
**Plain bearings — Hydrostatic plain
journal bearings with drainage
grooves under steady-state
conditions —**

Part 1:

**Calculation of oil-lubricated plain
journal bearings with drainage
grooves**

*Paliers lisses — Paliers lisses radiaux hydrostatiques avec rainures
d'écoulement fonctionnant en régime stationnaire —*

*Partie 1: Calcul pour la lubrification des paliers lisses radiaux avec
rainures d'écoulement*



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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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The committee responsible for this document is ISO/TC 123, *Plain bearings*, Subcommittee SC 8, *Calculation methods for plain bearings and their applications*.

This third edition cancels and replaces the second edition (ISO 12167-1:2016), which has been technically revised.

The main changes are as follows:

- subclause titles have been added;
- symbols have been corrected and added in [Table 1](#);
- calculation values in [Annex B](#) have been corrected;
- adjustments have been made according to ISO/IEC Directives, Part 2:2021;
- typographical errors have been corrected.

A list of all parts in the ISO 12167 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

Hydrostatic bearings use external lubrication to support pressure on the bearings; thus, they are less prone to wear and tear, run quietly, and have a wide useable speed, as well as high stiffness and damping capacity. These properties also demonstrate the special importance of plain journal bearings in different fields of application such as in machine tools.

Basic calculations described in this document may be applied to bearings with different numbers of recesses and different width/diameter ratios for identical recess geometry.

Oil is fed to each bearing recess by means of a common pump with a constant pumping pressure (system $p_{en} = \text{constant}$) and through preceding linear restrictors, e.g. capillaries.

In this document, only bearings with oil drainage grooves between the recesses are taken into account. As compared to bearings without oil drainage grooves, this type needs higher power with the same stiffness behaviour.

Equivalent calculation procedures that enable operating conditions to be estimated and checked against acceptable conditions may also be used.

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Plain bearings — Hydrostatic plain journal bearings with drainage grooves under steady-state conditions —

Part 1:

Calculation of oil-lubricated plain journal bearings with drainage grooves

1 Scope

This document specifies the calculation procedures to calculate and assess a given bearing design, as well as to design a bearing as a function of some optional parameters. This document contains the design of the required lubrication system including the calculation of the restrictor data.

This document applies to hydrostatic plain journal bearings under steady-state conditions.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 12167-2:2021, *Plain bearings — Hydrostatic plain journal bearings with drainage grooves under steady-state conditions — Part 2: Characteristic values for the calculation of oil-lubricated plain journal bearings with drainage grooves*

3 Terms and definitions

No terms and definitions are listed in this document.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

4 Symbols

Symbols and units are defined in [Table 1](#).

Table 1 — Symbols

Symbol	Term	Unit
a	Inertia factor	1
A_{lan}	Land area	m ²
A_{lan}^*	Relative land area	1
A_p	Recess area	m ²
b	Width perpendicular to the direction of flow	m

Table 1 (continued)

Symbol	Term	Unit
b_{ax}	Width of axial outlet $\left[b_{ax} = \frac{\pi \times D}{Z} - (l_c + b_G) \right]$	m
b_c	Width of circumferential outlet ($b_c = B - l_{ax}$)	m
b_G	Width of drainage groove	m
B	Bearing width	m
c	Stiffness coefficient	N/m
c_p	Specific heat capacity of the lubricant (p is a constant)	J/kg·K
C_R	Radial clearance	m
d_{cp}	Diameter of capillaries	m
D	Bearing diameter (D_J : shaft; D_B : bearing; $D \approx D_J \approx D_B$)	m
e	Eccentricity (shaft displacement)	m
f	Relative film thickness [$f = h/C_R$]	1
$f_{en,i}$	Relative film thickness at $\varphi = \varphi'_{1,i}$	1
$f_{ex,i}$	Relative film thickness at $\varphi = \varphi'_{2,i}$	1
F	Load-carrying capacity (load)	N
F_i	Radial force in recess i	N
F_h	Horizontal component of the resultant force of recesses	N
F_v	Vertical component of the resultant force of recesses	N
F^*	Characteristic value of load-carrying capacity	1
F_{eff}^*	Characteristic value of effective load-carrying capacity	1
$F_{eff,0}^*$	Characteristic value of effective load-carrying capacity for $N = 0$	1
h	Local lubricant film thickness (clearance gap height)	m
h_{en}	Oil film thickness at entrance edge of recess	m
h_{ex}	Oil film thickness at exit edge of recess	m
h_{min}	Minimum lubricant film thickness (minimum clearance gap height)	m
h_p	Depth of recess	m
i (index)	Consecutive number	1
k	Exponent	1
K_{rot}	Speed-dependent parameter	1
$K_{rot,nom}$	Normalized speed-dependent parameter	1
l	Length in the direction of flow	m
l_{ax}	Axial land length	m
l_c	Circumferential land length	m
l_{cp}	Length of capillaries	m
N	Rotational frequency (speed)	s ⁻¹
opt (index)	optimum	1
p	Recess pressure, general	Pa
\bar{p}	Specific bearing load [$\bar{p} = F/(B \times D)$]	Pa
p_{en}	Feed pressure (pumping pressure)	Pa
p_i	Pressure in recess i	Pa
p_i^*	Pressure ratio in recess i	1
$p_{i,0}$	Pressure in recess i , when $\varepsilon = 0$	Pa

Table 1 (continued)

Symbol	Term	Unit
p_{\max}	Maximum pressure in recess	Pa
p_{\min}	Minimum pressure in recess	Pa
P^*	Power ratio	1
P_f	Frictional power	W
$P_{f,\text{lan}}$	Frictional power in land area	W
$P_{f,p}$	Frictional power in recess area	W
P_f^*	Characteristic value for the frictional power	1
$P_{f,\text{lan}}^*$	Characteristic value for the frictional power in land area	1
$P_{f,p}^*$	Characteristic value for the frictional power in recess area	1
P_p	Pumping power	W
P_{tot}	Total power	W
P_{tot}^*	Characteristic value of total power	1
Q	Lubricant flow rate (for complete bearing)	m ³ /s
Q^*	Lubricant flow rate parameter	1
Q_{ax}	Lubricant flow rate from recess in the axial direction	m ³ /s
$Q_{\text{cp}, i}$	Lubricant flow rate from capillary into recess i	m ³ /s
Q_{en}	Inlet lubricant flow rate into recess in the circumferential direction	m ³ /s
Q_{ex}	Outlet lubricant flow rate from recess in the circumferential direction	m ³ /s
R_{cp}	Flow resistance of capillaries	Pa·s/m ³
$R_{\text{lan}, \text{ax}}$	Flow resistance of one axial land $\left(R_{\text{lan}, \text{ax}} = \frac{12 \times \eta \times l_{\text{ax}}}{b_{\text{ax}} \times C_{\text{R}}^3} \right)$	Pa·s/m ³
$R_{\text{lan}, \text{c}}$	Flow resistance of one circumferential land $\left(R_{\text{lan}, \text{c}} = \frac{12 \times \eta \times l_{\text{c}}}{b_{\text{c}} \times C_{\text{R}}^3} \right)$	Pa·s/m ³
$R_{p,0}$	Flow resistance of one recess, when $\varepsilon = 0$	Pa·s/m ³
Re	Reynolds number	1
Re_{cp}	Reynolds number in capillaries	1
Re_p	Reynolds number in recess	1
So	Sommerfeld number	1
T	Temperature	°C
T_{B}	Mean temperature in the bearings; see Formula (15)	°C
T_{cp}	Temperature in capillaries	°C
T_{en}	Inlet temperature	°C
u	Flow velocity	m/s
U	Circumferential speed	m/s
\bar{w}	Average velocity in restrictor	m/s
Z	Number of recesses	1
α	Position of first recess related to recess centre measured from load direction; see Figure A.3	rad
β	Attitude angle of shaft	°
γ	Exponent in viscosity formula	1
Δp_{lan}	Pressure difference in land area	Pa
ΔT	Temperature difference	K

Table 1 (continued)

Symbol	Term	Unit
ΔT_B	Mean temperature difference in the bearings	K
ΔT_{cp}	Temperature difference in capillaries	K
ε	Relative eccentricity	1
η	Dynamic viscosity	Pa·s
η_B	Dynamic viscosity for $T = T_B$	Pa·s
η_{cp}	Dynamic viscosity in capillaries	Pa·s
η_{40}	Dynamic viscosity at 40 °C	Pa·s
κ	Resistance ratio	1
ξ	Restrictor ratio	1
π_f	Relative frictional pressure	1
$\pi_{f,opt}$	Optimum relative frictional pressure	1
ρ	Density	kg/m ³
τ	Shearing stress	N/m ²
φ	Angular coordinate measured from radius opposite to eccentricity, e ; see Figure A.3	rad
φ_F	Angle of resultant force of recesses	rad
φ_G	Angle between the centre of land and the centre of drainage groove	rad
ψ	Relative bearing clearance	1
ψ_{opt}	Optimum relative bearing clearance	1
ω	Angular velocity ($\omega = 2 \times \pi \times N$)	s ⁻¹

5 Bases of calculation and boundary conditions

Calculation in accordance with this document is the mathematical determination of the operational parameters of hydrostatic plain journal bearings as a function of operating conditions, bearing geometry and lubrication data. This means the determination of eccentricities, load-carrying capacity, stiffness, required feed pressure, oil flow rate, frictional and pumping power, and temperature rise. Besides the hydrostatic pressure build up, the influence of hydrodynamic effects is also approximated.

Reynolds equation furnishes the theoretical basis for the calculation of hydrostatic bearings. In most practical cases of application, it is, however, possible to arrive at sufficiently exact results by approximation.

The approximation used in this document is based on two basic formulae intended to describe the flow through the bearing lands, which can be derived from Reynolds equation when special boundary conditions are observed. The Hagen-Poiseuille law describes the pressure flow in a parallel clearance gap and the Couette formula the drag flow in the bearing clearance gap caused by shaft rotation. A detailed presentation of the theoretical background of the calculation procedure is included in [Annex A](#). An example of the calculation procedure is given in [Annex B](#).

The following important premises are applicable to the calculation procedures described in this document:

- all lubricant flows in the lubrication clearance gap are laminar;
- the lubricant adheres completely to the sliding surfaces;
- the lubricant is an incompressible Newtonian fluid;
- in the whole lubrication clearance gap, as well as in the preceding restrictors, the lubricant is partially isoviscous;

- e) a lubrication clearance gap completely filled with lubricant is the basis of frictional behaviour;
- f) fluctuations of pressure in the lubricant film normal to the sliding surfaces do not take place;
- g) bearing and journal have completely rigid surfaces;
- h) the radii of curvature of the surfaces in relative motion to each other are large in comparison to the lubricant film thickness;
- i) the clearance gap height in the axial direction is constant (axial parallel clearance gap);
- j) the pressure over the recess area is constant;
- k) there is no motion normal to the sliding surfaces.

The bearing consists of Z cylindrical segments and rectangular recess of the same size and is supplied with oil through restrictors of the same flow characteristics. Each segment consists of a circumferential part between two centre lines of axial drainage grooves. With the aid of the above-mentioned approximation formulae, all parameters required for the design or calculation of bearings can be determined. The application of the similarity principle results in dimensionless similarity values for load-carrying capacity, stiffness, oil flow rate, friction, recess pressures, etc.

The results indicated in this document in the form of tables and diagrams are restricted to operating ranges common in practice for hydrostatic bearings. Thus, the range of the bearing eccentricity (displacement under load) is limited to $\varepsilon = 0$ to 0,5.

Limitation to this eccentricity range means a considerable simplification of the calculation procedure as the load-carrying capacity is a nearly linear function of the eccentricity. However, the applicability of this procedure is hardly restricted as in practice eccentricities $\varepsilon > 0,5$ are mostly undesirable for reasons of operational safety. A further assumption for the calculations is the approximated optimum restrictor ratio^[2] $\xi = 1$ for the stiffness behaviour.

As for the outside dimensions of the bearing, this document is restricted to the range bearing width/bearing diameter $B/D = 0,3$ to 1, which is common in practical cases of application. The recess depth is larger than the clearance gap height by a factor of 10 to 100. When calculating the friction losses, the friction loss over the recess in relation to the friction over the bearing lands can generally be neglected on account of the above premises. However, this does not apply when the bearing shall be optimized with regard to its total power losses.

To take into account the load direction of a bearing, it is necessary to distinguish between the two extreme cases, load in the direction of recess centre and load in the direction of land centre.

Apart from the aforementioned boundary conditions, some other requirements are to be mentioned for the design of hydrostatic bearings in order to ensure their functioning under all operating conditions. In general, a bearing shall be designed in such a manner that a clearance gap height of at least 50 % to 60 % of the initial clearance gap height is ensured when the maximum possible load is applied. With this in mind, particular attention shall be paid to misalignments of the shaft in the bearing due to shaft deflection which may result in contact between shaft and bearing edge and thus in damage of the bearing. In addition, the parallel clearance gap required for the calculation is no longer present in such a case.

In the case where the shaft is in contact with the bearing lands when the hydrostatic pressure is switched off, it can be necessary to check the contact zones with regard to rising surface pressures.

It shall be ensured that the heat originating in the bearing does not lead to a non-permissible rise in the temperature of the oil.

If necessary, a means of cooling the oil shall be provided. Furthermore, the oil shall be filtered in order to avoid choking of the capillaries and damage to the sliding surfaces.

Low pressure in the relieved recess shall also be avoided, as this leads to air being drawn in from the environment and this would lead to a decrease in stiffness (see [6.7](#)).

6 Method of calculation

6.1 General

This document covers the calculation, as well as the design, of hydrostatic plain journal bearings. In this case, calculation is understood to be the verification of the operational parameters of a hydrostatic bearing with known geometrical and lubrication data. In the case of a design calculation, with the given methods of calculation, it is possible to determine the missing data for the required bearing geometry, the lubrication data and the operational parameters on the basis of a few initial data (e.g. required load-carrying capacity, stiffness, rotational frequency).

In both cases, the calculations are carried out according to an approximation method based on the Hagen-Poiseuille and the Couette formulae, mentioned in [Clause 5](#), see also [A.2.2](#) and [A.2.3](#). The bearing parameters calculated according to this method are given as relative values in the form of tables and diagrams as a function of different parameters. The procedure for the calculation or design of bearings is described in [6.2](#) to [6.7](#). This includes the determination of different bearing parameters with the aid of the given calculation formulae or the tables and diagrams. The following calculation items are explained in detail:

- a) determination of load-carrying capacity with and without taking into account shaft rotation;
- b) calculation of lubricant flow rate and pumping power;
- c) determination of frictional power with and without consideration of losses in the bearing recesses;
- d) procedure for bearing optimization with regard to minimum total power loss.

For all calculations, it is necessary to check whether the important premise of laminar flow in the bearing clearance gap, in the bearing recess and in the capillary is met. This is checked by determining the Reynolds numbers. Furthermore, the portion of the inertia factor in the pressure differences shall be kept low at the capillary (see [A.3.1](#)).

If the boundary conditions defined in [Clause 5](#) are observed, this method of calculation yields results with deviations which can be neglected for the requirements of practice, in comparison with an exact calculation by solving the Reynolds equation.

6.2 Load-carrying capacity

Unless indicated otherwise, it is assumed in the following that capillaries with a linear characteristic are used as restrictors and that the restrictor ratio is $\xi = 1$. Furthermore, the difference is only made between the two cases, "load in direction of recess centre" and "load in direction of land centre". For this reason, it is no longer mentioned in each individual case that the characteristic values are a function of the three parameters, "restrictor type", "restrictor ratio" and "load direction relative to the bearing".

Even under the abovementioned premises, the characteristic value of load carrying capacity [[Formula \(1\)](#)]

$$F^* = \frac{F}{B \times D \times p_{en}} = \frac{\bar{p}}{p_{en}} \quad (1)$$

still depends on the following parameters:

- number of recesses, Z ;
- width/diameter ratio, B/D ;
- relative axial land width, l_{ax}/B ;
- relative land width in circumferential direction, l_c/D ;
- relative groove width, b_G/D ;