5
	·	•	
	Cam-plus-lifter wear avg, µ	iiii, illax	60
EDOOB! (Common ME)	Hot stuck rings	ina C min	none
5302 ^{B,L} (Sequence VE)	Average engine sludge ration		9.0
	Rocker arm cover sludge r		7.0
	Average piston skirt varnis	3 ,	6.5
	Average engine varnish rat	ting, ^c min	5.0
	Oil ring clogging, %		report
	Oil screen clogging, %, ma		20.0
	Compression ring sticking	(hot stuck)	none
	Cam wear, µm		
	Average, max		127
	Maximum, max	d <mark>ards.iteh.</mark> a	380
D6891 (Sequence IVA) ^L	Average cam wear, µm ^M		120
lus, D6593 ^L	Average engine sludge rati	ing, ^C min	7.8
Sequence VG)	Rocker arm cover sludge r		8.0
. ,	Average piston skirt varnis		7.5
	Average engine varnish ra		8.9
		O,	
	9 9	ax	
	Oil screen clogging, %, ma		20
5119 ^O (L-38)	Oil screen clogging, %, ma Hot stuck compression ring	gs 105 110	20 none
1/ 1 1 1 1	Oil screen clogging, %, ma Hot stuck compression ring Bearing weight loss, mg, m	gs nax485-11c	20 none 40
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r D6709° (Sequence VIII)	Oil screen clogging, %, ma Hot stuck compression ring Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m Shear stability	SAE 0W-20,	20 none 40 0d36225a9/as 26.4 26.4 P
r D6709 ^O (Sequence VIII)	Oil screen clogging, %, ma Hot stuck compression ring Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m	SAE 0W-20, SAE 5W-20, SAE 5W-20,	20 none 40 0d36225a9/as 26.4 26.4 P
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D6709 ^o (Sequence VIII) Bench Test and Meast Method D5800 volatility loss,	Oil screen clogging, %, ma Hot stuck compression ring Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m Shear stability	Viscosity Grad SAE 0W-20, SAE 5W-20, SAE 5W-30,	20 none 40 26.4 4485-11c de Performance Criteria All Others
D6709 ^o (Sequence VIII) Bench Test and Meast Method D5800 volatility loss,	Oil screen clogging, %, ma Hot stuck compression ring Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m Shear stability Bearing weight loss, mg, m Shear stability	Viscosity Grad SAE 0W-20, SAE 5W-20, SAE 5W-30, SAE 10W-30	20 none 40 0d36225a9/asi26.4 de Performance Criteria All Others 20 ^R 15 ^R
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TABLE 1 Continued

Viscosity Grade Performance Criteria		
SAE 0W-20,		
,	All Others	
SAE 5W-30,		
SAE 10W-30		
12	NR^T	
	SAE 5W-20, SAE 5W-30, SAE 10W-30	

		CAE 10VV 00
Test Method D5133 Gelation I	ndex, max	12 NR ^T
	API SL Categ	ory
Engine Test Method	Rated or Measured Paramet	er Primary Performance Cri
D6984 (Sequence IIIF)	Kinematic viscosity, % increase at 40 °C, max	275
	Average piston skirt varnish rating, c min	9.0
	Weighted piston deposit rating, H min	4.0
	Screened average cam-plus-lifter wear, µm, max	20'
	Hot Stuck Rings	none
	Low temperature viscosity performance Y	report
or D7320 (Sequence IIIG) ^J	Kinematic viscosity, % increase at 40 °C, max	150
	Weighted piston deposit rating, ^K min	3.5
	Cam-plus-lifter wear avg, µm, max	60
	Hot stuck rings	none
	Low temperature viscosity performance ^Z	report
D6891 (Sequence IVA)	Cam wear average, µm, ^M max	120
D5302 ^B	Cam wear average, µm, max	127
(Sequence VE ^{AA})	Cam wear max, µm, max	380
D6593	Cam wear max, pm, max	380
(Sequence VG)	Average engine sludge rating, c min	7.8
	Rocker arm cover sludge rating, min	8.0
	Average piston skirt varnish rating, ^C min	7.5
	Average engine varnish rating, min	8.9
	Oil screen clogging, %, max	20
	Hot stuck Compression rings	none
	Cold stuck rings	report
	Oil screen debris, %	report
D6709	Oil ring clogging, % Bearing weight loss, mg, max	26.4
(Sequence VIII)	Shear stability	20.4 P
Coquonos vini)	Bench Test and Measured Parameter	Performance Criteria
T+ M DOCET (D-II D.	Test), average gray value, min	CS.Itch.al) 100
Test Method D5800 volatility I	·	15
Test Method D6417 volatility I		raviaw 10
D6795 (EOFT), % flow reduct		T C V I C V V 50
D6794 (EOWTT), % flow redu	With 0.6 % H ₂ O	50
	With 0.6 % H₂O With 1.0 % H₂O	50
	- A CITIL / TO / / 10 //	11c 50
	With 2 0 0/ 11 0	50
https://standard.pital	With 3.0 % H ₂ O	lb-48c0-b6fc-9f00d36225a9/astr _{0.10} s4485-
	mass fraction priospriorus /6, max	0.10
	mass fraction phosphorus %, min	0.06
	lethod D5302 results are obtained)	
Test Method D892 foaming te		40/0
	Sequence I, max, foaming/settling	10/0
	Sequence II, max, foaming/settling	50/0
	Sequence III, max, foaming/settling ^V	10/0
	plending required) static foam max,	100/0 ^W
tendency/stability		X
Test Method D6922 homogen		^
0 1	erature deposits (TEOST MHT-4),	
deposit wt, mg, max	1 1 1 AB	45

^A Demonstrate passing performance in either Test Method D5844 or D6557.

Test Method D5133 (Gelation Index), max^{AB}

12^{AC}

^B Monitoring of this test method was discontinued in June 20, 2001. Valid test results shall predate the end of the last calibration period for the test stand in which this test method was conducted.

^C ASTM Deposit Rating Manual 20, available from ASTM Customer Relations, ASTM International, 100 Barr Harbor Drive, West Conshohocken, PA 19428-2959.

Demonstrate passing performance in either Test Method D5533 or D6984. However, an oil passing Test Method D6984 and containing less than 0.08 % mass phosphorus in the form of ZDDP shall also pass the wear limits in Test Method D5302 (see also footnote J). An oil-related stuck ring occurs on a piston with an individual oil ring land deposit rating <2.6.

F Determine at 60 h.

^G Determine at 80 h.

H Determine weighted piston deposits by rating the following piston areas and applying the corresponding weightings: undercrown, 10 %; second land, 15 %; third land, 30 %; piston skirt, 10 %; first groove, 5 %; second groove, 10 %; and third groove, 20 %. Use ASTM Deposit Rating Manual 20 for all ratings.

Calculate by eliminating the highest and lowest cam-plus-lifter wear results and then calculating an average based on the remaining ten rating positions.

For oils containing at least 0.06 % mass phosphorus in the form of ZDDP, demonstrating passing performance in the Sequence IIIG test obviates the need to also conduct Test Method D5302 (Sequence VE), which was previously required for oils with less than 0.08 % mass phosphorus.

^K Unlike the Sequence IIIF test, piston skirt varnish rating is not required in the Sequence IIIG test.

^L Demonstrate passing performance in Test Method D5302, or alternatively, in both Test Method D6891 and Test Method D6593.

M Determine cam wear according to Test Method D6891. Seven wear measurements are made on each cam lobe and the seven measured values are added to obtain an individual cam lobe wear result. The overall cam wear value is the average of the twelve individual cam lobe wear results.



- ^N Determine the average engine varnish rating by averaging the piston skirt, right rocker arm cover, and left rocker arm cover varnish ratings. Use ASTM Deposit Rating Manual 20 for all ratings.
- O Demonstrate passing performance in either Test Method D5119 or D6709.
- $^{\it P}$ Ten-hour stripped kinematic viscosity (oil shall remain in original viscosity grade).
- ^Q Meet the volatility requirement in either Test Method D5800, D5480, or D6417.
- ^R Passing volatility loss only required for SAE 15W-40 oils.
- ^S This is a noncritical specification as described in Practice D3244.
- ^TNR stands for Not Required.
- U Meet either Test Method D92 or Test Method D93 flash point requirement.
- ^V Determine settling volume, in mL, at 10 min.
- ^W Determine settling volume, in mL, at 1 min.
- X Homogeneous with SAE reference oils.
- Y Evaluate the 80 h test oil sample by Test Method D4684 at the temperature indicated by the low temperature grade of oil as determined on the 80 h sample by Test Method D5293
- ^Z Measure the viscosity of the EOT oil sample by Test Method D4684. The measured viscosity shall meet the requirements of the original grade or the next higher grade. The EOT sample can be either from a Sequence IIIG or a Sequence IIIGA test. (A Sequence IIIGA test is identical to a Sequence IIIG test, except only low temperature viscosity performance is measured.) Additional details are provided in the Sequence IIIG test method, in Section 13.6.
- AA Not required for oils containing a minimum of 0.08 % mass phosphorus in the form of ZDDP.
- AB Requirement applies only to SAE 0W-20, 5W-20, 0W-30, 5W-30, and 10W-30 viscosity grades.
- ^{AC} For gelation temperatures at or above the W grade pumpability temperature as defined in SAE J300.

is included in the SL performance specification to augment assessment of the wear control performance of oils containing less than 0.08 % mass of phosphorus from ZDDP additive.

Note 1-Prior to May 2004, the API SH, SJ, and SL categories required that oils with passing Test Method D6984 (Sequence IIIF) results, and containing less than 0.08 % mass phosphorus in the form of ZDDP, also demonstrate passing performance in Test Method D5302 (Sequence VE). This requirement was included to address concerns over adequate wear protection with low levels of ZDDP. However, Test Method D5302 has not been available to industry for some time, and an alternative method was needed. In a related activity, the next level of gasoline engine oil performance, the ILSAC GF-4 standard, was developed outside the normal ASTM consensus process. Deliberations during the GF-4 development process included careful consideration of the suitability of Test Method D7320, the Sequence IIIG, a new test, to evaluate the wear protection of oils with less than 0.08 % mass phosphorus. Data on oils with less than 0.08 % mass phosphorus in the form of ZDDP were reviewed by members of the D02.B0 Passenger Car Engine Oil Classification Panel (PCEOCP). These data were from Test Method D7320 (Sequence IIIG) tests and from field tests on large populations of older vehicles with different engine types. Based on these data, the PCEOCP recommended a ballot to allow the use of Test Method D7320 (Sequence IIIG) as an alternative to Test Method D6984 (Sequence IIIF) plus Test Method D5302 (Sequence VE) for demonstration of acceptable API SH, SJ, and SL performance on low phosphorus oils, establishing at least the mass fraction of phosphorus is 0.06% as the minimum level. That ballot was approved by Subcommittee D02.B0 in May 2004.

- 4.1.2.4 Test Method D6593, the Sequence VG gasoline engine test, has been correlated with the Sequence VE gasoline engine test and with vehicles used in stop-and-go service prior to 2000, with regard to sludge and varnish deposit control.
- 4.1.2.5 Test Method D6709, the Sequence VIII gasoline engine test, is used to measure copper-lead bearing weight loss under high-temperature operating conditions and has been shown to correlate with the L-38 gasoline engine test.⁹
- (1) The Sequence VIII gasoline engine test is also used to determine the ability of an oil to resist permanent viscosity loss due to shearing in an engine.
- 4.1.2.6 In addition to passing performance in the engine tests, oils shall also meet bench test requirements (see Table 1), which are discussed in the following subsections:
- (1) Test Method D6557 (Ball Rust Test), was developed to replace the Sequence IID gasoline engine test, and evaluates the ability of an oil to prevent the formation of rust under short-trip service conditions.

- (2) The volatility of engine oils is one of several factors that relates to engine oil consumption. For this engine oil category, volatility is measured by Test Methods D5800 and D6417.
- (3) Test Method D6795, the Engine Oil Filterability Test (EOFT) and Test Method D6794, the Engine Oil Water Tolerance Test (EOWTT) screen for the formation of precipitates and gels which form in the presence of water and can cause oil filter plugging.
- (4) Phosphorus compounds in excessive amounts can cause glazing of automotive catalysts and exhaust gas oxygen sensors and, thereby, deactivate them. Control of the phosphorus level in the engine oil may reduce this tendency. For this engine oil category, phosphorus content is measured by either Test Method D4951 or D5185.
- (5) Excessive foaming in engine oil can cause valve lifter collapse and a loss of lubrication due to the presence of air in the oil. Test Methods D892 and D6082 empirically rate the foaming tendency and stability of oils.
- (6) Test Method D6922, the H and M Test indicates the compatibility of an oil with standard test oils.
- (7) Newer engines designed to provide increased power and improved driveability and to meet future federal emissions and fuel economy requirements may be sensitive to internal deposits caused by elevated engine operating temperatures. Test Method D7097, the TEOST MHT-4 test may be useful in determining the piston deposit control capability of oils recommended for these engines.
- (8) Test Method D5133, the Gelation Index technique, might identify oils susceptible to air binding and might provide low-temperature protection not adequately measured by Test Method D4684.
- 4.1.2.7 Licensing of the API SL category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.3 *CH-4*—Oil meeting the performance requirements measured in the following diesel and gasoline engine tests and bench tests.

- 4.1.3.1 Test Method D6750, the 1K diesel engine test, has been correlated with vehicles equipped with engines used in high speed operation prior to 1989, particularly with respect to aluminum piston deposits and oil consumption when the mass fraction of sulfur content is nominally $0.4\,\%$. ¹⁰
- 4.1.3.2 Test Method D6681, the 1P diesel engine test, has been used to predict iron piston deposit formation and oil consumption in four-stroke-cycle, direct injection, diesel engines that have been calibrated to meet 1998 U.S. federal exhaust emissions requirements for heavy duty engines operated on fuel containing the mass fraction of sulfur less than 0.05 %.¹²
- 4.1.3.3 Test Method D6483, the T-9 diesel engine test, has been correlated with vehicles equipped with engines used in high speed operation prior to 1998, particularly in regard to ring and liner wear and used oil lead content. (Alternatives are Test Method D6987/D6987M, the T-10 diesel engine test—see 4.1.4.2, and Test Method D7422, the T-12 diesel engine test—see 4.1.3.2.)
- 4.1.3.4 Test Method D5967 extended, the T-8E engine test, has been shown to generate soot-related oil thickening in a manner similar to 1998 emissions-controlled heavy duty diesel engines using electronic injection control systems.
- 4.1.3.5 Test Method D6838, The M11 High Soot diesel engine test has been correlated with vehicles equipped with four-stroke-cycle diesel engines used in high speed operations prior to 1998, particularly with regard to soot related valve train wear, filter plugging, and sludge control. (An alternative is Test Method D7468, the Cummins ISM diesel engine test. See 4.1.5.5.)
- 4.1.3.6 Test Method D5966, the Roller Follower Wear Test, has been correlated with hydraulic roller cam follower pin wear in medium-duty indirect injection diesel engines used in broadly based field operations.
- 4.1.3.7 Test Method D6984, the Sequence IIIF test, is used to measure bulk oil viscosity increase, which indicates an oil's ability to withstand the higher temperatures found in modern diesel engines. (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.3.8 Test Method D6894, the EOAT has been correlated with oil aeration in diesel engines equipped with HEUI used in medium-duty diesel engines.¹⁵
- 4.1.3.9 Test Method D892, a foaming test, Sequences I, II and III, has been shown to predict foaming of engine oils in diesel engines.
- 4.1.3.10 Test Method D6594 operated at 135 °C, a High Temperature Corrosion Bench Test (HTCBT), has been shown to predict the corrosion of engine oil-lubricated copper and lead containing components used in diesel engines.
- 4.1.3.11 Test Method D6278, the Diesel Injector Shear Test, has been shown to correlate with permanent shear loss of

- engine oils in medium-duty direct injection diesel engines used in broadly based field operations.
- 4.1.3.12 Test Method D5800, Noack Volatility or, alternatively, Test Method D6417, are used to measure engine oil volatility loss under high temperature operating conditions.
- 4.1.3.13 Licensing of the API CH-4 category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.4 *CI-4*—Oil meeting the performance requirements measured in the following diesel and gasoline engine tests and bench tests.
- 4.1.4.1 Test Method D6923, the 1R single cylinder diesel engine test is used to measure engine oil performance with respect to piston deposits, oil consumption, piston and piston ring scuffing, and ring sticking using a two-piece iron/aluminum piston similar to that used in modern, production heavy-duty diesel engines. (An alternative is Test Method D6681, the 1P diesel engine test, see 4.1.3.2.
- 4.1.4.2 Test Method D6987/D6987M, the T-10 diesel engine test, is used to measure engine oil performance with respect to piston ring and cylinder liner wear, bearing lead corrosion, and oil consumption in an electronically governed, open chamber, in-line six-cylinder, four-stroke cycle, turbocharged, compression-ignition engine with exhaust gas recirculation. (An alternative is Test Method D7422, the T-12 diesel engine test, see 4.1.5.2.)
- 4.1.4.3 Test Method D6975, the M11 EGR heavy-duty diesel engine test, is used to evaluate oil performance with respect to valve train wear, sludge deposits, and oil filter plugging in an exhaust gas recirculation environment. (An alternative is the Cummins ISM diesel engine test. See 4.1.5.5.)
- 4.1.4.4 Test Method D5967 extended, the T-8E engine test, has been shown to generate soot-related oil thickening in a manner similar to 1998 emissions-controlled heavy-duty diesel engines using electronic injection control systems.
- 4.1.4.5 Test Method D6984, the Sequence IIIF gasoline engine test, is used to measure oil thickening under high temperature conditions in spark-ignition engines. (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.4.6 Test Method D6750 (1K), the 1K diesel engine test, or, alternatively, Test Method D6750 (1N), the 1N diesel engine test, is used to evaluate performance in diesel engines equipped with aluminum pistons. The 1K test has been correlated with vehicles used in high speed operation prior to 1989, particularly with respect to aluminum piston deposits and oil consumption, when the mass fraction of fuel sulfur was nominally 0.4 %. The 1N test has been used to predict aluminum piston deposit formation in four-stroke cycle, directinjection, diesel engines that have been calibrated to meet 1994 U.S. federal exhaust emissions requirements for heavy-duty engines operated on fuel containing the mass fraction of sulfur less than 0.05 %.
- 4.1.4.7 Test Method D5966, the Roller Follower Wear Test, has been correlated with hydraulic roller cam follower pin wear

¹² Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1441.

¹³ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1440.

¹⁴ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1439.

¹⁵ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1379.



TABLE 2 Energy Conserving Categories

	SJ-Related Energy Conse	erving Category
Test Procedure	SAE Viscosity Grade	Primary Performance Criteria ^A
D6202 (Sequence VIA)	0W-20 and 5W-20	FEI ^B relative to BC ^C , 1.4 %, min
D6837 (Sequence VIBSJ)	0W-20 and 5W-20	FEI^D relative to BC^C , 1.7 %, min
D6202 (Sequence VIA)	other 0W- and 5W-multi-grades	FEI ^B relative to BC, 1.1 %, min
D6837 (Sequence VIBSJ)	other 0W- and 5W-multi-grades	FEI ^D relative to BC, 1.3 %, min
D6202 (Sequence VIA)	all 10W-multi-grades	FEI ^B relative to BC, 0.5 %, min
D6837 (Sequence VIBSJ)	all 10W-multi-grades	FEI ^D relative to BC, 0.6 %, min
D6202 (Sequence VIA)	all others	FEI ^B relative to BC, 0.5 %, min
D6837 (Sequence VIBSJ)	all others	FEID relative to BC, 0.6 %, min
	SL-Related Energy Conse	erving Category
Test Procedure	SAE Viscosity Grade	Primary Performance Criteria
D6837 (Sequence VIB)	0W-20 and 5W-20	FEI 1 ^E relative to BC, 2.0 %, min, <i>and</i> FEI 2 ^F relative to BC, 1.7 % min
D6837 (Sequence VIB)	0W-30 and 5W-30	FEI 1 ^E relative to BC, 1.6 %, min, and FEI 2 ^F relative to BC, 1.3 % min, and sum of FEI 1 and FEI 2 relative to BC, 3.0 % min
D6837 (Sequence VIB)	all others	FEI 1 ^E relative to BC, 0.9 %, min, and FEI 2 ^F relative to BC, 0.6 % min, and sum of FEI 1 and FEI 2 relative to BC, 1.6 %, min

^A Passing performance shall be demonstrated in either Test Method D6202 (Sequence VIA) or Test Method D6837 (Sequence VIB). A passing result in only one of these procedures is required.

^B Fuel Economy Improvement (FEI) measured against the performance of BC run before and after the candidate oil, according to the requirements of the Sequence VIA

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in medium-duty indirect injection diesel engines used in broadly based field operations.

- 4.1.4.8 Test Method D6894, the EOAT procedure, has been correlated with oil aeration in diesel engines equipped with HEUI used in medium-duty diesel engines.
- 4.1.4.9 Test Methods D4171, D4683, and D5481 High Temperature High Shear (HTHS) tests are part of the SAE J300 Viscosity Classification System.
- 4.1.4.10 Test Method D4684 (MRV TP-1) has been shown to predict field failures resulting from poor low temperature pumpability.
- 4.1.4.11 Test Method D5800, Noack Volatility, is used to measure engine oil volatility loss under high temperature operating conditions.
- 4.1.4.12 Test Method D6594 operated at 135°C, a high temperature corrosion bench test (HTCBT), has been shown to predict corrosion of engine oil-lubricated copper and lead containing components used in diesel engines.
- 4.1.4.13 Test Method D6278, a diesel injector shear test, has been shown to correlate with permanent shear loss of engine oils in medium-duty direct injection diesel engines used in broadly based field operations.
- 4.1.4.14 Test Method D892, a foaming test, Sequences I, II, and III, has been shown to predict foaming of engine oils in diesel engines.

- 4.1.4.15 Test Method D7216, the Elastomer Compatibility Test is used to measure the performance of four widely used elastomer compounds when exposed to diesel engine oils.
- 4.1.4.16 Licensing of the API CI-4 category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.5 *CJ-4*—Oil meeting the performance requirements measured in the following diesel and gasoline engine tests, and bench and chemical tests.
- 4.1.5.1 Test Method D7156, the Mack T-11 diesel engine test has been shown to generate soot-related oil thickening in a manner similar to 2002 EGR emission-controlled heavy-duty engines with electronic injection control. This engine test uses fuel with sulfur content of 500 mg/kg.
- 4.1.5.2 Test Method D7422, the Mack T-12 diesel engine test is used to measure engine oil performance with respect to piston ring and cylinder liner wear, bearing corrosion, and oil consumption, using an in-line six cylinder, four-stroke, direct injection, turbo-charged engine with exhaust gas recirculation at levels expected for 2007 emission control engines. This engine test uses fuel with ultra low sulfur content of 15 mg/kg.

^B Fuel Economy Improvement (FEI) measured against the performance of BC run before and after the candidate oil, according to the requirements of the Sequence VIA procedure.

^C BC is the designation for the reference oil. In practice, dashed suffixes are used to indicate sequential batches of the reference oil. The minimum FEI values shown in Table 2 for the Sequence VIA were established for performance against Batch 2, and for the Sequence VIB against Batch 3. Performance requirements against currently approved batches of the reference oil can be provided by the ASTM Test Monitoring Center, 6555 Penn Ave., Pittsburgh, PA 15206-4489.

^D If the Sequence VIB is used to determine SJ-related Energy Conserving performance, calculate FEI at 16 h and base the comparison only to the BC run before the candidate. No BC stage after the candidate is required.

^E FEI 1 is fuel economy improvement measured after 16 h of candidate oil aging and compared to a ratio of results obtained with BC run before and after the candidate oil, according to the requirements of the VIB procedure.

FEI 2 is fuel economy improvement measured after 80 h of additional candidate oil aging beyond the 16 h aging used to establish FEI 1 (see Footnote E).

- 4.1.5.3 Test Method D7549, the Caterpillar C13 Advanced Combustion Emission Reduction Technology (ACERT) is an in-line six-cylinder engine used to measure engine oil consumption and piston deposits. The engine is equipped with a single-piece forged steel piston used in emission controlled engines. This engine test uses fuel with ultra low sulfur content of 15 mg/kg.
- 4.1.5.4 Test Method D7484, the Cummins ISB diesel engine test is used to evaluate oil performance with respect to cam and tappet wear with high soot level in the engine oil. This is an in-line six cylinder turbo-charged engine with a common-rail fuel system for emission control. This engine test uses fuel with ultra low sulfur content of 15 mg/kg.
- 4.1.5.5 Test Method D7468, the Cummins ISM diesel engine test is used to evaluate oil performance with respect to valve train wear, sludge and oil filter plugging with a high soot level in the engine oil. This is an in-line six cylinder, turbo-charged engine with EGR for emission control. This engine test uses fuel with sulfur content of 500 mg/kg.
- 4.1.5.6 Test Method D6750, the 1N diesel engine test, has been used to predict piston deposit formation in four-stroke cycle, direct injection, diesel engines that have been calibrated to meet 1994 U.S. federal exhaust emissions requirements for heavy-duty engines operated on fuel containing the mass fraction of sulfur less than 0.05 %.
- 4.1.5.7 Test Method D6984, the Sequence IIIF test, is used to measure bulk oil viscosity increase, which indicates an oil's ability to withstand the higher temperatures found in modern diesel engines. (An alternative is Test Method D7320, the Sequence IIIG test.)
- 4.1.5.8 Test Method D5966, the roller follower wear test (RFWT), has been correlated with hydraulic roller cam follower pin wear in medium-duty indirect injection diesel engines used in broadly based field operations.
- 4.1.5.9 Test Method D4684 (MRV TP-1) has been shown to predict field failures resulting from poor low temperature pumpability.
- 4.1.5.10 Test Method D7109, a diesel injector shear test, has been shown to correlate with permanent shear loss of engine oils in medium-duty direct injection diesel engines used in broadly based field operations.
- 4.1.5.11 Test Method D6594 operated at 135°C, a high temperature corrosion bench test (HTCBT), has been shown to predict corrosion of engine oil-lubricated copper and lead containing components used in diesel engines.
- 4.1.5.12 Test Methods D4171, D4683, and D5481 High Temperature High Shear (HTHS) tests are part of the SAE J300 Viscosity Classification System.
- 4.1.5.13 Test Method D892, a foaming test, Sequences I, II, and III, has been shown to predict foaming of engine oils in diesel engines.
- 4.1.5.14 Test Method D7216, the Elastomer Compatibility Test, is used to measure the performance of four widely used elastomer compounds when exposed to diesel engine oils.
- ¹⁶ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1321.

- 4.1.5.15 Test Method D6894, the EOAT procedure, has been correlated with oil aeration in diesel engines equipped with HEUI used in medium-duty diesel engines.
- 4.1.5.16 Licensing of the API CJ-4 category requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.
- 4.1.6 Energy Conserving Associated With SJ—As defined by Test Method D6202 or Test Method D6837, oil meeting performance requirements in Table 2.
- 4.1.6.1 Test Method D6202 has been correlated with the EPA FTP 75 vehicle test cycle using vehicles with engine types that represent a cross-section of engine technology circa 1996 in order that passing oils will demonstrate fuel economy benefits in consumer vehicle service.
- 4.1.6.2 Test Method D6837¹⁷ test has been correlated with the EPA FTP 75 vehicle test cycle using vehicles with engine types that represent a cross-section of current engine technology in order that passing oils will demonstrate fuel economy benefits in consumer vehicle service.
- 4.1.7 Energy Conserving Associated With SL—As defined by Test Method D6837, oil meeting performance requirements in Table 2.

Note 2—Energy-conserving oils are also described in SAE J1423.

4.1.8 Licensing of the Energy Conserving category as defined by Test Method D6202 or as defined by Test Method D6837 requires that candidate oils meet the performance requirements in this specification, and that the oils be tested in accordance with the protocols described in the ACC Petroleum Additives Product Approval Code of Practice. The methodology detailed in the ACC Code will help ensure that an engine oil meets its intended performance specification.

5. Performance Requirements

5.1 The oils identified by the categories discussed in Section 4 shall conform to the requirements listed in Tables 1-3.

Note 3—API has developed a symbol that can be licensed for use on containers of oils that conform to the requirements of one or more categories that are currently of commercial importance. API 1509 describes the symbol and licensing procedure.

Note 4—In practice, engine oils are often labeled with service category designations having some combination of both S and C prefixes.

Note 5—Intended service applications for the various categories described in 4.1.1 – 4.1.7 can be found in API 1509. Applicable sections of that publication have been included in Appendix X2.

6. Test Procedures

- 6.1 The requirements listed in this specification shall be determined in accordance with those standard test methods listed in Section 2.
- 6.2 Engine tests are run in test stands calibrated using reference oils.

 $^{^{17}}$ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D02-1469.



TABLE 3 C Engine Oil Categories

Category	Test Method	Rated or Measured Parameter	Prin	nary Performance Cr	iteria
			One-test	Two-test ^A	Three-test ^A
H-4	D6681 (1P) ^B	Weighted demerits (WDP), max	350	378	390
		Top groove carbon (TGC), demerits, max	36	39	41
D6750 (1K) ^D		Top land carbon (TLC), demerits, max	40	46	49
		Average Oil Consumption, g/h (0-360 h), max	12.4	12.4	12.4
		Final Oil Consumption, g/h (312-360 h), max	14.6	14.6	14.6
		Piston, ring, and liner scuffing	none	none	none ^C
	D6750 (1K) ^D	Weighted demerits (WDK), %, max	332	347	353
	,	Top groove fill (TGF), %, max	24	27	29
		Top land heavy carbon (TLHC), %, max	4	5	5
		Average Oil Consumption, g/MJ (0-252) h, max	0.139	0.139	0.139
	Do (00 (T.0)	Piston, ring, and liner scuffing	none	none	none ^C
	D6483 (T-9)	Average Liner Wear, normalized to 1.75 % soot, µm max	25.4	26.6	27.1
		Average Top Ring Weight Loss, mg max ^E	120	136	144
		EOT Used Oil Lead Content less New Oil Lead			
		Content, mg/kg, max	25	32	36
	or, D6987/D6987M (T-10)	Liner wear, µm, max	32	34	35
	o., 2000//2000/ (1 10)	Ring wear, mg, max	150	159	163
		Lead content at EOT, mg/kg, max	50	56	59
	or, D7422 (T-12)	Liner wear, µm, max	30.0	30.8	31.1
		Top Ring Weight Loss, mg, max	120	132	137
		Lead content at EOT, mg/kg, max	65	75	79
	D5966 (RFWT)	Average Pin Wear, mils, max	0.30	0.33	0.36
	()	(μm) max	(7.6)	(8.4)	(9.1)
	D6929 (M11)F	. ,	(1.0)	(0.7)	(3.1)
	D6838 (M11) ^F	Rocker Pad Average Wt. Loss, normalized to 4.5 % soot,	0.5	7.5	0.0
		mg max	6.5	7.5	8.0
		Oil Filter Differential Pressure at EOT, kPa max	79	93	100
		Average Engine Sludge, CRC Merits at EOT, min	8.7	8.6	8.5
	or, D7468 (ISM)	Crosshead wear, mg, max	7.5	7.8	7.9
	o., 27 .00 (.o)	Oil filter delta pressure, at 150 h, kPa, max	79	95	103
		1 ' ' '			
	D-00- (F . T 0F) G	Sludge rating, CRC merits, min	8.1	8.0	8.0
	D5967 (Ext. T-8E) ^G	Relative Viscosity at 4.8 % Soot by			
		TGA, max	2.1	2.2	2.3
		Viscosity increase at 3.8 % Soot by TGA, mm ² /s, max	11.5	12.5	13.0
	D6984 (Sequence IIIF)	60 h Viscosity at 40 °C, increase from 10 min sample, %			
	(max US 6// Stall UI all UIS 61	295	295 (MTAC) ^H	295 (MTAC) ^H
	or D7320 (Sequence IIIG)	Kinematic viscosity, % increase at 40 °C max	150	150 (MTAC)	150 (MTAC)
	· •	•			
	D6894 (EOAT) ^J	Aeration, volume, % max	8.0	8.0 (MTAC) ^H	8.0 (MTAC) ^H
	D6594 (135 °C, HTC BT)	Used Oil Elemental Concentration			
		Copper, mg/kg increase, max	20		
		Lead, mg/kg increase, max	120		
		Tin, mg/kg increase	report		
		Copper strip rating, max TM D4485-11	3		
	Deco (Ontion A		3		
	D892 (Option A	Foaming/Settling, mL, max			
	not allowed) In all Calla				
		Sequence I	10/0		
			10/0		
		·	20/0		
		Sequence II	20/0		
		·	20/0 10/0	SAE 15W 40	
	DE000	Sequence II Sequence III	20/0 10/0 SAE 10W-30	SAE 15W-40	
	D5800 or	Sequence II Sequence III % volatility loss at 250°C, max	20/0 10/0 SAE 10W-30 20	18	
	D6417	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max	20/0 10/0 SAE 10W-30 20 17	18 15	
		Sequence II Sequence III % volatility loss at 250°C, max	20/0 10/0 SAE 10W-30 20	18	
	D6417	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max	20/0 10/0 SAE 10W-30 20 17	18 15	
	D6417	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing,	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3	18 15 SAE XW-40 12.5	Three-test ^M
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test ^M	Three-test ^M
-4	D6417	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test	18 15 SAE XW-40 12.5 Two-test ^M 396	402
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52	18 15 SAE XW-40 12.5 Two-test ^M 396 57	402 59
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35	402 59 36
I-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC),	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52	18 15 SAE XW-40 12.5 Two-test ^M 396 57	402 59
l-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35	402 59 36
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1	402 59 36
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption,	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35	402 59 36 13.1
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1	402 59 36 13.1 IOC + 1.8
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8	402 59 36 13.1 IOC + 1.8
-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none	402 59 36 13.1 IOC + 1.8 none none
-4	D6417 D6278	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378	402 59 36 13.1 IOC + 1.8
-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none	402 59 36 13.1 IOC + 1.8 none none
-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39	402 59 36 13.1 IOC + 1.8 none none 390 41
-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46	402 59 36 13.1 IOC + 1.8 none none 390 41 49
l-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4
1-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6
-4	D6417 D6278 D6923 (1R) or, D6681 (1P)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none
-4	D6417 D6278 D6923 (1R)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6
-4	D6417 D6278 D6923 (1R) or, D6681 (1P)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing Merit rating, M min	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none 1000	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6 none 1000	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none 1000
-4	D6417 D6278 D6923 (1R) or, D6681 (1P) D6987/D6987M (T-10) or the T-12 (T-10) test	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing Merit rating, M min Merit rating, M min	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none 1000 1000	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6 none 1000 1000	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none 1000 1000
I-4	D6417 D6278 D6923 (1R) or, D6681 (1P)	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing Merit rating, M min Merit rating, M min Merit rating, M min Average crosshead wt. loss, mg, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none 1000 1000 20.0	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6 none 1000 1000 21.8	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none 1000 1000 22.6
-4	D6417 D6278 D6923 (1R) or, D6681 (1P) D6987/D6987M (T-10) or the T-12 (T-10) test	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing Merit rating, M min Merit rating, M min Average crosshead wt. loss, mg, max Average top ring weight loss, mg	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none 1000 1000 20.0 report	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6 none 1000 1000 21.8 report	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none 1000 1000 22.6 report
l-4	D6417 D6278 D6923 (1R) or, D6681 (1P) D6987/D6987M (T-10) or the T-12 (T-10) test	Sequence II Sequence III % volatility loss at 250°C, max % volatility loss at 371°C, max Kinematic Viscosity after shearing, mm²/s, min Weighted demerits (WDR), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Initial oil consumption (IOC), (0-252 h), g/h, average Final oil consumption, (432-504 h), g/h, average, max Piston, ring, and liner distress Ring sticking Weighted demerits (WDP), max Top groove carbon (TGC), demerits, max Top land carbon (TLC), demerits, max Average oil consumption, g/h (0-360 h), max Final oil consumption, g/h (312-360 h), max Piston, ring, and liner scuffing Merit rating, M min Merit rating, M min Merit rating, M min Average crosshead wt. loss, mg, max	20/0 10/0 SAE 10W-30 20 17 SAE XW-30 9.3 One-test 382 52 31 13.1 IOC + 1.8 none none 350 36 40 12.4 14.6 none 1000 1000 20.0	18 15 SAE XW-40 12.5 Two-test ^M 396 57 35 13.1 IOC + 1.8 none none 378 39 46 12.4 14.6 none 1000 1000 21.8	402 59 36 13.1 IOC + 1.8 none none 390 41 49 12.4 14.6 none 1000 1000 22.6