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Petroleum and natural gas industries — Drilling and production equipment — Offshore conductor design, setting depth and installation

Industries du pétrole et du gaz naturel — Équipements de forage et de production — Conception des tubes conducteurs en mer, profondeur de mise en place et installation

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 67, Materials, equipment and offshore structures for petroleum, petrochemical and natural gas industries, Subcommittee SC 4, Drilling and production equipment, in collaboration with the European Committee for Standardization (CEN) Technical Committee CEN/TC 12, Materials, equipment and offshore structures for petroleum, petrochemical and natural gas industries, in accordance with the Agreement on technical cooperation between ISO and CEN (Vienna Agreement).

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

This document provides requirements and guidance on the design, setting depth, and installation of offshore conductors used by the petroleum and natural gas industries worldwide. Sound engineering judgment is necessary in the use of this document.

Conductor design addresses actions and action combinations, strength and stability checks, and fatigue checks. Setting depth provides calculation methodologies for different installation methods. Installation identifies relevant methods and their applicability together with corresponding procedures as well as documentation and quality control requirements.

Some background to and guidelines on the use of this document is provided in Annex A.

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Petroleum and natural gas industries — Drilling and production equipment — Offshore conductor design, setting depth and installation

1 Scope

This document specifies the requirements and recommendations for the design, setting depth and installation of conductors for the offshore petroleum and natural gas industries. This document specifically addresses:

- design of the conductor, i.e. determination of the diameter, wall thickness, and steel grade;
- determination of the setting depth for three installation methods, namely, driving, drilling and cementing, and jetting;
- requirements for the three installation methods, including applicability, procedures, and documentation and quality control.

This document is applicable to:

- platform conductors: installed through a guide hole in the platform drill floor and then through guides attached to the jacket at intervals through the water column to support the conductor, withstand actions, and prevent excessive displacements;
- jack-up supported conductors: a temporary conductor used only during drilling operations, which
 is installed by a jack-up drilling rig. In some cases, the conductor is tensioned by tensioners attached
 to the drilling rig;
- free-standing conductors: a self-supporting conductor in cantilever mode installed in shallow water, typically water depths of about 10 m to 20 m. It provides sole support for the well and sometimes supports a small access deck and boat landing;
- subsea wellhead conductors: a fully submerged conductor extending only a few metres above the sea floor to which a BOP and drilling riser are attached. The drilling riser is connected to a floating drilling rig. The BOP, riser and rig are subject to wave and current actions while the riser can also be subject to VIV.

This document is not applicable to the design of drilling risers.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 19900, Petroleum and natural gas industries — General requirements for offshore structures

ISO 19901-4, Petroleum and natural gas industries — Specific requirements for offshore structures — Part 4: Geotechnical and foundation design considerations

ISO 19901-8, Petroleum and natural gas industries — Specific requirements for offshore structures — Part 8: Marine soil investigations

ISO 19902, Petroleum and natural gas industries — Fixed steel offshore structures

ISO 19906, Petroleum and natural gas industries — Arctic offshore structures

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at https://www.iso.org/obp
- IEC Electropedia: available at https://www.electropedia.org/

3.1

axial capacity

ability of conductor to resist vertical actions without soil failure

Note 1 to entry: The axial capacity of a conductor can change with time due to the soil disturbance and recovery.

3.2

conductor

tubular pipe set into the *seabed* (3.11) to provide the initial stable structural foundation for setting the *surface casing* (3.13) and protecting the internal well string from metocean actions

3.3

conductor shoe

short conductor joint whose upper end is connected to a whole conductor while its lower end has an internal chamfer to assist penetration

3.4 iTeh STANDARD PREVIEW

design situation

set of actions and combination of actions representing real conditions during a certain time interval, for which the design demonstrates that relevant limit states are not exceeded

3.5

drilling and cementing

method for installing a *conductor* (3.2) where a borehole is drilled, the conductor is lowered into the borehole and cement slurry placed in the annulus

3.6

driving

method for installing a *conductor* (3.2) where a vessel or rig is used to hammer the conductor into place

3.7

effective weight

weight in sea water or drilling fluid

3.8

jetting

method for installing a *conductor* (3.2) where the bottom hole assembly and conductor are combined, the borehole is washed by hydraulic force and the conductor simultaneously lowered into the hole

3.9

metocean action

effect of wind, wave and current on a conductor (3.2)

Note 1 to entry: The determination of these effects can include the influence of tide, surge, vortex induced vibrations and related processes.

3.10

sea floor

interface between the sea and the *seabed* (3.11) referring to the upper surface of all unconsolidated material

[SOURCE: ISO 19901-1:2015, 3.30]

3.11

seabed

materials below the sea in which the structure is founded, whether of soils such as sand, silt or clay, cemented material or of rock

Note 1 to entry: The seabed can be considered as the half-space below the sea floor (3.10).

[SOURCE: ISO 29400:2020, 3.128]

3.12

setting depth

distance between the depth reference point, usually the sea floor (3.10) or sea level, and the conductor shoe (3.3)

Note 1 to entry: A minimum setting depth is required to provide adequate axial capacity and formation integrity at the conductor shoe during surface casing drilling and cementing.

3.13

surface casing

casing that is run inside the *conductor* (3.2) to contain pressure in conjunction with the wellhead and blow-out preventer and to protect weak formations

undrained shear strength

maximum shear stress at yielding or at a specified maximum strain in an undrained condition

Symbols and abbreviated terms

4.1 Symbols

4.1.1	Symbols for conductor design	

4.1.1 Symbo	ls for conductor design ds/sist/e8d5c7c7-dc32-45f9-8d0a-3ecc979a939f/iso-
A	accidental actions 3421-2022
A_{cs}	cross-sectional area
C_{m}	moment reduction factor
D	deformation actions
D_{od}	outer diameter
D_{R}	Palmgren-Miner's sum or damage ratio during a certain time interval
E	Young's modulus of elasticity
$E_{\rm e}$	extreme quasi-static metocean actions due to wind, wave and current
E_{0}	metocean actions due to owner-specified operating wind, wave and current parameters
F_{d}	design value of action
f_{b}	representative bending strength
$f_{\rm c}$	representative axial compressive strength
$f_{ m e}$	Euler buckling strength

 $f_{\rm v}$

representative shear strength

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representative yield strength f_{y} Gpermanent actions moment of inertia of conductor cross-section Ι K effective length factor local experience factor K_{LE} L unbraced length calculated fatigue life L_{f} maximum bending moment on cross-section due to environmental actions and defor- $M_{\rm E}$ mation actions maximum bending moment on cross-section due to eccentricities of inner strings not $M_{\rm I}$ being centralized number of cycles to failure under constant amplitude stress range N_{i} number of cycles of stress range $n_{\rm i}$ Q variable actions conductor radius of gyration time period over which Palmgren-Miner's sum is determined Tt wall thickness utilization of conductor/standards/sist/e8d5c7c7-dc32-45t9-8d0a-3ecc979a939f/iso- $U_{\rm m}$ Vshear due to factored actions $Z_{\mathbf{p}}$ elastic section modulus plastic section modulus $Z_{\mathfrak{p}}$ partial action factor for extreme metocean action $\gamma_{\rm f.E.}$ partial action factors applied to the total quasi-static metocean actions plus equivalent quasi-static action representing dynamic response for operating and extreme metocean γ_{f,E_0} , γ_{f,E_0} conditions, respectively, and for which different values can be applicable for different design situations fatigue damage design factor $\gamma_{\rm FD}$ partial action factors for the various permanent, variable, deformation and accidental $\gamma_{\rm G}$, $\gamma_{\rm O}$, $\gamma_{\rm D}$, $\gamma_{\rm A}$ actions partial resistance factor for bending strength $\gamma_{R,b}$ partial resistance factor for axial compressive strength $\gamma_{\rm R.c}$ partial resistance factor for shear strength $\gamma_{\rm R.v}$ λ column slenderness parameter bending stress due to forces from factored actions σ_{b}

axial compressive stress due to forces from factored external axial actions of wellhead, $\sigma_{\rm ce}$

BOP, christmas tree, emergency equipment and Workover equipment

axial compressive stress due to forces from factored internal axial actions of inner cas- $\sigma_{
m ci}$

ings and tubing

maximum shear stress due to forces from factored actions $au_{
m b}$

4.1.2 Symbols for setting depth

side surface area $A_{\rm s}$

outer diameter $D_{\rm od}$

fluid density $ho_{
m fluid}$

partial safety factors $F_{\rm s1}$, $F_{\rm s2}$

axial force applied to the conductor during the BOP installation stage $F_{\rm xBOP}$

 $F_{\rm xcan}$ axial force applied to the conductor in the extreme design situation

 $F_{\rm xial}$ axial force in conductor

 $F_{\rm xsc}$ axial force applied to the conductor during the subsequent casings installation stage

 F_{xsur} axial force applied to the conductor during the surface casing installation stage

 $F_{\rm xXt}$ axial force applied to the conductor during the christmas tree and tubing installation stage

unit skin friction f(z)

acceleration due to gravity

Н jetted conductor setting depth in the seabed

minimum setting depth of the conductor h_{\min}

 $K_{\rm con}$ axial stiffness of the conductor

coefficient of lateral earth pressure K_0

axial stiffness of the coupled foundation composed of the surface casing and the conductor $K_{\rm cs}$

axial stiffness of the wellbore coupled system composed of all casings and the conductor $K_{\rm sys}$

length of conductor above the sea floor $L_{\rm a}$

 N_{load} axial force in conductor

 $P_{\rm f}$ soil fracture pressure

fluid circulation pressures $P_{\rm fluid}$

annular pressure loss of fluid P_1

conductor axial capacity immediately after jetting Q_0

skin friction resistance of conductor $Q_{\rm f}$

axial capacity of conductor $Q_{\rm r}$

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 $Q_{
m setup}$ set-up axial capacity of jetted conductor

 Q_{t} axial capacity of jetted conductor

R design safety factor of conductor capacity

S WOB utilization

 s_{ij} soil undrained shear strength

 $s_{\mathrm{u,ave}}$ mean soil undrained shear strength within the setting depth range

t time after the completing of jetting

u pore water pressure

 $W_{\rm BHA}$ effective weight of jetting BHA

 $W_{\rm BOP}$ effective weight of BOP

 W_{cap} effective weight of capping equipment

 $W_{\rm con}$ effective weight of conductor

 $W_{\rm cs}$ weight of cementing string in air

 $W_{\rm fc}$ weight of the fluid inside the cementing string

 $W_{\rm fdc}$ weight of the fluid displaced by the casing assembly

 W_{fs} weight of the fluid inside the surface casing

 W_{land} effective weight of surface casing during cementing $\frac{1}{2}$ 45/0-8d0a-3ecc979a939f/iso-

 $W_{\rm RT}$ effective weight of drill-ahead running tool

 $W_{\rm sc}$ weight of surface casing in air

 $W_{\rm squ}$ effective weight of subsequent casings after cementing

maximum action applied to the conductor from the time the surface casing is landed until

W_{sur} the cement is set

 W_{tub} effective weight of production tubing

 W_{WH} effective weight of wellhead housing

 $W_{
m WOB.last}$ last WOB recoded during jetting

 $W_{\rm XT}$ effective weight of christmas tree

 α_1 distribution coefficient for the effective weight of the BOP

 α_2 distribution coefficient for the effective weight of the subsequent casings

 $\Delta \alpha_{\mathsf{t}}$ soil set-up factor

 σ_3 minimum principal stress at the calculated depth

 $\sigma_h^{'}$ effective horizontal stress

 $\sigma_{\rm v}^{'}$ effective vertical stress, or overburden pressure α, β empirical coefficients of soil fracture pressure

4.2 Abbreviated terms

APB annular pressure build-up

BHA bottom hole assembly

BOP blow-out preventer

HFT hydraulic fracture test

LWD logging while drilling

OEM original equipment manufacturer

ROV remote operated vehicle

SCF stress concentration factors

VIV vortex induced vibrations

WOB weight on bit STANDARD PRRVIEW

5 General requirements and ards.iteh.ai)

5.1 General

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A conductor has the following main functions: 68d5c7c7-dc32-45f9-8d0a-3ecc979a939f/iso-

- a) to stabilize and to protect the near-surface sediments from collapse and fracturing under fluid pressures during surface casing drilling and cementing;
- to resist the effective weight of the first casing string (surface casing), which is landed shortly after installation of the conductor, or the first two casing strings if a liner is landed before the surface casing;
- c) as a composite system with the surface casing, to provide lateral stability for the well system and the BOP against cyclic and tensile loading from direct metocean actions, vessel motions and riser motions including VIV.

The exposure level of the well that a conductor supports shall be specified prior to the start of the design or assessment in accordance with ISO 19900.

5.2 Limit states for conductor design

Conductor design shall determine conductor outer diameter, wall thickness, steel grade and choice of connectors to satisfy design situations through all phases of the conductor's design service life, including the installation method.

The limit state approach shall be used for conductor design and assessment. ISO 19900 outlines the limit state verification requirements. The pertinent limit states are:

- a) ultimate limit states (ULS);
- b) abnormal/accidental limit states (ALS);