# INTERNATIONAL STANDARD



First edition

Determination of galvanic corrosion rate for assembled forms of carbon fibre reinforced plastics (CFRPs) and protection-coated metal — Electrochemical tests in neutral sodium chloride solution

Détermination du taux de corrosion galvanique pour les formes assemblées de plastiques renforcés de fibres de carbone (CFRP) et de métal revêtu de protection — Essais électrochimiques en solution neutre de chlorure de sodium

ISO/PRF 8057

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#### Foreword

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This document was prepared by Technical Committee ISO/TC 61, *Plastics*, Subcommittee SC 13, *Composites and reinforcement fibres*.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at <u>www.iso.org/members.html</u>.

### Determination of galvanic corrosion rate for assembled forms of carbon fibre reinforced plastics (CFRPs) and protection-coated metal — Electrochemical tests in neutral sodium chloride solution

#### 1 Scope

**1.1** This document specifies the electrochemical test for determining galvanic corrosion rate of CFRPs and metal assemblies with protection-coating, subjected to the corrosive environment of electrolyte diffusion through the coating. It specifies the apparatus, the test solutions, and the procedure to be used in conducting the electrochemical tests for

- a) the assessment of the Fick's diffusion parameter for protective coating on metallic materials, and
- b) the estimation of the galvanic corrosion rates with the conversion of ISO 21746 coating-free sample data.

**1.2** The following are intended situations of implementing an electrochemical test based on this document:

- a) when interested parties estimate the galvanic corrosion rate of bonded joints relating engineering metals with protection-coating and CFRPs of the potential drastically nobler than those of most metals, utilizing the resources of ISO 17475;
- b) when expanding CFRP-metal bonded joints applications using coatings to the fields of corrosionsensitive environments caused by electrolytes.

**11: 1.3** <sup>st</sup> It is not the intent of this document to fulfil the need for: <sup>3-9a2f-9bf8720de465/iso-prf-8057</sup>

- omitting relevant field tests for the applications in corrosive environment;
- superimposing test data for specific applications for the range of relevant data;
- comparative testing as a means of ranking different protections with respect to corrosion rates;
- ignoring the field hazards such as erosion, abrasion, and ultraviolet irradiation.

#### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 2808, Paints and varnishes — Determination of film thickness

ISO 17475, Corrosion of metals and alloys — Electrochemical test methods — Guidelines for conducting potentiostatic and potentiodynamic polarization measurements

ISO 21746, Composites and metal assemblies — Galvanic corrosion tests of carbon fibre reinforced plastics (CFRPs) related bonded or fastened structures in artificial atmospheres — Salt spray tests

#### 3 Terms and definitions

No terms and definitions are listed in this document.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <a href="https://www.iso.org/obp">https://www.iso.org/obp</a>
- IEC Electropedia: available at <u>https://www.electropedia.org/</u>

#### 4 Symbols

- *a* slope of *Q*-*t* plot
- *b* error in *Q*-*t* plot owing to charge duration and other factors
- *C* static capacity of capacitor
- *c*<sub>0</sub> saturated oxygen density in water
- *c*(*x*) electrolyte density function
- d coating thickness
- *D* Fick's diffusion parameter
- $D_{\rm ox}$  oxygen diffusion constant in water
- $E_{\rm cr}$  estimation of galvanic corrosion rate for coated sample site A and A
- $F_{pe}$  protection efficiency **Document Preview**
- J diffusion flux

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J<sub>ASO</sub> httpoxygen flux in air saturated static water st/2374cbf6-56fb-47c3-9a2f-9bf8720de465/iso-prf-8057

- $J_{\rm PC}$  steady flux through thin protective coating
- $J_{PCO}$  oxygen flux through protection coating
- $J_{\rm PFO}$  oxygen flux for protection free sample
- $J_{0Max}$  the maximum through coating flux of oxygen in the form of water solution
- $K_{\rm cr}$  galvanic corrosion rate of coating-free sample derived with ISO 21746
- *Q* charge at a time *t*
- $Q_0$  charge at linearly extrapolated time point  $t_0$
- *S* gird area of capacitor
- $t_0$  flux onset time
- $t_1$  upper bound time of linear section in time-charge plot
- *V* inter-grid potential of capacitor
- $x_1$  inter-grid distance of capacitor
- *X*<sub>2</sub> locational dimension in flux direction

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- the diffusion layer thickness of air saturated static water X<sub>DL</sub>
- diffusion layer thickness X<sub>DL</sub>
- permittivity of vacuum  $\varepsilon_0$
- $\varepsilon_r$ relative permittivity

#### **Principle** 5

#### 5.1 General

Protection coating behaves as a capacitor in the form between conductive materials and conductive electrolytes. Focusing on the capacitance, Fick's diffusion parameter is monitored by analysing the drift in charge due to the distance shrinkage with water absorption from the surface of the protective coating in the plate-shaped sample. The effect of the protective coating is evaluated by converting the value into the salt spray flux in the galvanic corrosion test.

#### 5.2 Capacitor model

Static capacity, *C*, of a capacitor in <u>Figure A.1</u> is expressed as <u>Formula (1)</u>:

$$C = \varepsilon_r \varepsilon_0 \frac{s}{x_1}$$
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where  $\varepsilon_0 = 8,85418762 \times 10^{-12}$  is the permittivity of vacuum.

The charge, Q, is expressed as follows when inter-grid potential, V, is loaded.

$$Q = CV$$
 (2)

Formulae (1) and (2) lead to the following expression. 56(b-47c3-9a2f-9bf8720de465/iso-prf-8057

$$Q = \varepsilon_r \varepsilon_0 \frac{SV}{x_1} \tag{3}$$

When the inter-grid distance x shrinks to  $x_1 - \Delta x_1$  through diffusion, the charge drift  $\Delta Q$  is expressed using Formula (3) as follows.

$$x_1 \Delta Q + Q \Delta x_1 = 0$$





Figure 1 — Schematic diagram of capacitor

A capacitor in Figure 1 is expressed as is shown in Figure 2 for a grid of conductive base material, a grid of electrolyte, and thin coating with the thickness  $x_1$  to separate the grids.



#### Key

- 1 water/electrolyte
- 2 conductive base
- 3 thin coating layer

#### Figure 2 — Capacitor formation with thin coating layer

### 5.3 Fick's diffusion coefficient for thin coating layer

A. Fick expressed the phenomenon of water diffusion in a mathematical form using an analogy with the laws of heat conduction derived by Fourier and the diffusion of electricity in a conductor derived by Ohm. The diffusive flux occurring in a unit of time through a medium of small distance is expressed in Fick's first law proportional to the difference of density and inversely proportional to the distance of the medium. Fick's second law is derived assuming the proportional coefficient constant – Fick's diffusion constant – and the conservation of mass for the unsteady state of diffusion. See <u>Annex A</u>.

For thick media, Fick's second law has been applied assuming the density distribution is regular along the thickness during the diffusion of unsteady flux. However, Fick's first law provides an acceptable approximation for thin region of media in the form of linear density distribution along the thickness at the diffusion of steady flux as illustrated in Figure 3.



- 5 regular
- 6 thin coating
- 7 linear

#### Figure 3 — Fick's diffusion model for a thick coating and the thin region

Fick's diffusion coefficient *D* is defined as follows in Fick's first law.

$$J = -D\frac{dc(x_2)}{dx}$$
(5)

where  $c(x_2)$  is the electrolyte density function, and  $x_2$  is the locational dimension in the flux direction. Formula (5) is approximated for a thin protective coating of the thickness  $d \rightarrow 0$  with steady flux through the thickness  $J_{PC}$  as follows.

$$J_{PC} \approx -D \frac{c(0) - c(d)}{d} \tag{6}$$

The flux  $J_{PC}$  is also approximated as follows atop of the coating in a short period of time  $\Delta t$ .

$$J_{PC} \approx (c(0) - c(d)) \frac{\Delta x_2}{\Delta t}$$
(7)

Fick's diffusion coefficient *D* is therefore approximated with the Formulae (6) and (7) as follows.

$$D = -d \cdot \frac{\Delta x_2}{\Delta t} \tag{8}$$

The Formulae (4) and (8) lead to an expression as follows for the case *x*=*d* in Formula (7).

$$D = d^{2} \cdot \frac{\left(\frac{\Delta Q}{Q}\right)}{\Delta t}$$
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$$\frac{\Delta Q}{Q} = \left(\frac{D}{d^2}\right) \cdot \Delta t.$$

Thereby Fick's diffusion coefficient *D* is given with a slope  $a = \frac{D}{d^2}$  on a  $\Delta Q/Q$  – it plot, as  $D = a \cdot d^2$ .

#### 5.4 Corrosion rate estimation

The galvanic corrosion rate is diffusion-limited of the oxygen supply for the anodic metal. Therefore, a known corrosion rate of protection free sample  $K_{cr}$  derived with ISO 21746 on the oxygen saturated

(10)