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ISO/TC 261

Date: 2022-12-262023-xx

Secretariat: DIN

Additive manufacturing of metals — Non-destructive testing and evaluation — Defect detection in parts

<u>Fabrication additive de métaux — Essais et évaluation non destructifs — Détection de</u> <u>défauts dans les pièces</u>

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The committee responsible for this document is ISO/TC-_261, <u>Additive manufacturing</u>, in cooperation with ASTM Committee F42, <u>Additive Manufacturing Technologies</u> on the basis of a partnership agreement between ISO and ASTM International with the aim to create a common set of ISO/ASTM standards on <u>Additive Manufacturing.additive manufacturing</u>, in collaboration with the European Committee for Standardization (CEN) Technical Committee CEN/TC 438, <u>Additive manufacturing</u>, in accordance with the Agreement on technical cooperation between ISO and CEN (Vienna Agreement).

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Introduction

In response to the urgent need for standards for Additive Manufacturing (AM), this document initially indicates Non-Destructive Testing (NDT) methods with potential to detect defects and determine residual strain distribution that are generated in AM processes. A number of these methods were verified. The strategy adopted was to review existing NDT standards for matured manufacturing processes which are similar to AM, namely casting and welding. This potentially reduces the number of standards required to comprehensively cover the defects in AM. For identified AM unique defects, this document proposes a two-level NDT approach: a star artefact as an Initial Quality Indicator (IQI) and *à la carte* artefact where an example shows the specific steps to follow for the very specific unique AM part to be built, paving the way for a structured and comprehensive framework.

Most metal inspection methods in NDT use ultrasound or X-rays, but these techniques cannot always cope with the complicated shapes typically produced by AM. In most circumstances X-ray computed tomography (CT) is a more suitable method, but it also has limitations and room for improvement or adaptation to AM, on top of being a costly method both in time and money.

This document includes post-process non-destructive testing of additive manufacturing (AM) of metallic parts with a comprehensive approach. It covers several sectors and a similar framework can be applied to other materials (e.g. ceramics, polymers, etc.). In-process NDT and metrology standards are referenced as they are being developed. This document presents current standards capability to detect which of the Additive Manufacturing (AM) flaw types and which flaws require new standards, using a standard selection tool. NDT methods with the highest potential will be tested.

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Additive manufacturing — Non-Destructive Testing and Evaluation — Standard Guideline for Defect Detection in Metallic Parts

1 Scope

This document categorises Additive Manufacturingadditive manufacturing (AM) defects in DED and PBF laser and electron category of processes, provides a review of relevant current NDT standards, details NDT methods that are specific to AM and complex 3D geometries and outlines existing non-destructive testing techniques that are applicable to some AM types of defects.

This document is aimed at users and producers of AM processes and it applies, in particular, to the following:

- <u>Safetysafety</u> critical AM applications;
- Assuredassured confidence in AM;
- <u>Reversereverse</u> engineered products manufactured by AM;
- <u>Testtest</u> bodies wishing to compare requested and actual geometries.

2 Normative references

<u>O/ASTM DTR 52905</u>

There are no normative references in this document. standards/sist/12b7de41-101c-47e

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 11484, Steel products — Employer's qualification system for non-destructive testing (NDT) personne

<u>ISO/ASTM 52900, Additive manufacturing — General principles — Fundamentals and vocabulary</u>

ASTM E1316, Terminology for Nondestructive Testing

<u>EN 1330-2, Non-destructive testing — Terminology — Part 2: Terms common to the non-destructive testing methods</u>

3 Terms and definitions

For the purposes of this document, the terms and definitions given in <u>ISO/ASTM 52900</u>, <u>ASTM E1316</u>, EN 1330-2, ISO 11484, and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

ISO-Online browsing platform: available at https://www.iso.org/obp

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IEC Electropedia: available at <u>https://www.electropedia.org/</u>https://www.electropedia.org/

3.1

flaw type

identifiable features that defines a specific flaw

Note 1 to entry: defect term, this word is used when a flaw that does not meet specified acceptance criteria and is rejectable.

Note 2 to entry: flawFlaw term, an imperfection or discontinuity that is not necessarily rejectable

3.2

lack of fusion

LOF

type of process-induced porosity, in which the powder or wire feedstock is not fully melted or fused onto the previously deposited substrate

Note 1 to entry: In PBF, this type of flaw can be an empty cavity, or contain unmelted or partially fused powder, referred to as unconsolidated powder.

Note 2 to entry: LOF typically occurs in the bulk, making its detection difficult.

Note 3 to entry: Like voids, LOF can occur on the build layer plane (layer/horizontal LOF) or across multiple build layers (cross layer/vertical LOF).

3.3

unconsolidated powder

unmelted powder that due to process failure was not melted and became trapped internally

3.4

layer shift

<u>SO/ASTM DTR 52905</u>

see stop/start for PBF laser/E beam. In addition, in E beam \leq E beam \geq when it is disturbed by a magnetic field a layer or a number of layers are shifted away from the other build layers.

Note 1 to entry: see stop/start for PBF laser/E beam.

3.5

trapped powder

unmelted powder that is not intended for the part but is trapped within internal part cavities

3.6

porosity

presence of small voids in a part making it less than fully dense

Note 1 to entry: Porosity may be quantified as a ratio, expressed as a percentage of the volume of voids to the total volume of the part.

[SOURCE: ISO/ASTM 52900:2019, 3.11.8]

3.7

keyhole

type of porosity characterised by a circular depression formed due to instability of the vapor cavity during processing

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Note 1 to entry: Keyhole porosity is created when the energy density is sufficiently high to cause a deep melt pool resulting in hydrodynamic instability of the surrounding liquid metal and subsequent collapse, leaving a void a the root of the keyhole.

Note 2 to entry: Like generic voids and gas porosity, keyhole porosity causes a part to be less than fully dense.

94_NDT potential for authentication and/or identification

Some of the NDT methods in this technical report have the additional potential to extract authentication and/or identification apparatus or design embedded in the design of the AM part. Such a potential clearly depends on the material(s), geometry and process elected to fabricate the part, however the design information and AM data file can embed in its geometry or texture ad-hoc devices that potentially could be extracted by NDT techniques. ISO/TC-_292-Security and Resilience specifies and maintains a number of standards supporting such devices within the ISO referential, and are fully applicable to AM digital information. The specific requirements of design techniques, materials, processes, NDT modalities and applications, however, still require careful evaluation, selection and classification.

<u>105</u> List of abbreviated terms

	AM	Additive Manufacturingadditive manufacturing Deleted Cells
_	BAE	British Aerospace and Engineering Systems
_	EB-PBF	Electron Beam Powder Bed Fusionelectron beam powder bed fusion
_	ESFR	European Synchrotron Research Facility
_	EWI	Edison Welding Institute
_	FMC	Full Matrix Capture <u>full matrix capture</u> ISO/ASTM DTR 52905
_	GE-PD ttps	General Electric Powder Divisiongeneral electric powder division -101c-47e1-acd3-83fd82ac1220/iso-
_	HZB	Helmholtz Zentrum Berlin astm-dtr-52905
_	ILL	Institute Laue-Langevin
_	IR	Infrared infrared
_	IRT	Infrared Thermographyinfrared thermography
_	J & J	Johnson & Johnson
_	LNE	Laboratoire National De Métrologie ET D'essais
_	PBF-LB	Laser Powder Bed Fusionlaser powder bed fusion
_	DED-LB	Laser Directed Energy Depositionlaser directed energy deposition
_	MTC	The Manufacturing Technology Centre
_	ND	Neutron Diffractionneutron diffraction
_	NDE	Nonnon-destructive evaluation
_	NDT	Nondestructive Testingnon-destructive testing
_	NI	Neutronneutron Imaging
_	NIST	National Institute of Standards and Technology
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_	NLA	Nonnon-linear Acoustic Testingacoustic testing
—	NLR	Nonnon-linear Resonance Testingtesting
_	PAUT	Phase Array Ultrasoundphase array ultrasound Testing
_	PCRT	Process Compensated Resonance Testingprocess compensated resonance testing
_	РТ	Pulsepulse thermography
_	RAM	Resonance Acoustic Methodresonance acoustic method
_	ROI	Region-of Interestinterest
_	SX	X-ray Synchrotron synchrotron
_	SHT	Step Heating Thermographystep heating thermography
_	TFM	Total Focusing Methodtotal focusing method
_	TMS	The Modal Shopthe modal shop
_	UoB	<u>Universityuniversity</u> of <u>Bathbath</u>
—	ХСТ	X-ray Computed Tomographycomputed tomography

116 Typical flaws/defects in AM

11.16.1 Flaw origins/causes

The causes of defects across different types of AM processes can be quite different, but the defects that they generate can be remarkably similar. Detecting the defects also does not depend on the cause, and in general only the size and geometry (and potentially morphology) of the defect matters for detection.

The causes and effects of a number of AM flaws have been reported in the European project AMAZE.^{[2][21]}, Table A.1 and Table A.2-in Annex A give explanations of the mechanisms by which these flaws are generated and those mechanisms are linked to the process parameters selected and the resulting processing conditions.^[3], see ISO 11484. Understanding the conditions under which flaws are generated and simplifying the terminology used to describe these flaws will hopefully aid the drive for quality improvement required for widespread implementation of the technology.

The flowchart displayed in Figure 1 gives an idea of the complexity of flaw generation within the PBF process. As can be seen, the generation of one flaw type can result in an anomalous processing condition, which in turn generates a second flaw. For example, the presence of a thick layer or low laser (or electron beam) power can lead to under-melting, which in turn can lead to unconsolidated powder. Coupled with the tendency of the power source to decrease the surface energy of unconsolidated powder under the action of surface tension, ensuing ball formation may arise due to shrinkage and worsened wetting, leading to pitting, an uneven build surface, or an increase in surface roughness $\frac{144}{30}$, see EN 1330-2.

Therefore, even when there are multiple causes, a single flaw type or conditions can be generated (excessive surface roughness) causing failure by a single failure mode (surface cracking leading to reduced fatigue properties). Alternatively, it is also conceivable that a single flaw type or condition can cause failure by several different failure modes.

11.26.2 Flaw/defects classification

Post-built AM flaws have been identified based on a report from the FP7 European AMAZE project. Potential flaws in directed energy deposition (DED) and powder bed fusion (PBF) are listed in <u>Table 1</u> and Table 2 respectively. A brief description for each flaw type is also given in the tables.

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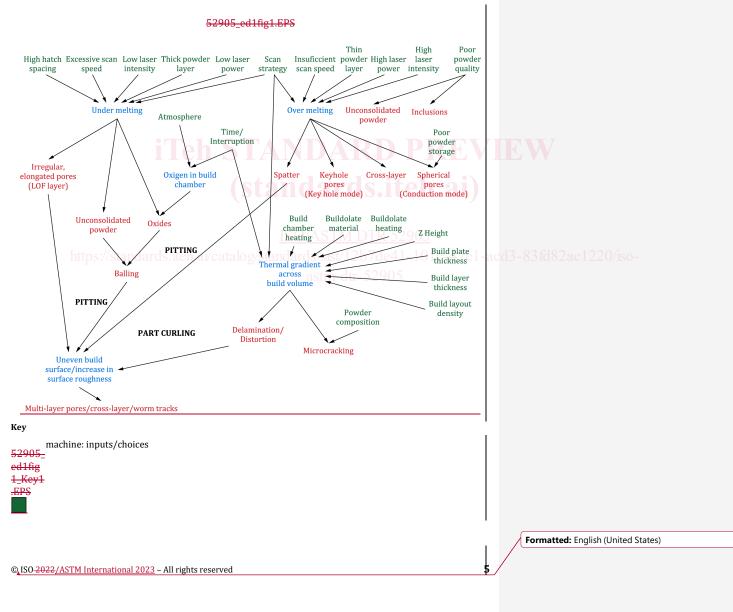
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Due to the similarity in manufacturing, defects from welding and casting bear some resemblance to defects from AM processes such as PBF and DED. Defects in post-built PBF and DED parts are identified and listed in various references [4–6]-EN 1330-2, ASTM E1316 and References [22]. As noted in Table 1 and Table 2, both technologies have common defects such as porosity, inclusions, undercuts, geometry, LOF, and a rough surface texture. However, the mechanisms for PBF and DED defect generation are very different, and more importantly, the relative abundance of each defect type will be very different due to the melting and solidification mechanisms involved (and the significantly higher thermal gradients present in DED). DED involves imparting a momentum into the melt pool rather than melting the powder that is already present. The important difference between the two methods is that of timescales.

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AM part: resulting defect/flaw 52905_ ed1fig 1_Key2 .EPS
process: resulting condition 52905_ ed1fig 1_Key3 .EPS
common type of failure 52905_ ed1fig 1_Key4 -FPS

Figure 1 — Causes, mode of failures and defect formation in PBF AM^[4] (see ISO/ASTM 52900)

In PBF, there is a balance of timescales between melting and re-solidification. If the melt rate is too low, then the melt pool can become unstable and break into multiple pools. If the melt rate is too high, powder partially melts in front of the melt pool, which can cause defects or heat affected zones. In DED, this balance is not relevant, but the powder (or wire) that is fed into the melt pool can melt sufficiently quickly. The issue of adding cold material (with a given momentum) to a melt pool is not well understood, but has a large effect on the Marangoni convection direction and thermal gradients present. It is likely that the melt pool depth will be much shallower (which may reduce powder surrounding the melt pool) and that the thermal gradients less severe (which cause a flatter melt pool), though this depends on the wetting between substrate (which has no surrounding powder) and the melt pool. This difference in the melt pool dynamics impacts its shape.

This has two important consequences, grain growth and bubble dynamics. Internal defects are attributable to cracking, pores, or lack of material. Cracking has many causes, but is generally related to the grain boundary (apart from solidification cracking). Note that the issue of "spattering" that is believed to be prominent in DED (or indeed welding) is still a significant issue in PBF. For L-PBF the issue is that of ablation at the surface of the melt pool caused by the large thermal gradients. For EB-PBF the problem occurs from two mechanisms; ablation and charging of the powder.

Table 1 — Typical flaws in Directed Energy Depositiondirected energy deposition

Flaw Type<u>type</u>	Description	
	The surface roughness on the part does not meet the target specification for the part. Measurement of the surface roughness is considered out-of-scope for NDT however, vis examination can be included.	

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Flaw Type<u>type</u>	Description	
	52905_ed1figTab1_01.EPS	
Porosity	Typically spherical in shape and contains gas. Porosities can grow in a line to form a chain or elongated porosity.	
	52905_ed1figTab1_02.EPS	
		IEW
Incomplete fusion	Fusion between the entire base metal surfaces and between adjoining welds are not complete. This occurs when new material has been used and the build parameters have not been optimised. Typically, this flaw is eliminated as the process improved when all parameters have been optimised.	cd3-83fd82ac1220/iso-
	52905_cd1ftgTab1_03.EPS	
Undercuts at the toe of the welds between adjoining weld beads	A groove melted into the base metal adjacent to the weld toe or weld face and left unfilled by weld metal.	

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