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**AMENDMENT 1**  
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**Gaseous hydrogen — Fuelling  
stations —**

**Part 8:  
Fuel quality control**

**AMENDMENT 1: Alignment with Grade D  
of ISO 14687**

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*Hydrogène gazeux — Stations de remplissage —*

*Partie 8: Contrôle qualité du carburant*

*ISO 19880-8:2019/Amd 1:2021*

*AMENDEMENT 1: Alignement avec le Grade D de l'ISO 14687*  
<https://standards.iteh.ai/en/standards/alignment-with-iso-14687-8204-07d1cc04a4a7/iso-19880-8-2019-amd-1-2021>



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# Gaseous hydrogen — Fuelling stations —

## Part 8: Fuel quality control

### AMENDMENT 1: Alignment with Grade D of ISO 14687

#### *Clause 5, first paragraph*

Replace the paragraph with the following:

The quality requirements of hydrogen fuel dispensed to PEM fuel cells for road vehicles are listed in Grade D of ISO 14687.

#### *8.4, first paragraph*

Replace the paragraph with the following:

It is necessary to evaluate the possible consequences on a fuel cell vehicle if any impurity exceeds the threshold value of ISO 14687 Grade D.

[ISO 19880-8:2019/Amd 1:2021](https://standards.iteh.ai/catalog/standards/sist/bb1db472-4309-4682-8204-07d1cc04a4a7/iso-19880-8-2019-amd-1-2021)

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#### *8.4, second paragraph*

[8204-07d1cc04a4a7/iso-19880-8-2019-amd-1-2021](https://standards.iteh.ai/catalog/standards/sist/bb1db472-4309-4682-8204-07d1cc04a4a7/iso-19880-8-2019-amd-1-2021)

Replace the paragraph with the following:

An estimation of the concentration above the ISO 14687 Grade D threshold values at which the severity increases (if applicable) is named “Level 1” and is given in column 5 for each impurity where the “severity class” is not already 4.

#### *Table 4*

Replace Table 4 with the following table:

Table 4 — Impact of impurities on fuel cell powertrain

| Impurity  |                        | ISO 14687 Grade D threshold value <sup>a</sup><br>[μmol/mol] | Severity class (from ISO 14687 Grade D threshold value to Level 1) | Level 1 value<br>[μmol/mol] | Severity class (greater than Level 1 threshold) |
|---|------------------------|--|--|-----------------------------|---|
| Total non-H <sub>2</sub> gases                                    |                        | 300  | UD <sup>b</sup>  | UD <sup>b</sup>             | 4   |
| Helium  | He                     | 300  | UD <sup>b</sup>  | UD <sup>b</sup>             | 4   |
| Nitrogen  | N <sub>2</sub>         | 300  | UD <sup>b</sup>  | UD <sup>b</sup>             | 4   |
| Argon   | Ar                     | 300  | UD <sup>b</sup>  | UD <sup>b</sup>             | 4   |
| Oxygen  | O <sub>2</sub>         | 5  | UD <sup>c</sup>  | UD <sup>c</sup>             | 4   |
| Carbon dioxide  | CO <sub>2</sub>        | 2  | 1  | 3                           | 4   |
| Carbon monoxide   | CO                     | 0,2  | 2-3 <sup>d</sup>   | 1                           | 4   |
| Methane   | CH <sub>4</sub>        | 100  | 1  | 300                         | 4   |
| Water   | H <sub>2</sub> O       | 5  | 4  | N/A                         | 4   |
| Total sulphur compounds   | H <sub>2</sub> S basis | 0,004  | 4  | N/A                         | 4   |
| Ammonia   | NH <sub>3</sub>        | 0,1  | 4  | N/A                         | 4   |
| Total hydrocarbons except methane                                 | CH <sub>4</sub> basis  | 2  | 1-4 <sup>d</sup>   | N/A                         | 4   |
| Formaldehyde  | HCHO                   | 0,2  | 2-3 <sup>d</sup>   | 1                           | 4   |
| Formic acid   | HCOOH                  | 0,2  | 2-3 <sup>d</sup>   | 1                           | 4   |
| Halogens  |                        | 0,05   | 4  | N/A                         | 4   |
| Maximum particulate concentration (liquid and solid) <sup>e</sup> |                        | 1 mg/kg  | 4  | N/A                         | 4   |

**Key**

UD: undetermined

N/A: not applicable

<sup>a</sup> The threshold value is according to hydrogen specification of Grade D of ISO 14687.

<sup>b</sup> The severity class (from ISO 14687 Grade D threshold value to Level 1) and Level 1 value for this impurity is undetermined because no specific study has been conducted yet in alignment with the new threshold value. It needs to be covered in the next edition of this document.

<sup>c</sup> The severity class (from ISO 14687 Grade D threshold value to Level 1) and Level 1 value for oxygen are undetermined because data are lacking to confirm those values. It needs to be covered in the next edition of this document.

<sup>d</sup> A higher value is to be considered for risk assessment approach until more specific data is available.

<sup>e</sup> Particulates are based upon mass density mg/kg.

*A.15 first paragraph*

Replace “ISO 14687-2” with “Grade D of ISO 14687” in the second last sentence.

*Table B.1*

Replace Table B.1 with the following table:

Table B.1 — Probability of occurrence for off-site SMR

| Impurity   | Threshold<br>μmol/mol | Possible causes<br>For the source studied   | Typical barriers employed in this process  | Probability<br>with<br>barriers |
|--|-----------------------|---|--|---------------------------------|
| <b>Inert gas<br/>N<sub>2</sub></b>   | 300                   | Present in natural gas and syngas<br>PSA malfunction  | — PSA<br>— Double analysis PSA outlet < 100 μmol/mol   | UD <sup>a</sup>                 |
| <b>Inert gas<br/>Ar</b>  | 300                   | Only ATR and POx present in O <sub>2</sub><br>typical 0,6 % in syngas from ATR  | — PSA. Not sized to remove Ar. Ar content may be higher if H <sub>2</sub> comes from ATR, POX or feeds with high Ar content  | UD <sup>a</sup>                 |
| <b>O<sub>2</sub></b>   | 5                     | Not present in syngas. O <sub>2</sub> is unstable in the condition of reforming and shift reactions. Combines with H <sub>2</sub> , CO, and CH <sub>4</sub> | — PSA cannot be used with significant O <sub>2</sub> content for safety reasons  | 0                               |
| <b>CO<sub>2</sub></b>  | 2                     | Present in syngas (%)   | — PSA adsorption strength of MS, activated carbon, silicagel higher for CO <sub>2</sub> than CO. A CO content lower than 10 μmol/mol insures a CO <sub>2</sub> content lower than 2 μmol/mol | 0                               |
| <b>CO</b>  | 0,2                   | Normal operation below threshold. Occasional peaks at μmol/mol level  | — Double analysis at the PSA outlet + trip if the CO > 1-10 μmol/mol at PSA outlet   | 4                               |
| <b>CH<sub>4</sub></b>  | 100                   | Present in syngas at % level  | — In most cases CO is sizing the PSA, therefore CO < 10 μmol/mol ==> CH <sub>4</sub> < 100 μmol/mol depending on users' specification (Europe pipeline 2 μmol/mol).                          | 2                               |
| <b>H<sub>2</sub>O</b>  | 5                     | Syngas saturated in H <sub>2</sub> O  | — PSA adsorbed in alumina and MS adsorption strength higher than CO <sub>2</sub> . A CO content lower than 10 μmol/mol insures a H <sub>2</sub> O content lower than 5 μmol/mol.             | 0                               |
| <b>Key</b>   |                       |   |  |                                 |
| UD: undetermined   |                       |   |  |                                 |
| <sup>a</sup> The probability of occurrence for this impurity is undetermined because no specific study has been conducted yet. |                       |   |  |                                 |

Table B.1 (continued)

| Impurity   | Threshold<br>µmol/mol | Possible causes<br>For the source studied    | Typical barriers employed in this process  | Probability<br>with<br>barriers |
|--|-----------------------|--|--|---------------------------------|
| <b>TS</b>  | 0,004                 | TS from natural gas                          | — Desulphuration upstream reformer (typical values: normal < 10 ppb, maximum < 20 ppb, guarantee < 50 ppb)   | 0                               |
|  |                       |  | — Typical dilution factor 2,5 (1 mole natural gas produces 2,5 mole H <sub>2</sub> )   |                                 |
|  |                       |  | — Pre-reformer catalyst poisoning by sulphur is irreversible. Sulphur trapped at this stage. In case of breakthrough, process condition cannot be achieved   |                                 |
|  |                       |  | — Reformer catalyst poisoning by sulphur is irreversible. Sulphur trapped at this stage. In case of breakthrough, process condition cannot be achieved   |                                 |
|  |                       |  | — Shift catalyst poisoning by sulphur is irreversible. Sulphur trapped at this stage. In case of breakthrough, process condition cannot be achieved  |                                 |
|  |                       |  | — PSA adsorption of H <sub>2</sub> S before CO, CO <sub>2</sub> , species  |                                 |
| <b>NH<sub>3</sub></b>  | 0,1                   | Traces present in syngas                     | — H <sub>2</sub> S adsorption in pipe and vessels. Strong affinity with steel  | 0                               |
|  |                       |  | — PSA adsorption strength of alumina and molecular sieve higher than CO. A CO content lower than 10 µmol/mol insures a NH <sub>3</sub> content lower than 0,1 µmol/mol   |                                 |
| <b>THC</b>   | 2                     | Traces of C2+ after reforming reaction       | — PSA C2 C3, C4-C5+ adsorbed by activated carbon layer. A CO content lower than 10 µmol/mol insures a THC (C <sub>2</sub> H <sub>4</sub> excluded) content lower than 2 µmol/mol   | 0                               |
| <b>HCHO</b>  | 0,2                   | May be present in syngas. essentially liquid | — PSA. Formaldehyde adsorption strength of alumina and molecular sieve higher than CO. A CO content lower than 10 µmol/mol insures a HCHO content lower than 0,1 µmol/mol. To guarantee 0,01 µmol/mol would require more experience of measuring at those levels | UD <sup>a</sup>                 |
| <b>HCOOH</b>   | 0,2                   | May be present in syngas essentially liquid  | — PSA. Formic adsorption strength of alumina and molecular sieve higher than CO. A CO content lower than 10 µmol/mol insures a HCOOH content lower than 0,2 µmol/mol   | 0                               |
| <b>Key</b>   |                       |  |  |                                 |
| UD: undetermined   |                       |  |  |                                 |
| <sup>a</sup> The probability of occurrence for this impurity is undetermined because no specific study has been conducted yet. |                       |  |  |                                 |



Table B.1 (continued)

| Impurity   | Threshold<br>μmol/mol | Possible causes<br>For the source studied  | Typical barriers employed in this process  | Probability<br>with<br>barriers |
|--|-----------------------|--|--|---------------------------------|
| <b>Halogens</b>  | 0,05                  | Present in natural gas   | <ul style="list-style-type: none"> <li>— Any Cl present in natural gas would be stopped by HDS</li> <li>— Pre-reformer catalyst poisoning by Cl irreversible. Cl trapped at this stage. If breakthrough, process condition cannot be achieved</li> <li>— Reformer catalyst poisoning by Cl irreversible. Cl trapped at this stage. I breakthrough, process condition cannot be achieved</li> <li>— Shift catalyst poisoning by Cl irreversible. Cl trapped at this stage. I breakthrough, process condition cannot be achieved</li> <li>— PSA adsorption of Cl before CO, CO<sub>2</sub>, species</li> </ul> | 0                               |
| <b>He</b>  | 300                   | Not present in natural gas in N Europe (<10 μmol/mol). Passes through the whole process. Dilution factor 2,5 |  | 0                               |
| <b>Key</b><br>UD: undetermined<br><sup>a</sup> The probability of occurrence for this impurity is undetermined because no specific study has been conducted yet. |                       |  |  |                                 |

Table B.2

Replace Table B.2 with the following table:

**Table B.2 — Probability of occurrence for pipeline**

| Impurity                           | Threshold<br>μmol/mol | Causes possible<br>For the item studied  | Typical barriers<br>employed in<br>this process   | Probability<br>with<br>barriers |
|------------------------------------|-----------------------|--|---|---------------------------------|
| <b>Inert gas</b><br>N <sub>2</sub> | 300                   | Air intake if some areas are at negative pressure<br>From seal gas or purge gas<br>Wrong purging after maintenance | Inlet pressure PSL trip on compressors  | UD <sup>a</sup>                 |
| <b>Inert gas</b><br>Ar             | 300                   | No potential   | 1 % Ar in the air.<br>100 μmol/mol would mean 1 % air in the pipe<br>Never been observed            | UD <sup>a</sup>                 |
| <b>O<sub>2</sub></b>               | 5                     | Air intake if some areas are at negative pressure  | Inlet pressure PSL trip on compressors  | 1                               |
| <b>CO<sub>2</sub></b>              | 2                     | From Air: CO <sub>2</sub> at 400 μmol/mol in the air   | 2 μmol/mol of CO <sub>2</sub> would mean 0,5 % air in the pipe<br>Never been observed               | 0                               |
| <b>CO</b>                          | 0,2                   | No potential   |   | 0                               |
| <b>CH<sub>4</sub></b>              | 100                   | No potential   |   | 0                               |
| <b>H<sub>2</sub>O</b>              | 5                     | Wrong drying after pressure hydraulic test   | H <sub>2</sub> > 40 bar ==> leak from H <sub>2</sub> O to H <sub>2</sub> unlikely during operation. | 0                               |
| <b>TS</b>                          | 0,004                 | No potential   |   | 0                               |
| <b>NH<sub>3</sub></b>              | 0,1                   | No potential   |   | 0                               |
| <b>THC</b>                         | 2                     | No potential   |   | 0                               |
| <b>HCHO</b>                        | 0,2                   | No potential   |   | UD <sup>a</sup>                 |
| <b>HCOOH</b>                       | 0,2                   | No potential   |   | 0                               |
| <b>Halogens</b>                    | 0,05                  | From cleaning material after maintenance   |   | 1                               |
| <b>He</b>                          | 300                   | No potential   |   | 0                               |

**Key**

UD: undetermined

<sup>a</sup> The probability of occurrence for this impurity is undetermined because no specific study has been conducted yet. It needs to be covered in the next edition of this document.

Table B.3

Replace Table B.3 with the following table:

**Table B.3 — Probability of occurrence for fuelling station to be source of impurities**

| Impurity  | Threshold<br>μmol/mol | Causes possible<br>For the source studied   | Existing barriers  | Probability     |
|---|-----------------------|---|--|-----------------|
| <b>Inert gas</b><br><b>N<sub>2</sub></b>  | 300                   | N <sub>2</sub> purging operation, air intake during normal operation or maintenance   |  | UD <sup>a</sup> |
| <b>Inert gas</b><br><b>Ar</b>   | 300                   | Air intake during normal operation or maintenance   | 1 % Ar in the air.<br>100 μmol/mol would mean 1 % air in the fuelling station<br>Never been observed | UD <sup>a</sup> |
| <b>O<sub>2</sub></b>  | 5                     | Air intake during normal operation or maintenance   |  | 2               |
| <b>CO<sub>2</sub></b>   | 2                     | Air intake during normal operation or maintenance   | 2 μmol/mol CO <sub>2</sub> would mean 0,5 % air in the fuelling station. Never been observed         | 0               |
| <b>CO</b>   | 0,2                   | No potential at fuelling station level  |  | 0               |
| <b>CH<sub>4</sub></b>   | 100                   | No potential at fuelling station level  |  | 0               |
| <b>H<sub>2</sub>O</b>   | 5                     | Maintenance, leaks from compressor exchangers, improper pressure vessel drying after periodic inspection, H <sub>2</sub> O coming from the vent in case of check valve malfunction, depending on fuelling station/compressor technology |  | 2               |
| <b>TS</b>   | 0,004                 | Materials gaskets, valve seats and tubing   | Material specifications  | 1               |
| <b>NH<sub>3</sub></b>   | 0,1                   | No potential  |  | 0               |
| <b>THC</b>  | 2                     | Oil carryover from compressor (depending on compressor technology)  |  | 2               |
| <b>HCHO</b>   | 0,2                   | No potential  |  | UD <sup>a</sup> |
| <b>HCOOH</b>  | 0,2                   | No potential  |  | 0               |
| <b>Halogens</b>   | 0,05                  | From degreasing material  |  | 1               |
| <b>He</b>   | 300                   | No potential at fuelling station level  | If pure He is not used for maintenance   | 0               |
| <b>Key</b>  |                       |   |  |                 |
| UD: undetermined  |                       |   |  |                 |
| <sup>a</sup> The probability of occurrence for this impurity is undetermined because no specific study has been conducted yet. It will be covered in the next edition of this document. |                       |   |  |                 |

Table B.4

Replace Table B.4 with the following table: