



Designation: **C1417M—11** **C1417M – 12**

Standard Specification for Manufacture of Reinforced Concrete Sewer, Storm Drain, and Culvert Pipe for Direct Design (Metric)¹

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1. Scope

1.1 This specification covers the manufacture and acceptance of precast concrete pipe designed to conform to the owner's design requirements and to the ASCE 15 or an equivalent design specification.

NOTE 1—The section on evaluation of core test results (14.3.3) and the Appendix are currently being rebalotted.

1.2 This specification is the SI companion to Specification C1417.

2. Referenced Documents

2.1 ASTM Standards:²

[A615/A615M](#) Specification for Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement

[A706/A706M](#) Specification for Low-Alloy Steel Deformed and Plain Bars for Concrete Reinforcement

[A1064/A1064M](#) Specification for Steel Wire and Welded Wire Reinforcement, Plain and Deformed, for Concrete

[C33](#) Specification for Concrete Aggregates

[C76](#) Specification for Reinforced Concrete Culvert, Storm Drain, and Sewer Pipe

[C150](#) Specification for Portland Cement

[C260](#) Specification for Air-Entraining Admixtures for Concrete

[C494/C494M](#) Specification for Chemical Admixtures for Concrete

[C497](#) Test Methods for Concrete Pipe, Manhole Sections, or Tile

[C595](#) Specification for Blended Hydraulic Cements

[C618](#) Specification for Coal Fly Ash and Raw or Calcined Natural Pozzolan for Use in Concrete

[C655](#) Specification for Reinforced Concrete D-Load Culvert, Storm Drain, and Sewer Pipe

[C822](#) Terminology Relating to Concrete Pipe and Related Products

[C989](#) Specification for Slag Cement for Use in Concrete and Mortars

[C1017/C1017M](#) Specification for Chemical Admixtures for Use in Producing Flowing Concrete

2.2 Other Standards:

[ASCE 15](#) Standard Practice for the Direct Design of Buried Precast Reinforced Concrete Pipe Using Standard Installations (SIDD)³

[ACI 318](#) Building Code Requirements for Reinforced Concrete⁴

3. Terminology

3.1 Definitions:

3.1.1 For definitions of terms relating to concrete pipe, see Terminology [C822](#).

3.1.2 *group of pipe sections*—each day's production run of pipe sections of a single concrete strength for a specific project.

3.1.3 *lot of pipe sections*—total of the number of groups of pipe sections of a single concrete strength produced for a specific project.

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² For referenced ASTM standards, visit the ASTM website, [www.astm.org](#), or contact ASTM Customer Service at [service@astm.org](#). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Available from American Society of Civil Engineers (ASCE), 1801 Alexander Bell Dr., Reston, VA 20191, [http://www.asce.org](#).

⁴ Available from American Concrete Institute (ACI), P.O. Box 9094, Farmington Hills, MI 48333-9094, [http://www.aci-int.org](#).

3.1.4 *running average*—average concrete compressive strength of all groups of pipe sections of a single concrete strength produced for a specific project, generally determined as each group is tested.

4. Basis of Acceptance of Design

4.1 *Manufacturing Design Data*—The manufacturer shall submit the following manufacturing design data for the concrete pipe to the owner for approval.

4.1.1 Pipe wall thickness.

4.1.2 Concrete strength.

4.1.3 *Reinforcement*:

4.1.3.1 Specification,

4.1.3.2 Reinforcement Type 1, 2, or 3, where:

Type 1:	Smooth wire or plain bars
Type 2:	Welded smooth wire reinforcement, 200 mm maximum spacing of longitudinals
Type 3:	Welded deformed wire reinforcement, deformed wire, deformed bars, or any reinforcement with stirrups, anchored thereto

4.1.3.3 Design yield strength,

4.1.3.4 Placement and design concrete cover,

4.1.3.5 Cross-sectional diameters,

4.1.3.6 Spacing,

4.1.3.7 Cross-sectional area,

4.1.3.8 Description of longitudinal members, and

4.1.3.9 If stirrups are used, developable stirrup design stress, stirrup shape, placement, and anchorage details.

4.1.4 Design factors and the assumed orientation angle.

4.1.5 Pipe laying length and joint information.

4.2 Approval of the manufacturing design data shall be based on its conformance to the owner's design requirements and to ASCE 15 or to an equivalent design specification.

5. Basis of Acceptance of Concrete Pipe

5.1 Acceptance of pipe shall be on the basis of concrete compression tests, materials tests, conformance to the manufacturing design data, conformance to this specification, and inspection of manufactured pipe for defects.

5.2 When mutually agreed in writing by the owner and the manufacturer, a certification may be made the basis of acceptance of the concrete pipe. This certification shall consist of a statement by the manufacturer that the concrete pipe conforms to the manufacturing design data and to this specification, and that the concrete and materials have been sampled and tested and conform to this specification.

5.3 *Age for Acceptance*—Pipe shall be considered ready for acceptance when they conform to the requirements of this specification.

6. Material

6.1 *Reinforced Concrete*—The reinforced concrete shall consist of cementitious materials; mineral aggregates; admixtures, if used; and water in which steel has been embedded in such a manner that the steel and concrete act together.

6.2 *Cementitious Material*:

6.2.1 *Cement*—Cement shall conform to the requirements for portland cement of Specification C150 or shall be portland blast-furnace slag cement or portland-pozzolan cement conforming to the requirements of Specification C595, except that the pozzolan constituent in the Type IP portland-pozzolan cement shall be fly ash.

6.2.2 *Slag Cement*—Slag cement shall conform to the requirements of Grade 100 or 120 of Specification C989.

6.2.3 *Fly Ash*—Fly ash shall conform to the requirements of Specification C618, Class F or Class C.

6.2.4 *Allowable Combinations of Cementitious Materials*—The combination of cementitious materials used in the concrete shall be one of the following:

6.2.4.1 Portland cement only.

6.2.4.2 Portland blast-furnace slag cement only.

6.2.4.3 Portland-pozzolan cement only.

6.2.4.4 A combination of portland cement and slag cement.

6.2.4.5 A combination of portland cement and fly ash, or

6.2.4.6 A combination of portland cement, slag cement (not to exceed 25 % of the total cementitious weight), and fly ash (not to exceed 25 % of the total cementitious weight).

6.3 *Aggregates*—Aggregates shall conform to the requirements of Specification **C33**, except that the requirement for gradation shall not apply.

6.4 *Admixtures*—The following admixtures and blends are allowable:

6.4.1 Air-entraining admixture conforming to Specification **C260**;

6.4.2 Chemical admixture conforming to Specification **C494/C494M**;

6.4.3 Chemical admixture for use in producing flowing concrete conforming to Specification **C1017/C1017M**; and

6.4.4 Chemical admixture or blend approved by the owner.

6.5 *Steel Reinforcement*—Reinforcement shall consist of wire and welded wire conforming to Specification **A1064/A1064M**; or of bars conforming to Specifications **A615/A615M**, Grade 40 or 60, or **A706/A706M**, Grade 60.

7. Joints

7.1 The joints shall be designed and the ends of the concrete pipe sections shall be formed so that the sections can be laid together to make a continuous line of pipe, compatible with the permissible variations given in Section **15**.

8. Manufacture

8.1 *Concrete*—The aggregates shall be sized, graded, proportioned, and mixed with cementitious material and water and admixtures, if any, to produce a ~~homogeneous~~ thoroughly mixed concrete mixture of such quality that the pipe will conform to the design requirements of this specification. The water-cementitious material ratio of all concrete shall be 0.53, or less, by weight. Minimum concrete strength shall be 27.6 MPa.

8.2 *Finish*—Pipe shall be substantially free of fractures, large or deep cracks, and surface roughness. The ends of the pipe shall be normal to walls and center line of the pipe, within the limits of variations given in Section **15**.

9. Circumferential Reinforcement

9.1 A line of circumferential reinforcement for any given total area may be composed of up to two layers for pipe with wall thicknesses of less than 180 mm or three layers for pipe with wall thickness of 180 mm or greater. The layers shall not be separated by more than the thickness of one longitudinal plus 6 mm. The multiple layers shall be fastened together to form a single cage. If the multiple layers of a cage contain circumferential splices, the individual layers shall be rotated so that the splices are staggered. All other specification requirements, such as laps, welds, tolerances of placement in the wall of the pipe, and so forth, shall apply to this method of fabricating a line of reinforcement. The design shall be based on the centroid of the layers.

9.2 Reinforcement placement and concrete cover shall conform to the approved manufacturing data. The nominal concrete cover over the circumferential reinforcement shall not be less than be 25 mm in pipe having a wall thickness of 63 mm or greater, and shall not be less than 19 mm in pipe having a wall thickness of less than 63 mm. The location of the reinforcement shall be subject to the permissible variations in dimensions given in Section **15**. Requirements for placement and protective covering of the concrete from the inner or outer surface of the pipe do not apply to that portion of a cage that is flared so as to extend into the bell or reduced in diameter so as to extend into the spigot.

9.3 Where the wall reinforcement does not extend into the joint area, the maximum longitudinal distance to the last circumferential from the inside shoulder of the bell or the shoulder of the spigot shall be 75 mm, except that if this distance exceeds one half of the wall thickness, the pipe wall shall contain at least a total reinforcement area of the minimum specified area per linear metre times the laying length of the pipe section. The minimum cover on the last circumferential near the spigot shoulder shall be 13 mm.

9.4 Where reinforcement is in the bell or spigot, the minimum end-cover on the last circumferential shall be 13 mm in the bell or 6 mm in the spigot.

9.5 The continuity of the circumferential reinforcing steel shall be maintained during the manufacture of the pipe, except when, as agreed upon by the owner, lift eyes or holes are provided in each pipe or the pipe is converted into a manhole tee.

10. Welds, Splices, and Development of Circumferential Reinforcement

10.1 *General:*

10.1.1 When pipe are not marked to show a specific orientation in the ground, any weld to, or splice of, a circumferential shall be considered to be at the point of the maximum flexural stress.

10.1.2 When pipe are marked to show a specific orientation in the ground, any weld to, or splice of, a circumferential shall be considered to be at a distance determined by the orientation angle closer to the point of maximum flexural stress than the marking indicates.

10.1.3 Splices of smooth and deformed wire shall be welded and shall meet the requirements of **10.3** and **10.4**.

10.2 *Notation:*

A_{wa} = actual steel area of the individual circumferential wire, mm².

- A_{wr} = steel area required for the individual circumferential wire for flexure, mm², either at the splice, for splices, or at the point of maximum moment, for quadrant mat reinforcement.
 d_b = diameter of reinforcing wire or bar, mm.
 f_c^t = design compressive strength of concrete, MPa.
 f_y = design yield strength of reinforcement, MPa.
 F_w = embedded weld factor (see 10.4.3).
 L_d = development length of reinforcing wire or bar, mm.
 P_t = pull test strength of wire or bar at break, N.
 s = spacing of wire to be developed or spliced, mm.

10.3 Welds:

10.3.1 For butt splices of circumferentials or where welds are made to circumferentials, pull tests of representative specimens of the circumferential across the finished weld shall demonstrate a strength of no less than 1.1 times the design yield strength of the circumferential except as provided in 10.4.

10.3.2 At the option of the manufacturer, a more detailed analysis may be made and the requirements of this section used instead of 10.3.1. For butt splices of circumferentials or where welds are made to circumferentials, pull tests, P_t , of representative specimens of the circumferential across the finished weld shall demonstrate a strength of no less than:

$$P_t = 1.1 A_{wr} f_y \quad (1)$$

or no less than:

$$P_t = 0.5 A_{wa} f_y \quad (2)$$

whichever is greater.

10.4 Lapped Splices of Circumferential Reinforcement:

10.4.1 Where lapped circumferentials are spliced by welding, they shall be lapped no less than 50 mm. Pull tests of representative specimens shall develop no less than 0.9 times design yield strength of the circumferential.

10.4.2 At the option of the manufacturer, a more detailed analysis may be made and the requirements of 10.4.2 and 10.4.3 used instead of 10.4.1. Where lapped circumferentials are spliced by welding, they shall be lapped no less than 50 mm. Pull tests, P_t , of representative specimens shall develop no less than:

$$P_t = F_w A_{wr} f_y \quad (3)$$

or not less than the strength required by Eq 2, whichever is the greater.

10.4.3 The embedded weld factor, F_w , relates the pull test strength of the non-embedded splice specimens to the strength of the splice embedded in the concrete of the pipe wall.

10.4.3.1 If the pull test break is in the wire, F_w shall be taken as 0.90.

10.4.3.2 If the pull test break is in the weld, F_w shall be taken as 0.70.

10.4.4 If lapped splices of circumferentials consisting of deformed bars #19 or less are not welded, they shall be lapped not less than L_d , where:

$$L_d = \frac{d_b f_y A_{wr}}{2.74 \sqrt{f_c^t} A_{wa}} \quad (4)$$

or not less than:

$$d_b = \frac{f_y}{5.48 \sqrt{f_c^t}} \quad (5)$$

whichever is greater. Splices of larger than #19 bars shall meet the requirements of ACI 318.

10.4.5 If lapped splices of circumferentials consisting of welded smooth wire reinforcement or welded deformed wire reinforcement are not welded, the overlap measured between the outermost longitudinals on each side of the splice shall be no less than the spacing of the longitudinals plus 25 mm, or L_d , where:

$$L_d = 3.25 \frac{A_{wr} f_y}{s \sqrt{f_c^t}} \quad (6)$$

whichever is greater.

10.4.6 At the option of the manufacturer, a more detailed analysis may be made and the following exception to the requirements of 10.4.5 may be applied. If the area of circumferential reinforcement is at least twice that required for flexure, the first requirement of 10.4.5 shall not apply. The overlap measured between the outermost longitudinals on each side of the splice shall be no less than that required by Eq 6, or 25 mm, whichever is greater.

10.4.7 Alternative splice designs that differ from 10.4 may be submitted to the owner for approval.

10.5 Development of Quadrant Mat Reinforcement:

10.5.1 Circumferential quadrant mat reinforcement shall consist of welded wire reinforcement with 200-mm maximum cross wire spacing. When quadrant mat reinforcement is used, the area of the main cage shall be no less than 25 % of the area required at the point of maximum moment. The quadrant mats shall extend at least 45° each side of the point of maximum moment.

10.5.2 At the option of the manufacturer, a more detailed analysis may be made and the requirements of 10.5.3 or 10.5.4 used instead of 10.5.1.

10.5.3 When circumferential quadrant mat reinforcement consists of welded smooth wire reinforcement or welded deformed wire reinforcement, the following requirements shall apply:

10.5.3.1 The outermost longitudinals on each end of the circumferentials shall be embedded in accordance with the following requirements: (1) past the point where the quadrant reinforcement is no longer required by the orientation angle plus the greater of twelve circumferential wire diameters or three quarters of the wall thickness of the pipe, and (2) past the point of maximum flexural stress by the orientation angle plus the development length, L_d , required by Eq 6.

10.5.3.2 The mat shall contain no less than two longitudinals at a distance 25 mm greater than that determined by the orientation angle from either side of the point requiring the maximum flexural reinforcement.

10.5.3.3 The point of embedment of the outermost longitudinals of the mat shall be at least a distance determined by the orientation angle past the point where the continuing reinforcement is no less than double the area required for flexure.

10.5.4 When circumferential quadrant mat reinforcement consists of #19 or less deformed bars, the following requirements shall apply:

10.5.4.1 Circumferentials shall extend past the point where they are no longer required by the orientation angle plus the greater of twelve wire diameters or three quarters of the wall thickness of the pipe.

10.5.4.2 Circumferentials shall extend either side of the point of maximum flexural stress not less than the orientation angle plus the development length, L_d , required by Eq 4.

10.5.4.3 Circumferentials shall extend at least a distance determined by the orientation angle past the point where the continuing reinforcement is no less than double the area required for flexure.

10.5.4.4 Development of larger than #19 bars shall meet the requirements of ACI 318.

11. Stirrup Reinforcement

11.1 The number of lines of stirrups shall be sufficient to include the distance determined by calculation where V_u is less than V_c plus the distance l_0 as determined in Section 12.6.4.1 of ASCE 15 or as determined by the requirements of an equivalent design specification. The required number of lines of stirrups shall be equally distributed on each side of the point of maximum moment.

11.2 Stirrups used to resist radial tension shall be anchored around each circumferential of the inside cage.

11.3 When stirrups are not required for radial tension but required for shear, their longitudinal spacing shall be such that they are anchored either at every or every other inside face tension circumferential. Such spacing shall not exceed 150 mm.

11.4 Stirrups intended to resist forces in the invert and crown regions shall be anchored around the inside circumferentials and anchored sufficiently in the concrete compression zone on the opposite side of the pipe wall to develop the design strength of the stirrup.

11.5 Anchorage of both ends of the stirrup shall be sufficient to develop the factored stress in the stirrup. The maximum factored tensile stress in the stirrup shall be the yield stress or the stress that can be developed by anchorage, whichever is less.

12. Longitudinal Reinforcement

12.1 Circumferential reinforcement shall be assembled into a cage containing sufficient longitudinal members to maintain the circumferential reinforcement in correct position within the pipe.

13. Joint Reinforcement

13.1 *General*—The length of the joint as used in this specification means the inside length of the bell or the outside length of the spigot from the shoulder to the end of the pipe section. The end distances or cover on the end circumferential shall apply to any point on the circumference of the pipe or joint. When convoluted reinforcement is used, these distances and reinforcement areas shall be taken from the points on the convolutions closest to the end of the pipe section. The following requirements for joint reinforcement shall apply.

13.2 *Non-Rubber Gasket Joints:*

13.2.1 For pipe less than 900 mm in diameter, neither the bell or spigot require circumferential reinforcement.

13.2.2 For pipe 900 mm and larger in diameter, either the bell or spigot shall contain circumferential reinforcement. This reinforcement shall be an extension of a wall cage or may be a separate cage of at least the area per linear metre of that specified for the outer cage or one half of that specified for single cage wall reinforcement, whichever is less.

13.2.3 Where bells or spigots require reinforcement, the maximum end cover on the last circumferential shall be one-half the length of the joint or 75 mm, whichever is less.

13.3 *Rubber Gasket Joints:*

13.3.1 For pipe 300 mm and larger in diameter, the bell ends shall contain circumferential reinforcement. This reinforcement shall be an extension of the outer cage or a single wall cage, whichever is less, or it may be a separate cage of at least the same area per linear metre with longitudinals as required in Section 12. If a separate cage is used, the cage shall extend into the pipe with the last circumferential wire at least 25 mm past the inside shoulder where the pipe barrel meets the bell of the joint.

13.3.2 When bells require reinforcement, the maximum end cover on the last circumferential shall be 38 mm.

14. Physical Requirements

14.1 *Concrete Compressive Strength Testing, Type of Specimen*—Compression tests for determining concrete compressive strength may be made on either concrete cylinders or on cores drilled from the pipe.

14.2 *Acceptance by Cylinder Tests:*

14.2.1 Cylinders shall be prepared in accordance with Section 11 of Test Methods C497.

14.2.2 *Number of Cylinders*—Prepare not less than five test cylinders from a group (one day's production) of pipe sections.

14.2.3 *Evaluation of Test Results:*

14.2.3.1 When the compressive strengths of all cylinders tested for a group are equal to or greater than the design concrete strength, the compressive strength of concrete in the group of pipe sections shall be acceptable.

14.2.3.2 When the running average compressive strength of all cylinders tested in a lot is equal to or greater than the design concrete strength, not more than 10 % of the cylinders tested have a compressive strength less than the design concrete strength, and no cylinder tested has a compressive strength less than 80 % of the design concrete strength, then the compressive strength of the concrete in the lot of pipe sections shall be acceptable.

14.2.3.3 If the concrete strength for a group does not meet the required concrete strength because of faulty cylinders or faulty production, the manufacturer may cull that group from the lot and running average. A group culled because of faulty cylinders may be accepted in accordance with the provisions of 14.2.3.4.

14.2.3.4 When the concrete compressive strength of the cylinders tested for a group or for a lot does not conform to the acceptance criteria in 14.2.3.1 or 14.2.3.2, the acceptability of the group or lot shall be determined by additional tests on cores in accordance with the provisions of 14.3.

14.3 *Acceptance by Core Tests:*

14.3.1 *Obtaining Cores*—Core specimens shall be obtained, prepared, and tested in accordance with Test Method C497.

14.3.2 *Number of Cores*—Three cores shall be taken from three sections (one core from each) selected at random from each group of pipe sections or fraction thereof of a single size from each continuous production run.

14.3.3 *Evaluation of Test Results:*

14.3.3.1 Concrete represented by these three core tests shall be considered acceptable if the average of the three core strengths is equal to or greater than 85 % of the required strength and no single core is less than 75 % of the required strength.

14.3.3.2 If the compressive strength of the three cores does not meet the requirements of 14.3.3.1, the sections from the cores were taken shall be rejected. Two pipe sections from the remainder of the group shall be selected at random and one core shall be taken from each and tested. If both cores have a strength equal to or greater than 85 % of the required strength, the remainder of the group is acceptable. If the compressive strength of either of the two cores is less than 85 % the required strength, the remainder of the group shall be rejected or, at the option of the manufacturer, each pipe section of the remaining group shall be cored and accepted individually, and any of these pipe sections that have core strengths less than 85 % of the required strength shall be rejected.

14.3.3.3 If the compressive strength of the re-core is less than the design concrete strength, the pipe section from which the core was taken shall be rejected. Two pipe sections from the remainder of the group shall be selected at random, and one core shall be taken from each pipe section. When the compressive strength of both cores is equal to or greater than the design concrete compressive strength, the concrete compressive strength of the remainder to the group shall be acceptable. If the compressive strength of either of the two cores tested is less than the design concrete compressive strength, then the remainder of the group shall be either rejected or, at the option of the manufacturer, each pipe section of the remainder of the group shall be cored and accepted individually, and any of the pipe sections that have a core with less than the design concrete compressive strength shall be rejected.

14.3.4 *Plugging Core Holes*—Core holes shall be plugged and sealed by the manufacturer in a manner such that the pipe section will meet all the requirements of the specification. Pipe sections so plugged and sealed shall be considered satisfactory for use.

15. Permissible Variations

15.1 *Pipe Diameter*—The internal diameter permissible variations utilizing SI units are as prescribed in Table 1.

15.2 *Reinforcement Area*—Reinforcement will be considered as meeting the design requirements if the area, computed on the basis of nominal area of the wire or bars used, equals or exceeds the design requirements. Actual area of the reinforcement used may vary from the nominal area in accordance with permissible variations of the standard specifications for the reinforcement.

15.3 *Reinforcement Placement*—The maximum variation in the nominal location of the reinforcement shall be $\pm 10\%$ of the wall thickness. In no case, however, shall the cover over the circumferential reinforcement be less than 16 mm.