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## Standard Guide for Estimation of LNAPL Transmissivity<sup>1</sup>

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### 1. Scope

1.1 This guide provides field data collection and calculation methodologies for the estimation of light non-aqueous phase liquid (LNAPL) transmissivity in unconsolidated porous sediments. The methodologies presented herein may, or may not be, applicable to other hydrogeologic regimes (for example, karst, fracture flow). LNAPL transmissivity represents the volume of LNAPL ( $L^3$ ) through a unit width ( $L$ ) of aquifer per unit time ( $t$ ) per unit drawdown ( $L$ ) with units of ( $L^2/T$ ). LNAPL transmissivity is a directly proportional metric for LNAPL recoverability whereas other metrics such as apparent LNAPL thickness gauged in wells do not exhibit a consistent relationship to recoverability. The recoverability for a given gauged LNAPL thickness in a well will vary between different soil types, LNAPL types or hydrogeologic conditions. LNAPL transmissivity accounts for those parameters and conditions. LNAPL transmissivity values can be used in the following five ways: (1) Estimate LNAPL recovery rate for multiple technologies; (2) Identify trends in recoverability via mapping; (3) Applied as a leading (startup) indicator for recovery; (4) Applied as a lagging (shutdown) indicator for LNAPL recovery; and (5) Applied as a robust calibration metric for multi-phase models (Hawthorne and Kirkman, 2011 **(1)**<sup>2</sup> and ITRC **(2)**). The methodologies for LNAPL transmissivity estimation provided in this document include short-term aquifer testing methods (LNAPL baildown/slug testing and manual LNAPL skimming testing), and long-term methods (that is, LNAPL recovery system performance analysis, and LNAPL tracer testing). The magnitude of transmissivity of any fluid in the subsurface is controlled by the same variables (that is, fluid pore space saturation, soil permeability, fluid density, fluid viscosity, the interval that LNAPL flows over in the formation and the gravitational acceleration constant). A direct mathematical relationship exists between the transmissivity of a fluid and the discharge of that fluid for a given induced drawdown. The methodologies are generally aimed at measuring the relationship of discharge versus drawdown for the occurrence of LNAPL in a well, which can be used to estimate the transmissivity of LNAPL in the formation. The focus, therefore, is to provide standard methodology on how to obtain accurate measurements of these two parameters (that is, discharge and drawdown) for multi-phase occurrences to estimate LNAPL transmissivity.

#### 1.2 Organization of this Guide:

1.2.1 Section 2 presents documents referenced.

1.2.2 Section 3 presents terminology used.

1.2.3 Section 4 presents significance and use.

1.2.4 Section 5 presents general information on four methods for data collection related to LNAPL transmissivity calculation. This section compares and contrasts the methods in a way that will allow a user of this guide to assess which method most closely aligns with the site conditions and available data collection opportunities.

1.2.5 Sections 6 and 7 presents the test methods for each of the four data collection options. After reviewing Section 5 and selecting a test method, a user of this guide shall then proceed to the applicable portion of Sections 6 and 7 which describes the detailed test methodology for the selected method.

1.2.6 Section 8 presents data evaluation methods. After reviewing Section 5 and the pertinent test method section(s) of Sections 6 and 7, the user of this guide shall then proceed to the applicable portion(s) of Section 8 to understand the methodologies for evaluation of the data which will be collected. It is highly recommended that the test methods and data evaluation procedures be understood prior to initiating data collection.

1.3 The values stated in inch-pound units are to be regarded as standard. The values given in parentheses are mathematical conversions to SI units that are provided for information only and are not considered standard.

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<sup>2</sup> The boldface numbers in parentheses refer to the list of references at the end of this standard.

1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

1.5 This document is applicable to wells exhibiting LNAPL consistently (that is, LNAPL transmissivity values above zero). This methodology does not substantiate zero LNAPL transmissivity; rather the lack of detection of LNAPL within the well combined with proper well development and purging procedures are required to confirm zero LNAPL transmissivity.

1.6 This document cannot replace education or experience and should be used in conjunction with professional competence in the hydrogeology field and expertise in the behavior of LNAPL in the subsurface.

1.7 This document cannot be assumed to be a substitute for or replace any laws or regulations whether federal, state, tribal or local.

## 2. Referenced Documents

2.1 ASTM Standards:<sup>3</sup>

**D653** Terminology Relating to Soil, Rock, and Contained Fluids

**D5088** Practice for Decontamination of Field Equipment Used at Waste Sites

**D5521** Guide for Development of Ground-Water Monitoring Wells in Granular Aquifers

**E2531** Guide for Development of Conceptual Site Models and Remediation Strategies for Light Nonaqueous-Phase Liquids Released to the Subsurface

## 3. Terminology

3.1 Definitions:

3.1.1 *air/LNAPL interface* ( $Z_{an}$ )—The surface shared by air and LNAPL in a control well. (L)

3.1.2 *calculated water-table elevation* ( $Z_{CGW}$ )—the theoretical location of the air/water surface based on a density correction if LNAPL were not present in a well. (L)

3.1.3 *confined LNAPL*—LNAPL trapped in an aquifer beneath a layer that exhibits a pore entry pressure greater than the capillary LNAPL head, thereby impeding the upward migration of LNAPL limits the upward movement of the LNAPL. The term confined LNAPL is used because the mobile LNAPL is under pressure greater than gauge pressure against the underside of the LNAPL confining layer.

3.1.4 *control well*—well by which the aquifer is stressed or tested.

3.1.5 *discharge*—the flow of a fluid into or out of a well. ( $L^3/t$ )

3.1.6 *drawdown*—a pressure differential in terms of fluid head. (L)

3.1.7 *effective well radius*—the radius that represents the area of the well casing and the interconnected porosity of the filter pack. (L)

3.1.8 *equilibrium fluid levels*—gauged fluid levels that represent the oil head and the water head or the calculated water-table elevation of the formation. Under equilibrium fluid levels no net oil or water flow occurs between the formation and the well.

3.1.9 *fluid level*—the level of a fluid interface (either air/oil, LNAPL/water, or potentiometric surface).

3.1.10 *formation thickness* ( $b_{nf}$ )—the interval that LNAPL flows over in the formation. For unconfined conditions this is approximately equal to the gauged LNAPL thickness. Confined and perched conditions the gauged LNAPL thickness under equilibrium conditions is not equal to the formation thickness. (L)

3.1.11 *gauged LNAPL thickness* ( $b_n$ )—The difference between the gauged air/LNAPL interface and the water/LNAPL interface in a well. (L)

3.1.12 *hydraulic conductivity* (*derived via field aquifer tests*)—the volume of water at the existing kinematic viscosity that will move in a unit time, under a unit hydraulic gradient, through a unit area, measured at right angles to the direction of flow. (L/t)

3.1.13 *LNAPL*—Light Non Aqueous Phase Liquid.

3.1.14 *LNAPL baildown test*—a procedure which includes the act of removing a measured LNAPL volume from a well and filter pack to induce a head differential and the follow-up gauging of fluid levels in the well.

3.1.15 *LNAPL borehole volume*—the volume of LNAPL existing within the casing and the drainable volume existing within the filter pack of a well. Based on effective radius and gauged thickness of LNAPL. ( $L^3$ )

3.1.16 *LNAPL slug test*—a procedure which includes the act of removing or displacing a known volume of LNAPL from a well to induce a head differential and the follow-up gauging of fluid levels in the well.

<sup>3</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

3.1.17 *LNAPL specific yield ( $S_{yn}$ )*—the volume of LNAPL an aquifer releases or takes into storage per unit surface area of the aquifer per unit change in LNAPL head for gravity drainage conditions. (unitless)

3.1.18 *LNAPL specific yield filter pack ( $S_{yf}$ )*—the volume of LNAPL released or takes into storage per unit surface area of the filter pack per unit change in LNAPL head for gravity drainage conditions. (unitless)

3.1.19 *LNAPL storage coefficient ( $S_n$ )*—the volume of LNAPL an aquifer releases from or takes into storage per unit surface area of the aquifer per unit change in LNAPL head. For a confined aquifer, it is based on the volume of fluid released due to decompression. For an unconfined aquifer, the storage coefficient is approximately equal to the LNAPL specific yield. (unitless)

3.1.20 *LNAPL transmissivity ( $T_n$ )*—the volume of LNAPL at the existing kinematic viscosity that will move in a unit time under a unit hydraulic gradient through a unit width of the aquifer. ( $L^2/t$ )

3.1.21 *observation well*—a well screened across all or part of an aquifer.

3.1.22 *oil/water interface ( $Z_{ow}$ )*—The surface shared by LNAPL and water in a control well. (L)

3.1.23 *perched LNAPL*—mobile LNAPL that accumulates in the vadose zone of a site for some time period above a layer that exhibits a pore entry pressure greater than the capillary LNAPL head, thereby impeding the downward migration of LNAPL.

3.1.24 *potentiometric surface*—see *calculated water-table elevation*.

3.1.25 *radius of influence*—the distance from a well that the pumping induced head differential from non-pumping conditions is zero, head differentials due to background gradients may still exist at this radius. (L)

3.1.26 *slug*—a volume of water or solid object used to induce a sudden change of head in a well.

3.1.27 *test well*—a well by which the aquifer is stressed, for example, by pumping, injection, or change of head.

3.2 For definitions of other terms used in this test method refer to Terminology, Guide [D653](#).

## 4. Significance and Use

### 4.1 Application:

4.1.1 LNAPL transmissivity is an accurate metric for understanding LNAPL recovery, is directly proportional to LNAPL recoverability and tracking remediation progress towards residual LNAPL saturation.

4.1.2 LNAPL transmissivity can be used to estimate the rate of recovery for a given drawdown from various technologies.

4.1.3 LNAPL transmissivity is not an intrinsic aquifer property but rather a summary metric based on the aquifer properties, LNAPL physical properties, and the magnitude of LNAPL saturation over a given interval of aquifer.

4.1.4 LNAPL transmissivity will vary over time with changing conditions such as, seasonal fluctuations in water table, changing hydrogeologic conditions and with variability in LNAPL impacts (that is, interval that LNAPL flows over in the formation and LNAPL pore space saturation) within the formation. [ASTM E2856-13](#)

4.1.5 Any observed temporal or spatial variability in values derived from consistent data collection and analysis methods of LNAPL transmissivity is not erroneous, rather is indicative of the actual variability in subsurface conditions related to the parameters encompassed by LNAPL transmissivity (that is, fluid pore space saturation, soil permeability, fluid density, fluid viscosity, and the interval that LNAPL flows over in the formation).

4.1.6 LNAPL transmissivity is a more accurate metric for evaluating recoverability and mobile LNAPL than gauged LNAPL thickness. Gauged LNAPL thickness does not account for soil permeability, magnitude of LNAPL saturation above residual saturation, or physical fluid properties of LNAPL (that is, density, interfacial tension, and viscosity).

4.1.7 The accurate calculation of LNAPL transmissivity requires certain aspects of the LNAPL Conceptual Site Model (LCSM) to be completely understood and defined in order to calculate LNAPL drawdown correctly. The methodologies for development of the LCSM are provided in Guide [E2531](#). The general conceptual site model aspects applicable to this guide include:

4.1.7.1 Equilibrium fluid levels (for example, air/LNAPL and LNAPL/water).

4.1.7.2 Soil profile over which LNAPL is mobile.

4.1.7.3 LNAPL hydrogeologic scenario (for example, unconfined, confined, perched, macro pores, and so forth).

4.1.7.4 LNAPL density.

4.1.7.5 Hydraulic conductivity for each soil type within the well screen interval.

4.1.7.6 Well screen interval in the vadose and saturated zones.

4.1.8 Incorporation of LNAPL transmissivity can further LCSMs by providing a single comparable metric that quantifies LNAPL recoverability at individual locations across a site.

4.1.9 Each of the methods provided in this document is applicable to LNAPL in confined, unconfined, and perched conditions. Any differences in evaluation are discussed in Section [5](#).

4.2 *Purpose*—The methods used to calculate LNAPL transmissivity have been published over the past 20 years; however little effort has been focused on providing quality assurance for individual tests or refinement of field procedures. In addition to summarizing the existing methods to calculate LNAPL transmissivity, this document will provide guidance on refined field procedures for data collection and minimum requirements for data sets before they are used to calculate LNAPL transmissivity.

4.2.1 *Considerations*—The following section provides a brief review of considerations associated with LNAPL transmissivity testing.

4.2.1.1 *Aquifer Conditions (confined, unconfined, perched)*—In general, each testing type is applicable to confined, unconfined, and perched conditions; however, consideration should be given to how LNAPL drawdown is calculated from well gauging data relative to formation conditions. Calculation of LNAPL transmissivity for confined and perched conditions is possible; however, the soil profile needs to be considered in combination with the fluid levels to accurately calculate drawdown. Drawdown values for perched and confined conditions can easily be overestimated without proper consideration. This results in LNAPL transmissivity being underestimated. The calculations of drawdown under perched and confined conditions are discussed within this document. Tidal influences or a vertical gradient on the water table also affect measurements and could distort the transmissivity results. Tidal influences are discussed in more detail in [Appendix X1](#).

4.2.1.2 *Well Construction*—Any well being tested should be screened over the entire mobile interval of LNAPL. For locations where multiple discrete mobile intervals exist, it may be preferable to screen individual wells across each mobile interval. This will simplify the calculation of drawdown and derivation of LNAPL transmissivity. The interval of mobile LNAPL does not always correspond to the elevation of the air/LNAPL interface (for example, the mobile interval can be beneath the base of a confining layer under confined conditions). Appropriately screened wells can be substantiated based on vertical delineation of the entire LNAPL impacted interval (see Guide [E2531](#)).

4.2.1.3 *LNAPL Type*—No limitations have been identified for LNAPL type. However, the specific gravity of the LNAPL must contrast with that of the water to be measurable with an interface probe.

4.2.1.4 *Well Development*—In order to derive the most accurate LNAPL transmissivity value, appropriate well development should be conducted to ensure connectivity between LNAPL in the formation and the well (Hampton 2003) (3). Industry experience has observed that LNAPL can require up to several months following well installation to saturate the filter pack and establish connectivity within the well. Well development can help to reduce this time frame and should be completed in accordance with Guide [D5521](#).

4.2.2 *Analysis Method*—An understanding of the analysis method and theory is necessary prior to the field testing to ensure that all appropriate dimensions and measurements are properly recorded.

4.3 *Precision and Bias*—At this time this document aims to provide methodologies for data collection and analysis to yield an accuracy of LNAPL transmissivity values within a factor of two (compared with the unknown actual value). This modest accuracy is reasonable based on the overall industry experience in implementing these procedures and the lack of comparison studies. The objectives initiated through development of this document are to provide improved guidance for more consistent data collection and analysis methodology, which in turn will provide a larger and more accurate data set on which to base future methodology revisions and improvements.

## 5. Method Selection

5.1 The following section describes each of four test methods for the user to evaluate which methodology best fits their data objectives, site setting, and hydrogeologic conditions. An overview of this section is provided in [Table A2.1](#) and [Table A2.2](#). A review of the required parameters to be measured is provided in [Tables A2.3-A2.9](#).

### 5.2 *Baildown/Slug Testing:*

5.2.1 *Overview*—The LNAPL baildown/slug test consists of either removing the entire LNAPL from the well casing and filter pack or the displacement of a partial volume to induce a head differential, respectively. Following the induction of the head differential, fluid levels are gauged during recovery.

5.2.2 *Data Analysis*—The LNAPL baildown/slug test field procedure is used in conjunction with LNAPL slug test analytical procedures to provide estimates of LNAPL transmissivity at any well exhibiting sufficient LNAPL thickness (that is, at least 0.5 ft/15.2 cm).

5.2.3 *Waste Disposal*—The baildown/slug test provides an advantage over other tests in that it does not typically require the disposal of large quantities of LNAPL or water that may be produced, nor does it require specialized equipment.

5.2.4 *Aquifer Extent Represented*—LNAPL baildown/slug tests reflect conditions near the well, and therefore represent a limited radius of influence. LNAPL transmissivity values from baildown/slug tests may not compare well with transmissivity values estimated using recovery system-based data (5.3) because of the differences in scale of evaluation between the two methods. However, increasing or decreasing trends in transmissivity will be seen in both recovery system-based data and baildown testing-based data.

5.2.5 *Capital Cost*—The capital cost for this method is low because it can be implemented on existing wells exhibiting LNAPL, does not require the construction of a recovery system nor does it require specialized equipment above and beyond other methods.

5.2.6 *Test Duration*—The test length timeframe is inversely related to the transmissivity of LNAPL and directly related to the effective well radius. LNAPL baildown/slug tests may require minutes to months to completely recover as LNAPL transmissivity may vary by several orders of magnitude across sites. However, in cases of slow recovery (that is, greater than a month) and where high confidence exists that the initial fluid levels represent equilibrium conditions, it is not necessary to allow the well to fully recover. A data set representing partial recovery combined with substantiated equilibrium fluid levels can be used to estimate an LNAPL transmissivity or at a minimum place an upper bound on recoverability.

### 5.2.7 *Special Considerations:*

5.2.7.1 Existence of a vertical gradient or tidal influences on the water table may limit the accuracy of the slug and/or baildown test, because the initial thickness in the well may be exaggerated (downward hydraulic gradient) or thin (upward hydraulic gradient), compared with static conditions. The relationships between LNAPL thickness, vertical gradient, and LNAPL recovery (recharge) rate may be complex and distort test data and the interpretation and are beyond the scope of this guide.

5.2.7.2 Periodic LNAPL removal events from wells have historically resulted in wells in a continual state of non-equilibrium and result in inaccurate equilibrium fluid levels. Equilibrium fluid level data is required for accurate drawdown calculations. LNAPL drawdown has historically been one of the primary variables inducing significant error to LNAPL baildown/slug tests.

5.2.7.3 The baildown test methodology provided minimizes filter pack recharge effects and is applicable where formation storativity effects are not significant in test results. Slug tests will exhibit larger borehole storage effects at a given well because the slug represents a relatively small percentage of the LNAPL volume in the well and filter pack. However, slug tests are more ideal for an instantaneous removal event, which is needed where steady state conditions are not well approximated due to formation storage effects. The advantage of baildown test methods with their larger removal volumes and stresses is the minimization of borehole storage induced errors. The advantage of slug test methods with their smaller, faster removal is the minimization of non-instantaneous effects. The quantified magnitude of these individual differences has not been widely studied.

5.2.7.4 The error associated with the recharge rate calculations is directly related to the error in gauged LNAPL thickness measurement. Smaller equilibrium thicknesses either result in fewer data points being collected or data points representing smaller changes in well recovery. Based on the accuracy of estimating the LNAPL/water and air/water interface with available interface probes, it is possible but generally not recommended to complete baildown tests at wells with a gauged LNAPL thickness of less than 0.5 ft (for 2-in. or 4-in. wells). Baildown/slug testing should not be attempted at wells with a measured thickness of LNAPL less than 0.2 ft.

### 5.3 *Manual LNAPL Skimming Tests:*

5.3.1 *Overview*—The manual LNAPL skimming test is conducted by removing LNAPL at a rate that maintains drawdown in the well until a consistent LNAPL recovery rate is achieved.

5.3.2 *Data Analysis*—This manual LNAPL skimming test field procedure is used in conjunction with a skimming test analytical method, to derive estimates of LNAPL transmissivity.

5.3.3 *Waste Disposal*—The manual LNAPL skimming test typically generates more waste than baildown/slug or tracer tests and less than recovery system methods.

5.3.4 *Aquifer Extent Represented*—The manual LNAPL skimming test provides an advantage over other tests in that; the longer period of time the test is performed, the larger the area of the formation it represents and the accuracy of recovery volume estimates increase, which are used in the calculation of LNAPL transmissivity.

5.3.5 *Capital Cost*—The capital cost of this method is relatively low as it can be completed at existing wells with LNAPL and typically requires similar equipment to baildown tests. If LNAPL transmissivity is sufficiently high then the use of a pump could incur additional costs. This method requires less capital cost than recovery system-based or tracer tests.

5.3.6 *Test Duration*—The length of the manual skimming tests is inversely related to the LNAPL transmissivity and directly related to the well diameter and LNAPL storativity in the formation. The manual skimming test duration is similar or longer in time frame compared with baildown/slug tests and a shorter timeframe than tracer tests.

5.3.7 LNAPL skimming tests may be completed at any well exhibiting a gauged LNAPL thickness. This test is especially useful for wells exhibiting a gauged thickness less than 0.5 ft because it allows the measurement of LNAPL volume above-ground. In addition, the error associated with estimating the recharged LNAPL volume at this initial gauged thickness can be more accurately estimated above-ground than in-situ.

5.3.8 Recovery system based-data transmissivity values may not compare identically with “instantaneous” and “point” transmissivity method results (for example, manual skimming test results) because of the differences in scale of evaluation between the two methods. However, increasing or decreasing trends in transmissivity will be seen in both recovery system-based data and manual skimming testing-based data.

5.3.9 Manual LNAPL skimming tests may be conducted in all types of aquifer materials.

5.3.10 Manual LNAPL skimming tests do not provide data to graphically estimate equilibrium fluid levels. Therefore, a good understanding of fluid level behavior (for example, hydrograph) is required to ensure initial fluid levels represent equilibrium conditions for accurate calculation of LNAPL drawdown.

### 5.4 *Recovery Data-Based Methods:*

5.4.1 This guide provides general procedures for deriving LNAPL transmissivities using data obtained from continuous operation of LNAPL skimmer pumps and/or other types of product recovery systems where aquifer conditions approach steady-state conditions. These recovery systems are designed to extract LNAPL, groundwater and/or formation air/vapor from a recovery well.

5.4.2 Because LNAPL transmissivity is being continually reduced through product recovery, steady-state conditions can be approached but not reached. Steady-state conditions are approximated when the maximum radius of influence (ROI) is reached for the current drawdown induced via the given technology.

5.4.3 The derivation of LNAPL transmissivity using recovery system data is based on the theory of radial fluid flow. Subsurface barriers (for example, building foundations) or significant heterogeneities can result in an under-estimation of LNAPL transmissivity when calculation methods involve the use of the radius of influence parameter. The equation for radial fluid flow will provide an average LNAPL transmissivity for all directions. However, it will under estimate LNAPL transmissivity in directions away from a subsurface barrier. Changes in soil type or lithologic properties affecting the hydraulic or pneumatic permeability of the formation and occurring within the recovery system radius of influence can affect the accuracy of the LNAPL transmissivity results. This effect is not significant when the fluid production ratio equations are used and the changes in subsurface conditions affect all extracted fluids and phases similarly. Accounting for such variability via site characterization data and accurate site conceptual models is necessary to achieve the most accurate results.

5.4.4 If the recovery system is operating consistently and the LCSM is well developed and understood, this method can provide high accuracy and repeatability of transmissivity calculations. However, use of recovery system-based data for estimation of LNAPL transmissivity requires a well-defined LCSM and frequent monitoring of recovery system operational parameters. LNAPL transmissivity values estimated from recovery data are representative of a region within an area of mobile LNAPL that is proportional to drawdown induced, recovery well spacing, and operational time. In other words, the area represented by an LNAPL transmissivity value is proportional to the drawdown induced, length of time run and distance between recovery well locations. As a result, recovery data transmissivity values may differ significantly from those obtained using “instantaneous” and “point” transmissivity method results (for example, baildown/slug test results) because of the differences in scale of evaluation between the methods. However, increasing or decreasing trends in transmissivity will be seen in both recovery system-based data and baildown testing-based data.

5.4.5 LNAPL transmissivity measurement by long-term operation of a skimming device or other LNAPL recovery system assumes continuous operation over the temporal interval of interest. Complete knowledge and maintenance of the system operation representing optimal conditions (for example, pump depth corresponds to the interval of mobile LNAPL or ensuring sufficient storage tank capacity) is necessary to obtaining representative LNAPL transmissivity values.

5.4.6 The LNAPL transmissivity values derived by recovery system data are based on fluid flow through a porous media and not karst environments or fractured rock. Attempts to apply this document to estimate LNAPL transmissivities in fractured rock, karst environments or other non-porous media may result in inaccurate LNAPL transmissivity values.

5.4.7 Fluctuations of water table elevation during the LNAPL recovery data collection period that significantly change the relationship between the groundwater/LNAPL interface (or the air/LNAPL interface) relative to the location of the recovery pump(s) can result in inaccurate transmissivity determinations. In addition, both horizontal and vertical pneumatic formation permeability must be determined when estimating the air radius of influence for determining transmissivity using LNAPL systems that incorporate vacuum-enhanced recovery.

5.4.8 The relative depths of the recovery well screen intervals, the groundwater/LNAPL interface, the air/LNAPL interface, and the depth of pump(s) intake(s) must be known. In addition, the configuration of the well construction, interfaces, and pump(s) intake(s) must be appropriate for the specific recovery system used to derive LNAPL transmissivity.

5.4.9 This guide provides analytical equations to calculate LNAPL transmissivity ( $T_n$ ) using recovery system-based data from four types of remediation technologies:

5.4.9.1 LNAPL only liquid removal (skimming).

5.4.9.2 Vacuum-enhanced LNAPL only liquid removal (vacuum-enhanced skimming).

5.4.9.3 Water-enhanced LNAPL removal (total fluids pumping, single or dual pump).

5.4.9.4 Water and vacuum-enhanced LNAPL removal (multi-phase fluid extraction [MPE]).

#### 5.5 *Tracer Test-Based Methods:*

5.5.1 *Overview*—This tracer test field procedure shall be utilized in conjunction with a tracer test analytical procedure to derive LNAPL flux and estimates of LNAPL transmissivity at any properly screened well exhibiting LNAPL thickness greater than 0.2 ft.

5.5.2 Tracer tests can be conducted under conditions of a natural or imposed gradient. Imposed gradient test can be conducted about active recovery wells. Natural gradient tests do not require fluid extraction.

5.5.3 *Test Duration*—Natural gradient tests are conducted over several weeks or months and, therefore, provide temporally-averaged and vertically-averaged transmissivity values. Imposed gradient tests can be conducted in period of hours to days.

5.5.4 *Waste Disposal*—LNAPL or water disposal is not required since the testing method does not generate water or LNAPL.

5.5.5 *Data Analysis*—Data reduction methods assume steady-state conditions, which can occur under natural or ambient conditions, or during steady-state recovery.

5.5.6 The LNAPL flux measurement is representative of a few feet outside the borehole. The LNAPL gradient is representative of the LNAPL surface within the well network density.

5.5.7 Although the flux measurement does not require a uniform flow field, it is combined with the LNAPL gradient to calculate an LNAPL transmissivity value. The LNAPL gradient estimates assume a uniform flow field between wells. Therefore, this method is more applicable to a uniform LNAPL flow field. Uniform LNAPL flow fields occur in homogenous conditions and can be induced by active recovery.

5.5.8 LNAPL tracer tests may be conducted in unconfined, perched and confined aquifer materials where the fluid levels are in equilibrium with the formation.

5.5.9 Inputs for data analysis (analytical procedure) should be known prior to the field testing to ensure that all appropriate dimensions and measurements are properly recorded.

5.5.10 *Specialized Equipment Needed*—A hydrophobic fluorescent tracer and a UV/VIS spectrometer with a down hole fiber optic cable are needed to make measurements of tracer concentration through time.

5.5.11 *Screening Factors for Test Method Selection:*

5.5.11.1 Using hydrophobic tracers to determine LNAPL transmissivity is a relatively new method, and it is expected that this method will become more refined in the future. The following methods have been proven at a laboratory scale (Smith et al, 2011) (4) and at seven field sites (Mahler et al, 2011) (5).

5.5.11.2 *Measurement of LNAPL Gradient*—The local LNAPL gradient must be measured or estimated as an input to the equation for LNAPL transmissivity using tracer tests.

## TEST METHODS

### 6. Short-Term Aquifer Testing-Based Methods

6.1 *Baildown/Slug Testing Field Methods*—This test method describes the field procedures involved in conducting an instantaneous LNAPL baildown/slug test. The LNAPL baildown/slug test method involves causing a sudden change in LNAPL head in a control well and measuring the fluid level response within that control well. Head change is induced by removing a known and measurable LNAPL volume from the control well.

6.1.1 *Apparatus*—This test method describes the types of equipment that can be used. Since there can be an infinite variety of testing conditions and because similar results can be achieved with different apparatus, engineering specifications for testing equipment are not discussed in this document. This test method specifies the results to be achieved by the equipment to satisfy the requirements of this guide.

6.1.1.1 *LNAPL Displacement Equipment*—Because a variety of equipment can be used to induce a change in LNAPL head, this method will not provide engineering specifications of the exact means in which head is changed, but will rather identify how common types of equipment can affect the final results. Single slug displacement or removal methods such as solid slugs or bailers, respectively, will provide a more instantaneous change in LNAPL head. This is useful at well locations exhibiting higher LNAPL transmissivities. The use of solid slugs is acceptable since their volume can easily be measured. However use of equipment such as peristaltic pumps to remove the entire volume of LNAPL in the well casing and borehole will result in minimizing filter pack recharge effects. It is strongly recommended to use equipment that can remove LNAPL from the well and allow the use of graduated containers to measure the total volume within 10 %. Vacuum trucks at best have a detection limit of 5 gal and an accuracy of 1 gal above 5 gal (19 L). Down-hole non-intrinsically safe electrical pumps need to remain submerged below the air/LNAPL interface to prevent explosions; therefore down-hole electrical pumps used to evacuate LNAPL to zero thickness, for example, are not acceptable practices.

6.1.1.2 In some cases the LNAPL removal equipment available will not be able to remove LNAPL at a high enough rate to completely purge the control well. If this occurs during the test, a slug test or any of the other LNAPL transmissivity test methods discussed in this document can be applied.

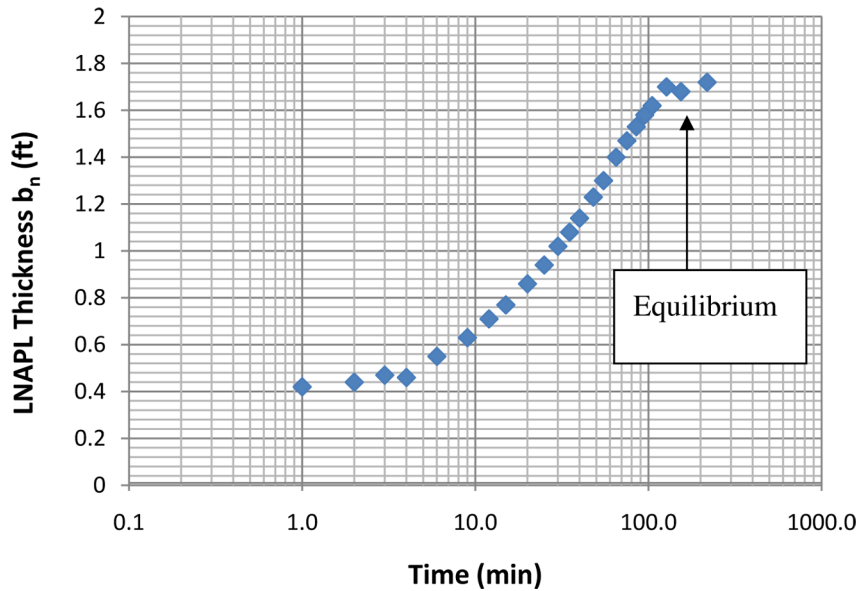
6.1.1.3 *Fluid Level Measurement Equipment*—Typically, the air/LNAPL and LNAPL/water interfaces will be gauged using an interface probe. Currently the most precise available interface probes utilize optical and electrical resistivity technologies. Additionally, current technology allows for probes to be relatively small (5/8-in.) in diameter. The optical and electrical resistivity type interface probes increase the ability to measure fluid interfaces to typical accuracies from 0.01 to 0.02 ft (0.3 to 0.6 cm). The small probe diameter causes less displacement to fluids in the well. When the recovery of LNAPL occurs rapidly (that is, less than 1 h), tests can be conducted with an intrinsically safe pressure transducer, where the pressure transducer is set near the bottom of the well (in the water phase). Then the field staff only will be required to measure the depth to the air/LNAPL interface following removal of LNAPL. By only measuring the air/LNAPL interface less disturbance will be introduced to the well during recovery since the probe does not need to penetrate the fluid column to measure the LNAPL/water interface. Two pressure transducers can still be used, where one transducer is placed in the water phase and a second within the LNAPL phase; however, they are not necessary.

6.1.1.4 *Time Piece*—Used to record the elapsed time of the test.

6.1.1.5 *Graduated Container*—A container for water and LNAPL collection that is graduated to measure within 10 % of total estimated recovery volume (unit conversion: 1 gallon = 3.825 litres = 3,825 millilitres (mL) = 0.134 cubic feet). For example, a container that can measure 0.1 gal (~400 mL) intervals for an expected 1 gal (~4000 mL) of recovered product, or a container that can measure 1 gal (~4000 mL) intervals for an expected 10 gal (40 000 mL) of recovered LNAPL.

6.1.1.6 *Decontamination Equipment*—Typically, LNAPL in a well can foul measuring devices and should be cleaned with an appropriate cleaning agent. If multiple wells are tested, equipment should be cleaned of well fluids between testing separate wells.

6.1.1.7 *Test Forms*—Test forms should be used to record the parameters listed in 6.1.2 and 6.1.3 (that is, Conditioning & Procedure). Semi-log graph paper should be used to plot data during the test in order to understand when equilibrium is reached and the test is completed. Fig. 1 provides an example of LNAPL thickness reaching equilibrium during a test.



Graph illustrating how the frequency of gauging data should be based on consistent changes in LNAPL thickness rather than time, and demonstrating the attainment of recharge equilibrium conditions.

FIG. 1 Gauging Data Graph

6.1.2 Conditioning:

6.1.2.1 Pre-Test Well Information—The following well construction information needs to be obtained prior to initiating the baildown tests:

- (1) Borehole diameter of well to be tested (feet).
- (2) Casing and screen diameter (inches).
- (3) Top of screen relative to top of casing (feet).
- (4) Bottom of screen interval relative to top of casing (feet).
- (5) Total well depth (feet).
- (6) Verify interval that the well is screened over the formation thickness.

6.1.2.2 Baildown/slug tests are used to evaluate the transmissivity of LNAPL in the aquifer. It is recommended that the LNAPL existing within the well and borehole need to be occasionally evacuated prior to the baildown test in order for the LNAPL to stay in communication with the formation. The maximum lag time between removal events is two years.

6.1.2.3 Prior to the test, the well being tested should be fully recharged; this will ensure the starting LNAPL thickness, LNAPL head, and potentiometric surface head are all representative of equilibrium formation conditions.

6.1.3 Pre-Test Procedure:

6.1.3.1 Measuring Pre-Test Fluid Levels—Measure the fluid levels in the well before the test for a period longer than the time it will take the well to recover in order to ensure equilibrium fluid levels are known and to calculate the effective well volume. This should be established during the initial evacuation of LNAPL from the well prior to the test (see 6.1.2.2).

6.1.3.2 Errors associated with erroneously assumed equilibrium fluid levels will reduce test accuracy and may invalidate the test.

6.1.3.3 Plan on gauging the well until complete equilibration occurs (Fig. 1) for wells where recovery behavior is not well understood or the pretest gauging data is realized not to represent equilibrium conditions.

6.1.3.4 The scope of work should plan for gauging to potentially be conducted over days or even weeks.

6.1.3.5 For unconfined conditions, the filter pack typically holds the majority of the stored LNAPL volume within the effective well radius. Partial displacement or removal of the LNAPL will result in the test being dominated by filter pack recharge.

6.1.3.6 Filter pack effects can be reduced through larger displacement volumes for slug tests or the complete removal of LNAPL in the filter pack and casing during baildown tests. The following equations can be used to approximate the volume of LNAPL within the well casing and borehole.

$$V_b = S_y b_b \pi (r_b^2 - r_c^2) \tag{1}$$

$$V_c = b_r \pi r_c^2 \tag{2}$$

$$V_t = V_c + V_b \quad (V_c = b_c \pi r_c^2) \tag{3}$$

$$V_t = V_c + V_b \tag{3}$$



where:

- $V_t$  = total effective borehole LNAPL volume ( $L^3$ ),
- $V_b$  = volume of LNAPL in the borehole ( $L^3$ ),
- $V_c$  = volume of LNAPL in the casing ( $L^3$ ),
- $b_b$  = LNAPL thickness existing within borehole (L),
- $b_n$  = gauged LNAPL thickness (L),
- $r_c$  = well casing radius (L),
- $r_b$  = well borehole radius (L), and
- $S_{yf}$  = specific yield or storage coefficient of well filter pack.

6.1.3.7 To account for borehole porosity and LNAPL saturation, a storage coefficient needs to be estimated. Empirical data suggest that 0.175 to 0.190 is a good value for this parameter at any site. If viscosity of the LNAPL is known, an alternate method of estimating storage coefficient that has been tested between viscosities of 0.7 and 2 centipoises can be derived by using Eq 4 (Lundy, 2005) (6). Using Eq 2 combined with viscosities of 0.5 cp and 5 cp results in a range in storativity of 0.23 to 0.13 where the geometric mean is 0.175. The empirical data and Eq 4 suggest an average value of 0.175 and the range should not vary by more than a factor of 50 %.

$$S_{yf} = -0.0418 \ln(\mu_n) + 0.2007 \quad (4)$$

where:

- $S_{yf}$  = filter pack LNAPL specific yield, and
- $\mu_n$  = dynamic viscosity of LNAPL (M/Lt).

6.1.3.8 Well construction data will need to be reviewed to evaluate if the filter pack exists over the entire gauged interval of LNAPL. If the well screen and filter pack do not exist across the entire gauged thickness, then the filter pack thickness, used in Eq 1 will have to be reduced from the gauged thickness value.

#### 6.1.4 Test Procedure:

6.1.4.1 Where the LNAPL transmissivity or recharge behavior is not well known, plan to start the baildown portion of the test early in the work day and on a day when you will be able to return frequently to the well. This will ensure that sufficient measurement frequency can be obtained within the first 8 h of the test.

6.1.4.2 Remove the known LNAPL volume up to a maximum as calculated using Eq 3. Smaller removal volumes will exhibit larger filter pack recharge effects and be more instantaneous. Larger removal volumes will minimize filter pack recharge effects although may not be instantaneous relative to the test duration.

6.1.4.3 Baildown/slug test LNAPL head change rate must be induced in a time that is  $1/100^{\text{th}}$  or less of the total test duration, in order to approximate instantaneous head change. If full removal of LNAPL from filter pack and well casing requires longer time and an analysis method that relies on instantaneous withdrawal is being used (for example, Cooper-Jacob), then a slug method or alternative method should be used.

6.1.4.4 Instantaneous removal or slug introduction is relative to total length of test. For example 15 min of purging can be considered instantaneous if the length of the test is 1 day or more. Non-instantaneous removals can potentially be corrected in conjunction with steady state based slug test solutions (that is, Bouwer-Rice), which is discussed in Section 8. However, efforts should be made to complete the slug/fluid removal in as short of a timeframe as is practical so that removal approximates an ‘instantaneous’ head change.

6.1.4.5 Record the start and finish time of LNAPL removal. Record the total volume of LNAPL and water removed or slug length and volume. If large volumes (over 5 gal/ 19 L) of LNAPL are removed or removal occurs for a relatively long period of time (over 30 min), record several interim measurements of volume removed and time.

6.1.4.6 Baildown tests conducted in wells containing low viscosity LNAPL (that is, <1 centipoise) generally require 30 min or less for purging, while higher viscosity LNAPL (that is, >2 centipoises) can require a few hours. This is acceptable if the baildown test takes days to complete, the time for removal in this case would approximate instantaneous head change relative to the test duration.

6.1.4.7 Following LNAPL removal, begin recording the time and measuring the depth to the air/LNAPL and LNAPL/water interfaces. Depth to the air/LNAPL interface should be decreasing (or remaining the same). The gauged LNAPL thickness should be increasing. Re-measure and report any readings that do not match these trends. Record notes regarding the methodology taken to confirm or revise anomalous data.

6.1.4.8 The depth to the air/LNAPL interface could decrease if the overall groundwater elevation at the site is dropping. To verify whether the water-table elevation is dropping, a nearby control well can be measured prior to and during testing.

6.1.4.9 The best practice for gauging fluid levels during the baildown test is to collect a measurement at a maximum frequency of every 0.05 to 0.1 ft (1.5 cm) change in LNAPL thickness from static. A minimum change in thickness that is reasonable for use in data analysis is 0.05 to 0.1 ft (1.5 cm) of change in thickness.

6.1.4.10 The best practice also consists of gauging fluid levels at a minimum frequency corresponding to a change in thickness that represents 5 % of the equilibrium gauged LNAPL thickness or 0.05 ft (that is, 1.5 cm), whichever is less. This methodology is conducted for the first 100 min of recovery. The remainder of the test can be completed by gauging measurements on a frequency

corresponding to a change of 5 to 10 % of the equilibrium thickness. This methodology will result in data being collected on a logarithmic timescale which is appropriate for data analysis. Because the recovery rate will drop as the well recovers, measurements can be collected on a logarithmic time scale (that is, at some point, the well may only have to be gauged weekly or monthly).

6.1.4.11 The minimum practical time for measuring fluid levels with a single interface probe is at 1-minute intervals since two interfaces need to be gauged.

6.1.4.12 After the first 100 min of a test, the data should be reviewed and a schedule should be prepared by the field staff based on the collected data set.

6.1.4.13 Plotting the recovered LNAPL thickness versus the log of time will help to forecast future events and help to provide data to support the conclusion of the test (see Fig. 1).

6.1.4.14 The time point representing the next change in thickness of 5 to 10 % of the static thickness or 0.05 ft (1.5 cm), whichever is less, can then be forecast based on the graph. For example, if over the initial 100 min the well has recovered less than 5 % of its initial thickness, the next measurement would be at least an additional 100 min from the current time.

6.1.4.15 In order to ensure that equilibrium fluid levels are understood and can be used to calculate LNAPL drawdown, gauging data representing consistent equilibrium fluid levels must exist for a period that is equal to the length of a completed test. This data can represent fluid levels prior to start of test or following test.

6.1.4.16 If the initial gauging data is insufficient to ensure equilibrium fluid levels (for example, one data point immediately before the test) then plan on obtaining test measurements until the LNAPL thickness has stabilized to its static thickness. This will provide the most complete insight into the LNAPL distribution in the formation and confirm the initial equilibrium fluid levels. A typical indication of LNAPL thickness stabilizing is when the LNAPL thickness reaches a plateau for approximately one quarter to one half of a log cycle. This should be documented with 3 measurements over that period (see Fig. 1).

6.1.4.17 The actual time and date of each measurement should be recorded, particularly when it may deviate from the initial schedule. If the change in LNAPL thickness between each event is less than the percentages listed above, then the frequency of measurements may be decreased. However, if the change in LNAPL thickness is greater than the percentages listed above, then measurement frequency should be increased.

NOTE 1—During the test, accurate measurements of the depths to LNAPL and water are critical. Every effort should be made to ensure that these readings are consistent and reliable. It is important to evaluate the data as it is collected and confirm any apparent erratic gauging data. Confirmation readings should be supported with comments on the field form. LNAPL thickness should ideally be increasing (or remaining the same) from one measurement to the next, not decreasing.

6.1.4.18 In some cases, fluid levels may change more rapidly than can be measured manually. Under these circumstances a LNAPL baildown test can be conducted using a pressure transducer. Conduct a baildown test with a pressure transducer with the following modifications from the procedure described above:

(1) Synchronize the transducer clock with the time piece used to collect gauging measurements. Next, set the measurement schedule to collect a minimum of 50 readings over the estimated test duration. Ensure that the pressure transducer has the appropriate battery life and is calibrated.

(2) Lower the pressure transducer to the bottom of the well and gauge the well until the fluid levels have stabilized again.

(3) Following stabilization, record and compare the gauged measurements to the reading on the pressure transducer to ensure it is working properly.

(4) Start and run the test as described above in 6.1.4 except that the LNAPL/water interface does not need to be gauged during the test. The air/LNAPL and LNAPL/water interfaces should be gauged prior to initiating the test and following completion of the test for use in calibration of the pressure transducer depth.

(5) Gauge the air/LNAPL interface as frequently as possible throughout the test.

(6) Review manufacturer specifications to understand the accuracy and precision of transducer data collected and ensure the data to be potentially used is not limited by equipment specifications.

(7) *Post-Test Procedure*—Conduct preliminary analysis of data before leaving the field and evaluate the test regarding the criteria given in this test method. The test data should be analogous to the trend shown in Fig. 1. The drawdown and time magnitudes are expected to vary but the overall trend on a semi-log plot should be similar.

#### 6.1.5 Report:

6.1.5.1 Include the information listed below in the report of the field procedure:

(1) Well identification.

(2) Well construction (well depth, filter pack and screen interval, inner casing, screen, and borehole diameter).

(3) Date and time of initial fluid gauging data.

(4) Initial fluid levels.

(5) Field staff.

(6) Known LNAPL characteristics (for example, LNAPL density and product type).

(7) Well Identification (ID), casing diameter and other known well information.

(8) Method of LNAPL withdrawal removal notes.

(9) Calculated well volume.

- (10) Establish and record the measurement point from which all measurements of fluid levels were made.
- (11) All gauging data collected prior to and during the test.
- (12) Start and stop date and time of LNAPL purge event or slug withdrawal.
- (13) Volume of LNAPL and water removed during purge or slug withdrawal event.
- (14) If the fluid levels are measured with a pressure transducer, report the model type of the pressure transducer used, recorded pressure versus time data, and the data used to convert pressure data to fluid depth (that is, calibration fluid level data and the fluid density).

#### 6.1.6 Precision and Bias:

6.1.6.1 *Precision*—It is not practical to specify the precision of this specific test method because the response of aquifer systems during testing is dependent upon ambient system stresses.

6.1.6.2 *Bias*—No statement can be made about bias because no true reference values exist.

6.2 *Manual Skimming Field Methods*—This test method describes the field procedures involved in conducting a LNAPL manual skimming test. This test consists of the removal of LNAPL from the well casing and borehole on a repeated basis, without allowing more than approximately 25 % of recharge to occur in between product removal events. The rate of removal is therefore dependent on well recharge behavior. The key criterion is that greater than 75 % of the maximum skimming drawdown must be consistently induced. Purging is completed until the recovery rate stabilizes. The LNAPL discharge or recovery rate for each LNAPL removal step is calculated. The recovery volume and gauging data, along with the volume of LNAPL removed, can be used to estimate the LNAPL transmissivity and recoverability. LNAPL transmissivity is calculated from the stabilized LNAPL discharge data. This test ranges from a few hours for wells exhibiting higher LNAPL transmissivities to in excess of weeks for wells exhibiting lower LNAPL transmissivities. The manual skimming test can be performed on most wells that contain LNAPL.

6.2.1 *Apparatus*—This section describes the types of equipment that can be used. Since there are an infinite variety of testing conditions and because similar results can be achieved with different apparatus, engineering specifications for apparatus are not discussed in this guide. This test method specifies the results to be achieved by the equipment to satisfy the requirements of this guide.

6.2.1.1 *LNAPL Removal Equipment*—Because a variety of equipment can be used to induce a change in LNAPL head, this method will not provide engineering specifications of the exact means in which head is changed, but rather identify how common types of equipment can affect the final results.

6.2.1.2 *Fluid Level Measurement Equipment*—Typically, the air/LNAPL and LNAPL/water interfaces will be gauged using an interface probe. Currently the most precise available interface probes utilize optical and electrical resistivity technologies. Additionally, current technology allows for probes to be relatively small ( $\frac{5}{8}$ -in.) in diameter. The optical and electrical resistivity type interface probes increase the ability to measure fluid interfaces to typical accuracies from 0.01 to 0.02 ft (0.3 to 0.6 cm) and the small probe diameter causes little displacement to fluids in the well.

6.2.1.3 *Time Piece*—Used to record the elapsed time of the test.

6.2.1.4 *Graduated Container*—A container for water and LNAPL collection that is graduated to measure within 10 % of total estimated recovery volume between fluids removal events. For example, a container that can measure 0.1 gal intervals for an expected 1 gal of recovered product, or a container that can measure 1 gal intervals for an expected 10 gal of recovered LNAPL.

(1) *Decontamination Equipment*—Typically, LNAPL in a well can foul measuring devices and should be cleaned with an appropriate cleaning agent. If multiple wells are tested, equipment should be cleaned of well fluids between testing separate wells.

(2) *Test Forms*—Test forms should be used to record the parameters listed in 6.3.2 and 6.3.4 (that is, Conditioning and Procedure).

#### 6.2.2 Conditioning:

6.2.2.1 *Pre-Test Well Information*—The following well construction information needs to be obtained prior to initiating the manual skimming tests:

- (1) Borehole diameter of well to be tested.
- (2) Casing and screen diameter.
- (3) Top of screen relative to top of casing.
- (4) Bottom of screen interval relative to top of casing.
- (5) Total well depth.
- (6) Verify interval that the well is screened over the formation thickness.

6.2.2.2 Manual skimming tests are used to evaluate the transmissivity of LNAPL in the formation. It is recommended that the LNAPL existing within the well and borehole be occasionally evacuated prior to the manual skimming test in order for the LNAPL to stay in communication with the formation. Prior to the test, the well being tested must be fully recharged. This will ensure the starting fluid levels surface head are all representative of equilibrium formation conditions.

6.2.2.3 *Measuring Pre-Test Fluid Levels*—Measure the fluid levels in the well before beginning the test to determine the pre-test fluid levels.

6.2.2.4 The pre-test fluid levels need to represent equilibrium conditions in order for the accurate calculation of LNAPL drawdown.

6.2.2.5 No other pre test procedures are required.

### 6.2.3 Test Procedure:

6.2.3.1 Because of the LNAPL extraction and measurement frequency needed over the first 8 h, plan to start the manual skimming portion of the test early in the work day and on a day when you will be able to return frequently to the well.

6.2.3.2 The test consists of the following four steps:

- (1) Initial gauging of fluid levels.
- (2) Purging the well and borehole of the LNAPL.
- (3) Periodically returning to the well to:
  - (a) Gauge fluid levels.
  - (b) Purge any recovered LNAPL.
  - (c) Gauge fluid levels following purging.
- (4) Data analysis.

6.2.3.3 To start the test, remove LNAPL until further LNAPL removal is not possible while minimizing the groundwater recovered. Record the start and finish time of LNAPL removal. Record the total volume of LNAPL and water removed. If large volumes (over 5 gal/19 L) of LNAPL are removed or removal occurs over a long period of time (over 30 min), record several interim measurements of volume removed and time. Try not to disturb the static potentiometric surface level during LNAPL removal. Methods of LNAPL removal may include bailers, peristaltic pumps, vacuum truck removal and other skimmer pumps as long as the volumes can accurately be measured.

6.2.3.4 Remove LNAPL until the product is no longer being removed.

6.2.3.5 Begin recording the date/time and measured depths to the air/LNAPL interface and LNAPL/water interface immediately after removing the LNAPL. Once the well has recovered  $\frac{1}{4}$  of the initial thickness, re-purge the LNAPL in the well. Record the start and stop time of purging and the gauging data before and after each purging event. The time elapsed between the completion of the initial purge and the start time of the following purging event will provide an estimated return time for the next event.

6.2.3.6 A best practice of the test is to gauge and purge the well before the well recovers  $\frac{1}{4}$  of the original thickness. The following frequencies are provided as an initial recommendation and should be adjusted based on field observations:

- (1) First hour: every 10 min (6 measurements).
- (2) 2 h to 4 h: every 30 min (4 measurements).
- (3) 4 h till end of first day (1 measurement).
- (4) Second day: 2 to 3 times.
- (5) Subsequent days: At least twice per day until the LNAPL discharge rate has stabilized.

6.2.3.7 The actual time and date of each measurement should be recorded, especially when it may deviate from the initial schedule. The calculated recharge will typically start out high and decrease until it reaches a constant value. The test should continue until the calculated recharge into the well stabilizes. At some locations this may take a week. Following the first 4 h and the first day of testing, the data should be reviewed to improve the timeline with which gauging and purging events will be conducted. If previous knowledge of the recovery behavior for a given well is available, the provided timescale can be modified based on those data.

6.2.3.8 If the well is recovering less than  $\frac{1}{4}$  of its initial thickness between each measurement, the frequency of measurements may likely be decreased. However, if the LNAPL thickness recovers to more than  $\frac{1}{4}$  of the initial thickness, frequency of gauging and purging should be increased.

6.2.3.9 The maximum practical measurement and purge frequency is 5 min for a single field staff due to the constraints of gauging, fluid removal activities, recovered fluid volume removal measurement and documentation. It is not necessary to increase the frequency beyond this. If the well recovers too fast for these conditions to be met then an alternate testing methodology should be employed, such as a pilot test with an automated skimming pump in conjunction with the recovery system-based field and analysis method.

6.2.3.10 The test is complete when three or four consecutive discharge rates are within 25 % of each other and no consistently decreasing trend is observed.

6.2.3.11 During the test, accurate measurements of the recovered volume and depths to air/LNAPL and LNAPL/water interfaces are critical. Every effort should be made to ensure that these readings are consistent and reliable. Re-measure and document any readings that seem anomalous and then make notes regarding the methodology taken to confirm or revise anomalous data.

6.2.3.12 Ensure that the bucket/container used for measuring recovered volume spans the volumes being recovered each period. Typically the removal volumes for each purging event will be less than  $\frac{1}{2}$  gal. A 5-gal bucket is not precise enough for measuring the recovered volume following the initial removal. See section 6.3.1 (Apparatus).

6.2.3.13 *Post-Test Procedure*—Make a preliminary analysis of the data before leaving the field and evaluate the test regarding the criteria given in this test method to determine if the test should be rerun.

6.2.4 *Report*—Include the information listed below in the report of the field procedure:

- 6.2.4.1 Well identification.
- 6.2.4.2 Well construction (well depth, filter pack and screen interval, inner casing, screen, and borehole diameter).
- 6.2.4.3 Date and time of initial fluid gauging data.
- 6.2.4.4 Initial fluid levels.

- 6.2.4.5 Field staff.
- 6.2.4.6 Known LNAPL characteristics (for example, LNAPL density and product type).
- 6.2.4.7 Casing diameter and other known well information.
- 6.2.4.8 Method of LNAPL withdrawal removal notes.
- 6.2.4.9 Calculated well volume.
- 6.2.4.10 Establish and record the measurement point from which all measurements of fluid levels were made.
- 6.2.4.11 All gauging data collected prior to the test.
- 6.2.4.12 Date and time of test start.
- 6.2.4.13 Depth to fluid levels before and after each purge event.
- 6.2.4.14 Start and stop date and time of each gauging and purge event.
- 6.2.4.15 Volume of LNAPL and water removed during each purge event.

#### 6.2.5 *Precision and Bias:*

6.2.5.1 *Precision*—It is not practical to specify the precision of this test method because the response of aquifer systems during LNAPL manual skimming tests is dependent upon ambient system stresses.

6.2.5.2 *Bias*—No statement can be made about bias because no true reference values exist.

6.3 *Long-term Recovery System Method*—This test method describes the field procedures involved with collecting product recovery system data for the purposes of estimating LNAPL transmissivity under steady state conditions. LNAPL transmissivity calculations for recovery systems are based on the achieved LNAPL recovery rate versus drawdown induced. Therefore, this section is focused on methods used to estimate LNAPL recovery rate for all systems and specific methods used to estimate drawdown induced by the specific technologies.

6.3.1 *Apparatus*—The equipment consists of storage containers which allow for measurement of fluid volumes recovered over time, flow meters for individual and/or total fluids and instantaneous flow measurements. In addition, equipment used to measure pneumatic and/or hydraulic head at individual well locations and/or for the system as a whole. Because there are an infinite number of recovery system designs, this guide does not specify the equipment to be used, but rather the equipment used must meet the data objectives set forth in the guide.

6.3.2 *Conditioning*—All recovery wells where LNAPL transmissivity is estimated should be properly developed in order to ensure non-linear head losses are minimized. Maintenance schedules should consist of development following well installation, as well as, periodic rehabilitation to prevent deterioration of the well performance to scaling and biofouling. One time well development is not sufficient for most active recovery systems that run longer than five years.

6.3.3 Verify interval that the well is screened over the formation thickness.

6.3.4 *Procedure*—Because the procedure for measurement is dependent on system design and equipment, it is not feasible to specify the measurement procedure for each parameter in this method. Field forms for individual technologies are provided in [Annex A1](#) and identify the minimum field parameters, as well as, where additional measurements would provide multiple lines of evidence for LNAPL transmissivity calculations.

6.3.5 *Report*—Field forms included in [Annex A1](#) identify the reporting requirements for individual technologies. The report consists of measured input values and justification for each parameter measured on the field forms and variables provided in [Tables A2.5-A2.8](#).

#### 6.3.6 *Precision and Bias:*

6.3.6.1 *Precision*—It is not practical to specify the precision of this test method because the response of aquifer systems during LNAPL recovery is dependent upon ambient system stresses.

6.3.6.2 *Bias*—No statement can be made about bias because no true reference values exist.

## 7. Tracer Test Field Methods

7.1 This test method describes field procedures for conducting LNAPL tracer tests.

7.2 *Apparatus*—This section describes the types of equipment that can be used. Because of the infinite variety of testing conditions, engineering specifications for apparatus are not provided. This test method specifies the results to be achieved by the equipment to satisfy the requirements of this guide.

7.2.1 *Spectrometer/Fiber Optic Cable and Computer*—To date, a temperature regulated, visible light spectrometer has been used to measure the tracer presence and relative concentration in the LNAPL. The spectrometer consists of a light source to induce fluorescence in the tracer. The output from the spectrometer is converted to a digital signal and transmitted to a laptop computer, Program Logic Controller (PLC), or similar device to store and display the measured values.

7.2.2 The fiber optic cable used to date consists of multiple fibers. A portion of the fibers within the cable are used to transmit the excitation light source to the tracer in the LNAPL in the well, and others return the resulting fluorescence response back to the spectrometer.

7.2.3 The spectrum of excitation and measured fluorescence response is key as fiber optic cables tend will attenuate signals too rapidly to be of use if they are not appropriate for the excitation and fluorescence spectrums of intent. Typically, attenuation occurs more rapidly for shorter wavelengths (for example, less than 290 nm).

7.2.4 To date, a laptop computer equipped with software to communicate with the spectrometer has been used to control the spectrometer and display a graph of the spectrum (intensity versus wavelength) and record output.

7.2.5 *Tracer:*

7.2.5.1 The tracer used to date is BSL 715.<sup>4</sup> This tracer is a concentrated liquid hydrocarbon which has unique fluorescence peaks at 545 and 580 nm when excited at 470 nm. It fluoresces yellow under ultraviolet light and is used in the automotive industry to detect oil leaks. This tracer is specifically listed (Sale et. al., 2008) (7) because it has undergone testing to ensure that it will not decrease in concentration over time in the well based on non-flow related mechanisms such as dissolution, volatilization, or sorption. Any new tracer used to estimate LNAPL transmissivity will need to be tested to ensure that it acts as a conservative tracer.

7.2.5.2 The tracer has the following characteristics:

- (1) It is detectable in LNAPL at low concentrations (less than 1 ppm in Soltrol 220, Woodlands, Texas).
- (2) It is insoluble in water.
- (3) It has no significant effect (at application concentrations) on the physical properties of LNAPL.
- (4) It fluoresces at a wavelength where most LNAPLs have low background fluorescence.
- (5) It has low toxicity relative to constituents present in most LNAPLs.

7.2.6 *In-Well Calibration Standards*—In-well calibration standards are used to correct for potential non-tracer related fluorescence from the LNAPL induced by the 470 nm light source. Small diameter pipes are inserted within the test well to occlude a volume of LNAPL without tracer and a volume of LNAPL with the initial tracer concentration. A small-diameter pipe is inserted into the test well, through the LNAPL before tracer is added, for Eq 5 this well is called  $C_0$ . Tracer is then added and mixed with the LNAPL. A second pipe is then inserted into the test well through the LNAPL. This well is called  $C_{100}$  in Eq 5. The two pipes, one without tracer and one with the initial tracer concentration allow for in-well spectrometer calibrations to be made with each tracer concentration measurement. Measurements of remaining tracer in the test wells at the end of each measurement period are corrected using the calibrations assuming a linear relationship between fluorescence and intensity can be calculated as:

$$\frac{C_{T_{t+\Delta t}}}{C_{T_t}} = \frac{\frac{I_{test\_well,t+\Delta t} - I_{Cal\_well,C_{0,t+\Delta t}}}{I_{Cal\_well,C_{100,t+\Delta t}} - I_{Cal\_well,C_{0,t+\Delta t}}}}{\frac{I_{test\_well,t} - I_{Cal\_well,C_{0,t}}}{I_{Cal\_well,C_{100,t}} - I_{Cal\_well,C_{0,t}}}} \quad (5)$$

where:

- $C_{T_{t+\Delta t}}$  = concentration of tracer mass remaining at time of measurement ( $M/L^3$ ),
- $C_{T_t}$  = concentration of initial tracer mass ( $M/L^3$ ),
- $I_{test\_well,t+\Delta t}$  = fluorescence intensity in test well at time of measurement (unitless),
- $I_{Cal\_well,C_{0,t+\Delta t}}$  = fluorescence intensity in  $C_0$  calibration well at time of measurement (unitless),
- $I_{Cal\_well,C_{100,t+\Delta t}}$  = fluorescence intensity in  $C_{100}$  well at time of measurement (unitless),
- $I_{test\_well,t}$  = initial fluorescence intensity in test well (unitless),
- $I_{Cal\_well,C_{0,t}}$  = initial fluorescence intensity in  $C_0$  well (unitless), and
- $I_{Cal\_well,C_{100,t}}$  = initial fluorescence intensity in  $C_{100}$  well (unitless).

7.2.7 *Interface Probe*—An interface probe should be used to record LNAPL thickness in the test well each time tracer concentration is measured. Additionally, the interface probe is used to measure the LNAPL and hydraulic gradients occurring throughout the test duration.

7.2.8 *Pressure Transducer*—The use of a pressure transducer should be considered for sites where the fluid levels are expected to vary the LNAPL gradient over the length of the test and where site gauging events are expected to be infrequent.

7.2.9 *Decontamination Equipment*—LNAPL must be cleaned from the fiber optic cable between calibration standard measurements and test well measurements to ensure that there is no transfer of tracer dye between standards or test well. A cleaning agent such as detergent or isopropyl alcohol should be used to clean the fiber optic cable between readings. Further information on decontamination can be found in Practice D5088. Additionally, LNAPL can foul other fluid-level measurement devices. These devices should be cleaned with an appropriate cleaning agent. If multiple wells are tested, equipment should be cleaned of fluids between testing of separate wells.

7.3 *Conditioning:*

7.3.1 Collect representative LNAPL samples from monitoring wells to be used for testing prior to initiating the LNAPL tracer tests. Measure and record fluorescence of the LNAPL sample using the spectrometer. Add tracer to the LNAPL sample, thoroughly mix the sample, and measure and record fluorescence of the sample. Repeat the preceding step adding increasing amounts of tracer to evaluate the dose-response relationship between tracer concentration and fluorescence intensity. Initial tracer concentrations should be determined for each LNAPL type based on the following guidelines.

7.3.2 Review well construction logs to ensure the current LNAPL thickness is within the well screened interval.

<sup>4</sup> The sole source of supply of the apparatus known to the committee at this time is Bright Solutions Inc., Troy, Michigan. If you are aware of alternative suppliers, please provide this information to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,<sup>1</sup> which you may attend.