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Displacement and dynamic compressors—Performance test code for electric driven low-pressure air compressor packages

Compresseurs volumétriques et turbocompresseurs — Code d'essai de performance des ensembles de compresseurs basse pression à entraînement électrique

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Introduction

This document was developed in response to a recognized need to provide a methodology to correct performance of a low-pressure air compressor to guarantee conditions for positive displacement and dynamic compression types.

In dynamic compression, air is drawn between the blades on a rapid rotating compression impeller and accelerates to high velocity. The gas is then discharged through a diffuser, where the kinetic energy is transformed into static pressure. Dynamic low-pressure compressors are of a radial flow design, with the following typical examples:

- —single-stage centrifugal (aka high speed "turbo") compressors;
- multi-stage centrifugal compressors without intercooling.

Positive displacement low-pressure compressors work on the principle of trapping a volume of air and reducing its volume, internally or externally. Two basic types are typical, as follows:

- —Rotary screw positive displacement compressor where air is drawn into a compression chamber
 formed by intermeshing rotors¹. As the rotors turn, the cavity between the rotors becomes smaller,
 reducing the volume of the trapped air and increasing its pressure;
- Rotary lobe positive displacement compressor where air is drawn into the case and is trapped between the rotor and the case wall. These air pockets are progressively moved to the discharge port. At the discharge port, a back flow of air into the pocket from the higher-pressure discharge line produces a constant volume pressure rise.

Existing standards (e.g. <u>ISO 1217</u>, <u>ISO 5389</u>, <u>ISO 18740</u>) for positive displacement compressors and dynamics compressors, do not provide clear and concise means of comparing different technologies.

This document provides simplified wire to air performance test methods that measure true performance of low-pressure air compressor packages.

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¹- In this document the terms "rotor" and "impeller" are used to describe the rotating element(s) which cause(s) compression, and can be considered to be interchangeable.

¹⁾ In this document the terms "rotor" and "impeller" are used to describe the rotating element(s) which cause(s) compression, and can be considered to be interchangeable.

Displacement and dynamic compressors—Performance test code for electric driven low-pressure air compressor packages

1 Scope

This document specifies the performance test method of electrically driven low-pressure air compressor packages, where the compression is performed by positive displacement or dynamic compression; utilising atmospheric air as the compression gas. Low-pressure air compressor packages are often referred to as "blowers".

NOTE Throughout this document, the term 'low-pressure compressor' is used to describe a low-pressure algreement compressor ("blower") package

Low-pressure compressors with and without means of controlling flow (control may be electrical (e.g. with privariable frequency drive) or mechanical or both) are covered.

This document applies to low-pressure compressors meeting all the following limits:

- Atmospheric inlet air pressure between 0,5 bar and 1,1 bar.
- Discharge vs inlet pressure differential between 0,1 bar and 2,5 bar.
- Discharge vs inlet pressure ratio between 1,1 and 3,5.

This document is not applicable to:

- —positive displacement low-pressure compressors with a liquid in the compression element (such a liquid ring pumps and liquid injected low-pressure compressor of screw type)
- multi-stage low-pressure compressors other than multistage centrifugal compressors comprised df multiple, identical or very similar uncooled sections along a single shaft (repeating stages).
- —single shaft, multistage centrifugal compressors are treated from the point of measurement and calculation as a single stage

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

<std>ISO 5167-ISO 5167-I, Measurement of fluid flow by means of pressure differential devices inserted in circular cross-section conduits running full — Part 1: General principles and requirements</sd>

<std>ISO 9300, Measurement of gas flow by means of critical flow nozzles</std>

<std>ISO 17089-ISO 9300, Measurement of gas flow by means of critical flow nozzles

ISO 17089_1, Measurement of fluid flow in closed conduits — Ultrasonic meters for gas — Part 1: Meters for custody transfer and allocation measurement </br>

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3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- -ISO Online browsing platform: available at <u>https://www.iso.org/obp</u>https://www.iso.org/obp
- IEC Electropedia: available at https://www.electropedia.org/

3.1

acceptance test

performance test carried out in accordance with this document

Note 1-to-entry: See Annex C for an example of acceptance test report.

3.2

displacement compressor

packaged compressor where a static pressure rise is obtained by allowing successive volumes of gas to be aspired into and exhausted out of a closed space by means of the displacement of a moving member

[SOURCE: ISO 5390:1977, 3.1]

3.3

dynamic compressor

packaged compressor in which the fluid pressure increase is obtained by transformation of kinetic energy into potential energy with continuous flow from intake point to discharge point

[SOURCE: ISO 5390:1977, 3.2]

3.4

external coolant

medium externally supplied to the compressor to which the generated heat is finally rejected

Note 1-to-entry:-This is usually ambient air or cooling water $\frac{dards}{180}/29501e9d-6704-4033-b819$

[SOURCE: ISO 1217:2009, 3.1.7]

3.5

packaged compressor

compressor with prime mover, transmission, fully piped and wired internally, including ancillary and auxiliary items of equipment where these are within the scope of supply

[SOURCE: ISO 1217;2009, 3.1.13]

3.6

isentropic compression

idealized (i.e. reversible) adiabatic thermodynamic compression process that occurs without transfer of heat into or out of a system

3.7

2

rotational speed

number of revolutions of the compressor drive shaft per unit of time

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ISO/FDIS-22484:2024(en) Formatted: Font: 11 pt, Bold Formatted: Font: 11 pt, Bold Formatted: HeaderCentered, Left, Space After: 0 pt, [SOURCE: ISO 1217:2009, 3.1.18] Line spacing: single Formatted: Default Paragraph Font process air inlet point Formatted: Default Paragraph Font point upstream of any technically required component Formatted: Default Paragraph Font Note 1-to-entry:-In the case in which a technically required component is not physically present during the test the Formatted: Default Paragraph Font impact of the component on performance shall be accounted for Formatted: Adjust space between Latin and Asian text, Adjust space between Asjan text and numbers, Tab stops: Not at 0.7 cm + 1.4 cm + 2.1 cm + 2.8 cm + process air discharge point 3.5 cm + 4.2 cm + 4.9 cm + 5.6 cm + 6.3 cm + 7 cmpoint downstream of any technically required component Formatted: Adjust space between Latin and Asian text, Adjust space between Asian text and numbers Note 1-to-entry:-In the case in which a technically required component is not physically present during the test the impact of the component on performance shall be accounted for **Formatted** 3.10 Formatted guarantee conditions site conditions for which the equipment is expected to perform. Typically, this will include atmospheric pressure and ambient temperature 3.11 Commented [eXtyles3]: The term "absolute pressure" is absolute pressure Formatted pressure with reference to absolute zero, i.e. with reference to an absolute vacuum-Formatted: Default Paragraph Font Note 1 to entry: It equals the algebraic sum of atmospheric pressure and gauge pressure (static pressure or tot Formatted: Default Paragraph Font Formatted: Default Paragraph Font Formatted: Default Paragraph Font [SOURCE: ISO 3857-1:1977, 1.3], modified — The second sentence was moved as a note Formatted: Default Paragraph Font 3.12 Formatted: Default Paragraph Font ambient pressure Formatted: Default Paragraph Font absolute pressure (3.11) (3.11) of the atmospheric air measured in the vicinity of the compressor Formatted: Default Paragraph Font [SOURCE: ISO 1217:2009, 3.2.2] Formatted: Default Paragraph Font 3.13 Formatted: Default Paragraph Font atmospheric pressure Formatted: Default Paragraph Font absolute pressure (3.11)(3.11) of the atmospheric air measured at the test place Formatted: Default Paragraph Font [SOURCE: ISO 1217;2009, 3.2.3] Formatted: Default Paragraph Font Formatted: Default Paragraph Font discharge pressure Formatted: Default Paragraph Font total mean absolute pressure (3.11)(3.11) at the process air discharge point (3.9)(3.9)Formatted: Default Paragraph Font Formatted: Default Paragraph Font inlet pressure Formatted: Font: 10 pt total mean absolute pressure (3.11)(3.11) at the standard process air inlet point (3.8)(3.8)Formatted: Font: 10 pt 3.16 Formatted: Font: 10 pt total pressure Formatted: FooterCentered, Left, Line spacing: single pressure measured at the stagnation point when a gas stream is brought to rest and its kinetic energy Formatted: Font: 11 pt, Not Bold converted by an isentropic compression (3.6)(3.6) from the flow condition to the stagnation condition Formatted: Font: 11 pt [SOURCE: ISO 1217;2009, 3.2.9] **Formatted**

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3.17

ambient temperature

total temperature (3.20) (3.20) of the atmospheric air in the vicinity of the compressor, but unaffected by it

[SOURCE: ISO 1217;2009, 3.3.1]

3.18

discharge temperature

total temperature (3.20)(3.20) at the process air discharge point (3.9)(3.9)

3.19

inlet temperature

total temperature (3.21)(3.21) at the standard process air inlet point (3.8)(3.8)

3.20

total temperature

temperature that would be measured at the stagnation point if a gas stream were brought to rest and its kinetic energy converted by an *isentropic compression* (3.6)(3.6) from the flow condition to the stagnation condition

[SOURCE: ISO 1217;2009, 3.3.4]

3.21

relative humidity

ratio, in humid air, expressed as a percentage, of the water vapour actual pressure to the saturated vapour pressure at the same dry bulb temperature

 $\varphi = \frac{p}{p_{sa}}$

 $\varphi = \frac{p}{p_{\rm sa}}$

where p is partial pressure (ISO 80000-4:20062019, item 4-1514.1) of vapour and p_{sat} is its partial pressure at saturation (at the same temperature)

[SOURCE: ISO 80000-5: 2007 2019, 5-30 33]

3.22

isentropic exponent

ratio of the specific heat at constant pressure to the specific heat at constant volume

3.23

actual volume flow rate

volume flow rate of air, compressed and delivered at the standard discharge point, referred to conditions of *total temperature* (3.20), (3.20), total pressure and composition prevailing at the standard inlet point

3.24

isentropic power

power that is theoretically required to compress an ideal gas under constant entropy, from given inlet conditions to a given $discharge\ pressure\ \frac{(3.14)(3.14)}{(3.14)}$

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ISO 80000-4:2019, Quantities and units — Part 4: Mechanics

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Note 1-to-entry:-The term "ideal gas" is used to indicate any gas in a condition or state so that it follows closely the ideal gas law

[SOURCE: JSO 1217; 2009 Amendment / Amd. 1:2016, 3.5.1]

3.25

isentropic efficiency

ratio of the required *isentropic power* (3.24)(3.24) to measured power for the same specified boundaries with the same gas and the same inlet conditions and *discharge pressure* (3.14)(3.14)

$$\frac{\eta_{\text{isen}}}{P_{\text{real}}} = \frac{P_{\text{isen}}}{P_{\text{real}}}$$

$$\eta_{\text{isen}} = \frac{P_{\text{isen}}}{P_{\text{real}}}$$

[SOURCE: ISO 1217;2009 Amendment / Amd. 1:2016, 3.6.1]

3.26

power input

sum of the electrical power inputs to the prime mover and any ancillaries and auxiliaries driven from the compressor shaft or by a separate prime mover at rated supply conditions, including the effect of all equipment included in the *packaged compressor* (3.5)(3.5)

Note 1-to entry:-Auxiliaries include oil pump, cooling fan and integral compressed air dryer

Note 2-to entry:-Rated supply conditions refer to phase, voltage, frequency and ampere capability

[SOURCE: ISO 1217;2009, 3.5.3]

3.27

specific energy requirement

<of a packaged compressor> power input (3.26)(3.26) per unit of compressor actual volume flow rate [SOURCE: ISO 1217;2009, 3.7.2]

2 20

specific isentropic compression work

work expressed as energy per unit mass of air during isentropic compression (3.6)(3.6)

3.29

specific isochoric compression work

work expressed as energy per unit mass of air during isochoric compression

3.30

$specific\ combined\ compression\ work$

sum of the *specific isentropic compression work* (3.29)[3.28] and *specific isochoric compression work* (3.29), (3.29), weighted by the internal volume ratio

3.31

internal volume ratio

ratio of the enclosed volume at moment of closure of the inlet port to the enclosed volume at the moment of opening of the discharge port for a positive *displacement compressor* (3.2)(3.2)

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3.32

rotor tip speed

peripheral speed at the largest rotor/impeller tip diameter

3.33

machine Mach number

ratio of the rotor tip speed to the speed of sound of the fluid inlet state at inlet conditions

3.34

accounted for value

means (measured/estimated/calculated/corrected) – a simulated or calculated substitute characteristic of components not available for the test, for example; the pressure drop of a remote air filter

3.35

idle power consumption

total consumed power when the *packaged compressor* (3.5)(3.5) is not producing flow to the discharge but is rotating at significant speed. i.e. for *packaged compressor* (3.5)(3.5) equipped with idling functionality

3.36

standby power consumption

power required to keep the packaged compressor (3.5)(3.5) ready for immediate start from non-rotating state

3.37

flow coefficient

flow velocity formed from the inlet volume flow and an impeller cross-section area and rendered dimensionless by the tip speed of the impeller

3.38

work coefficient

specific compression work of the reference process rendered dimensionless by the kinetic energy of tip speed

3.39

reduced speed

alternate test speed used to achieve ratio of Mach number for contract to test equal to one 4_4033_b819_beed40d8df05/iso_fdis-22484

3.40

two speed test

combination of one test to determine the thermodynamic performance and one test to determine the electromechanical performance

3.41

package motor

item(s) that is a part of the packaged compressor (3.5)(3.5) including any additional drive train components

3.42

test motor

item(s) that replaces the package motor (3.41) for testing

3.43

6

shaft power

mechanical input power at the rotor/impeller

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