

# International Standard

ISO 21771-1

First edition

# Cylindrical involute gears and gear pairs —

Part 1:

Concepts and geometryi Teh Standar Is

Roues et engrenages cylindriques à développante — 2000 2005 1000 2000

Partie 1: Concepts et géométrie

Document Preview

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#### Foreword

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The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see <a href="https://www.iso.org/directives">www.iso.org/directives</a>).

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This document was prepared by Technical Committee ISO/TC 60, *Gears*, Subcommittee SC 1, *Nomenclature* and wormgearing.

This first edition of ISO 21771-1 cancels and replaces ISO 21771:2007, which has been technically revised.

The main changes are as follows:

- the sign convention for internal gears used in the ISO 6336 series<sup>[8]</sup> has been adopted. The negative value for the number of teeth of an internal gear is applied to the diameters and centre distance, so these dimensions of internal gears have negative values;
- flank direction has been renamed as hand of helix and sign (+/-) of helix angle is used;
- a definition of normal surface has been added and this is used rather than normal plane;
- the annex on tooth thickness was removed because it is now addressed in ISO 21771-2.

Additional material has been added to cover:

- calculation of form diameters for tooth tip corner radius and tooth root fillet radius in the transverse plane for an involute cylindrical gear (<u>Clauses 10</u>, <u>11</u> and <u>Annex B</u>);
- calculation of the tooth tip corner radius for a specified form diameter and tip diameter of an involute cylindrical gear;
- calculation of a radius tangent to the involutes of adjacent teeth at root or tip diameter (Annex A);
- generated tooth root fillet shape for individual involute cylindrical gears (Annex B);
- concepts and parameters for involute cylindrical gear pairs with crossed axes (<u>Clause 6</u> and <u>Annex C</u>);
- geometry of surfaces in contact (Annex D);
- projection of a transverse plane profile of a tooth onto another plane (Annex E);

— interface to ISO 10828 for involute worm gear geometry (Annex F).

A list of all parts in the ISO 21771 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at <a href="https://www.iso.org/members.html">www.iso.org/members.html</a>.

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# Cylindrical involute gears and gear pairs —

### Part 1:

# **Concepts and geometry**

## 1 Scope

This document specifies the geometric concepts and parameters for cylindrical gears with involute helicoid tooth flanks. Flank modifications are included. The formulae in this document apply to all pressure angles.

It also covers the concepts and parameters for involute cylindrical gear pairs with parallel or crossed axes, and a constant gear ratio. Gear and mating gear in these gear pairs have the same basic rack tooth profile.

#### 2 Normative references

There are no normative references in this document.

### 3 Terms, definitions, symbols, subscripts and units

#### 3.1 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <a href="https://www.iso.org/obp">https://www.iso.org/obp</a>
- IEC Electropedia: available at https://www.electropedia.org/

#### 3.1.1

#### basic rack tooth profile for involute gear teeth

tooth profile of a normal section through the teeth of a basic rack which corresponds to an external spur gear with number of teeth  $z = \infty$  and diameter  $d = \infty$ 

Note 1 to entry: The tooth of the basic rack tooth profile is bounded by the tip line at the top and by the parallel root line at the bottom. The fillet between the straight part of the profile and the root line is a circular arc with a radius equal to  $\rho_{\rm fP}$ .

#### 3.1.2

#### counterpart rack tooth profile

rack tooth profile symmetrical to the basic rack tooth profile about the datum line P-P and displaced by half a pitch relative to it

#### 3.1.3

#### nominal involute flank

pure involute flank prior to any modifications

Note 1 to entry: See 4.4 for more information on a gear tooth involute flank.

#### 3.1.4

## $tip\ alteration\ coefficient$

k

change to the addendum relating to the standard addendum of one normal module, it is made non-dimensional by dividing by the normal module

Note 1 to entry: Tip alteration is also known as addendum modification, tip shortening or truncation.

#### 3.1.5

#### generating gear pair

generating tool (rack, hob, pinion-type cutter, or grinding wheel) and the gear being machined during gear tooth machining process

### 3.2 Symbols

<u>Table 1</u> provides all the symbols used in this document.

Table 1 — Symbols

Symbol	Description	Subclause
A	pinion lower end point of meshing (near pinion root)	5.5.6.1
$a_w$	working centre distance of a cylindrical gear pair	5.3.3, 5.3.5, 6.3.12
a <sub>w0</sub>	centre distance in the generating process with pinion-type cutter	11.2
В	pinion lower point of single tooth contact (LPSTC)	5.5.6.1
b	facewidth I I CHI Stantuarus	4.3.9
$b_{Ea}$	length of relief near tip	8.5.2
$b_{ m Ef}$	length of relief near root	8.5.2
$b_{ m F}$	usable facewidth Proview	4.3.9
$b_{\mathrm{w}}$	active facewidth (the facewidth used)	5.5.9.2
С	working pitch point with subscript: amount of relief for modifications	<u>5.3.5</u> <u>8</u>
$C_{ay}$	modification of the profile by function	85/180-pri-8.6/71-1
$C_{\rm Ea}$	amount of triangular end relief modification at tip	8.5.2
$C_{\mathrm{Ef}}$	amount of triangular end relief modification at root	8.5.2
$C_{ m Hlpha}$	amount of transverse profile slope modification	8.3.3
$C_{\mathrm{H}\beta}$	amount of flank line slope modification	8.4.2
$C_{i,j}$	amount of modification at point (i,j)	<u>8.5.1</u>
$C_{\alpha}$	amount of profile crowning (barrelling)	8.3.4
$C_{\alpha a}$	amount of tip relief	8.3.2
$C_{\alpha f}$	amount of root relief	8.3.2
$C_{\beta}$	amount of flank line crowning	8.4.3
$C_{\beta I}$ , $C_{\beta II}$	amount of end relief	<u>8.4.1</u>
$C_{eta y}$	modification of the flank line by function	<u>8.6</u>
$C_{\Sigma \mathrm{y}}$	modification of the flank surface by function	<u>8.6</u>
С	tip clearance	<u>5.3.8, 6.3.15</u>
$c_{\mathrm{F}}$	form over dimension	<u>5.5.5</u>
D	pinion highest point of single tooth contact (HPSTC)	<u>5.5.6.1</u>
d	reference diameter	4.3.4
$d_{\rm a}$	tip diameter	4.6.5
$d_{a0}$	tip diameter of pinion-type cutter	<u>11.1</u>

Symbol	Description	Subclause
$d_{ m b}$	base diameter	<u>4.4.2</u>
$d_{ m b0}$	base diameter of the pinion-type cutter	<u>11.1</u>
$d_{ m bK}$	chamfering base diameter	8.2.2
$d_{Clpha a}$	tip relief start diameter	8.3.2
$d_{C\alphaf}$	root relief start diameter	<u>8.3.2</u>
$d_{\mathrm{Cf}}$	Profile control diameter	<u>8.3.2</u>
$d_{\mathrm{Ea}}$	diameter for start of triangular end relief at tooth tip	<u>8.5.2</u>
$d_{ m Ef}$	diameter for start of triangular end relief at tooth root	8.5.2
$d_{\mathrm{Fa}}$	tip form diameter	<u>9.7</u>
$d_{ m Ff}$	root form diameter	<u>5.5.2, 9.7</u>
$d_{ m f}$	root diameter (nominal dimension)	4.6.7
$d_{ m fE}$	root diameter produced	<u>9.6</u>
$d_{ m Na}$	active tip diameter	<u>5.5.2</u> , <u>6.4.3</u>
$d_{ m Nf}$	start of active profile diameter (SAP diameter, active root diameter)	<u>5.5.2</u> , <u>6.4.3</u>
$d_{\rm v}$	V-circle diameter	4.6.2
$d_{\mathrm{w}}$	working pitch diameter	<u>5.3.5</u>
$d_{\rm v}$	Y-circle diameter	4.6.3
$d_0$	reference diameter of pinion-type cutter	<u>11.1.1</u>
E	pinion upper end point of meshing (near pinion tip)	<u>5.5.6.1</u>
$E_{ m sni}$	lower tooth thickness limit deviation for normal tooth thickness at reference cylinder	9.4
$E_{\rm sns}$	upper tooth thickness limit deviation for normal tooth thickness at reference cylinder	9.4
$e_{\rm n}$	normal space width on the reference cylinder	4.8.7
$e_{ m P}$	space width of the basic rack tooth profile	4.3.3
$e_{t}$	transverse space width on the reference cylinder	4.8.4
$e_{ m yn}$	normal space width on the y-cylinder O/PRF 2177[-]	4.8.7
httpe://star	transverse space width on the y-cylinder abd99-aa53-4275-8ea0-bb8fe79bc285/1	so-prf <u>4.8.4</u> 71-1
F	force	<u>D.3</u>
$g_{\mathrm{a}}$	length of addendum path of contact	<u>5.5.6.2</u> , <u>6.4.5.2</u>
$g_{ m f}$	length of dedendum path of contact	<u>5.5.6.2</u> , <u>6.4.5.2</u>
$g_{\alpha}$	length of path of contact	5.5.6.2
$g_{\alpha y}$	distance of a point Y from working pitch point C	<u>5.7.5</u>
$g_{eta}$	overlap roll length (arc of contact)	<u>5.5.9.4</u>
h	tooth depth (between tip line and root line)	4.7.1
$h_{\rm a}$	addendum from reference pitch circle	4.7.2
$h_{aP}$	addendum of the basic rack tooth profile	4.3.2
$h_{aP0}$	addendum of the counterpart of the basic rack tooth profile	9.2.2
$h_{\rm aw}$	addendum from working pitch circle	4.7.2
$h_{a0}$	addendum of pinion-type cutter	11.1.1
$h_{\rm FaP0}$	straight part of tip flank of tool-generating profile	9.2.2
$h_{\mathrm{FfP}}$	portion of the dedendum to root form line, of the basic rack tooth profile	4.3.2
$h_{\mathrm{FfP0}}$	portion of the dedendum to root form line of the counterpart rack tooth profile	9.2.1
$h_{\mathrm{fP0}}$	dedendum of the counterpart rack tooth profile and rack tool	9.2.2
$h_{\rm f}$	dedendum from reference circle	4.7.2
$h_{\mathrm{fP}}$	dedendum of the basic rack tooth profile	4.3.3

Symbol	Description	Subclause
$h_{\mathrm{fw}}$	dedendum from working pitch circle	4.7.2
$h_{ m K}$	height of the tip corner chamfering or tip corner rounding	<u>8.2.2</u>
$h_{ m P}$	tooth depth of basic rack tooth profile	4.3.2
$h_{\mathrm{w}}$	working depth of teeth in a gear pair	<u>5.3.7</u> , <u>6.3.14</u>
i	transmission ratio of a gear pair	<u>5.3.2</u>
inv	involute function (not a variable)	<u>4.4.5</u>
$j_{ m bn}$	normal base backlash	<u>5.6.4</u> , <u>6.5.2</u>
$j_{ m bt}$	transverse backlash	<u>5.6.2</u>
$j_{\rm r}$	radial backlash	<u>5.6.5</u>
$j_{t}$	circumferential backlash at the reference circle	<u>5.6.3</u> , <u>6.5.3</u>
$j_{ m wn}$	working normal backlash	<u>6.5.2</u>
$j_{\mathrm{wt}}$	circumferential backlash at the working pitch circle	<u>5.6.3</u> , <u>6.5.3</u>
$K_{\rm g}$	sliding factor	<u>5.7.6</u>
$K_{\rm ga}$	sliding factor at tooth tip	<u>5.7.6</u>
$K_{\rm gf}$	sliding factor at tooth root	<u>5.7.6</u>
k	tip alteration coefficient	3.1.3, 4.6.4, 5.3.9, 6.3.16
$L_{Ca}$	tip relief roll length	8.3.2
$L_{Cf}$	root relief roll length	8.3.2
$L_{\rm Cl}$ , $L_{\rm ClI}$	length of end relief	<u>8.4.1</u>
$L_{Ea}$	tip roll length of triangular end relief modification	<u>8.5.2</u>
$L_{ m Ef}$	root roll length of triangular end relief modification	<u>8.5.2</u>
$L_{\mathrm{y}}$	length of roll to y-cylinder of the preview	4.4.10
$L_{ m yt}$	length of involute profile to y-cylinder	4.4.11
$l_{\max}$	maximum length of a contact line ISO/PRE 21771_1	<u>5.5.10</u>
httr.Mv/sta	a point on a tooth flank where radius of curvature is calculated	so-prf- <del>7.1</del> 771-1
m	module	4.3.7
$m_{\mathrm{n}}$	normal module	4.3.7
$m_{t}$	transverse module	4.3.7
$m_{\mathrm{x}}$	axial module	4.3.7
N	number of tooth or pitch	4.2.6
$n_{\rm a}$	rotational speed of driving gear (rpm)	<u>5.3.2</u>
$n_{\mathrm{b}}$	rotational speed of driven gear (rpm)	<u>5.3.2</u>
0	centre of a circle	<u>6.3.4</u>
$P_{\rm d}$	diametral pitch	4.3.8
$P_{\rm nd}$	normal diametral pitch	4.3.8
$p_{\rm bn}$	normal base pitch	<u>4.5.5.1</u>
$p_{\mathrm{bt}}$	transverse base pitch	<u>4.5.5.1</u>
$p_{\rm en}$	normal base pitch on the path of contact	4.5.5.3
$p_{\mathrm{et}}$	transverse base pitch on the path of contact	4.5.5.2
$p_{\rm n}$	normal pitch on the reference cylinder	4.5.2.2
$p_{t}$	transverse pitch on the reference cylinder	4.5.2.1
$p_{\mathrm{wn}}$	normal pitch at the working diameter	<u>6.3.6</u> , <u>6.5.2</u>
$p_{\rm x}$	axial pitch	4.5.4

Symbol	Description	Subclause
$p_{ m yn}$	normal pitch on the y-cylinder	4.5.3
$p_{ m yt}$	transverse pitch on the y-cylinder	4.5.3
$p_{\rm z}$	lead	4.4.6
pr	protuberance of the tool (as seen in ISO 6336-3)	9.2.1
q	machining allowance on tooth flank	<u>9.3</u>
$q_{ m Fs}$	magnitude (amount) of undercut in transverse plane	8.2.1
R'	first principal radius of curvature of surface	<u>7.4</u>
R''	second principal radius of curvature of surface	<u>7.4</u>
$R_{\rm c}$	radius of curvature of trochoid at point M	<u>10.4</u>
$R_{\rm fp}$	radius of curvature of the basic rack profile at point Q	<u>10.4</u>
R <sub>tro-y</sub>	radius of the fillet at point Q	<u>10.4</u>
$r_{a0}$	tip radius of the pinion-type cutter	<u>11.1.1</u>
$r_{\rm b0}$	base radius of the pinion-type cutter	<u>11.2</u>
$r_{\rm ea}$	x axis of ellipse	<u>10.4</u>
$r_{\rm eb}$	y axis of ellipse	10.4
$r_{\rm Fa0}$	tip form radius of the pinion-type cutter	11.1.1
$r_{\mathrm{Ff}}$	root form radius	10.3
$r_{\rm inv}$	radius to point on involute	10.1, 11.4.4.1
$r_{M0}$	radius for the centre of the tool tooth tip rounding of the pinion-type cutter	11.1.1
$r_{\rm tro}$	radius to point on trochoid	10.1
$r_{\rm w}$	manufacturing pitch circle radius of the gear	11.4.3
$r_{\rm w0}$	manufacturing pitch circle radius of the pinion-type cutter	11.4.3
$r_{\rm ya0}(\theta_{\rm M})$	radial polar coordinate of point M on tip radius of pinion-type cutter	Figure B.1
$r_{\rm vft}(\theta_{\rm M})$	radial polar coordinate of point M on the gear fillet generated with pinion-type cutter	
$S_{\alpha}$	twist of the transverse profile   SO/PRF 2177 -	8.5.3
http $S_{\dot{\beta}}$ /star	twist of the flank line /standards/iso/859abd99-aa53-4275-8ea0-bb8fe79bc285/i	so-prf <u>8.5.3</u> 71-1
$s_{aK}$	tip transverse tooth thickness when tip chamfering or tip rounding	8.2.2
$S_{\rm n}$	normal tooth thickness at the reference diameter	4.8.6
S <sub>ni</sub>	minimum normal tooth thickness at the reference diameter	9.4
S <sub>ns</sub>	maximum normal tooth thickness at the reference diameter	9.4
S <sub>P</sub>	tooth thickness of the basic rack tooth profile	4.3.3
Spr	residual fillet undercut (on normal surface)	10.1
s <sub>prt</sub>	residual fillet undercut (transverse plane)	11.4.1
$S_{t}$	transverse tooth thickness at the reference diameter	4.8.2
S <sub>wn</sub>	normal tooth thickness at working diameter	<u>6.3.6, 6.5.2</u>
S <sub>wt</sub>	transverse tooth thickness at working diameter	6.3.8
S <sub>yn</sub>	normal tooth thickness at the Y circle diameter	4.8.6
S <sub>yt</sub>	transverse tooth thickness at the Y circle diameter	4.8.2
T	tangent point on base circle of line normal to involute	4.4.9
T <sub>1</sub>	point of contact between the line of action and the base circle of pinion	5.5.6.1
$T_2$	point of contact between the line of action and the base circle of gear wheel	5.5.6.1
$T_1$	unit vector of reference helix	4.10
$T_2$	unit vector of generator	4.10

Symbol	Description	Subclause
$T_{M1}$	tangency point between the base cylinder of the pinion and a line normal to a contact line through point $\mathbf{M}_{\mathbf{y}}$	<u>7.1</u>
$T_{M2}$	tangency point on the base cylinder of the gear wheel and a line normal to a contact line through point $\mathbf{M}_{\mathbf{y}}$	<u>7.1</u>
U	involute point of origin	4.4.9
и	gear ratio gear	<u>5.3.1</u>
v	circumferential velocity at reference diameter	<u>5.7.2</u>
$v_{\rm b}$	circumferential velocity at base diameter	<u>5.7.2</u>
$v_{\rm g}$	sliding velocity	<u>5.7.5</u>
$v_{\rm ga}$	sliding velocity at the active addendum	<u>5.7.5</u>
$v_{\rm gf}$	sliding velocity at the active dedendum	<u>5.7.5</u>
$v_{ m Mg}$	sliding velocity at point M	6.6.4
$v_{\rm n}$	normal velocity	<u>5.7.3</u>
$v_{\rm ry}$	rolling velocity at diameter $d_{ m v}$	<u>5.7.4</u>
$v_{\mathrm{w}}$	circumferential velocity of the working pitch circles	<u>5.7.2</u> , <u>5.7.6</u>
$v_{\rm y}$	circumferential velocity at diameter $d_{\mathrm{v}}$	<u>5.7.2</u>
X	profile shift coefficient	4.3.10
x <sub>E</sub>	generating profile shift coefficient	<u>9.2.1</u>
$x_{\rm Ei}$	lower limit generating profile shift coefficient	<u>9.5</u>
$x_{\rm Es}$	upper limit generating profile shift coefficient	<u>9.5</u>
$x_{\rm EsV}$	profile shift coefficient for rough machining, upper limit	<u>9.5</u>
x <sub>EiV</sub>	profile shift coefficient for rough machining, lower limit	<u>9.5</u>
$x_{\rm Eu}$	generating profile shift coefficient at undercut limit	9.8
<i>x</i> <sub>0</sub>	profile shift coefficient of the pinion-type cutter	<u>11.1.1</u>
X <sub>1</sub>	point on x axis of coordinate system of surface 1	<u>D.1</u>
X <sub>2</sub>	point on x axis of coordinate system of surface 2	D.1
ttps://sta Y	any point on a tooth flank or involute	4.4.3
Y <sub>1</sub>	point on y axis of coordinate system of surface 1	<u>D.1</u>
Y <sub>2</sub>	point on y axis of coordinate system of surface 2	<u>D.1</u>
Z	number of teeth	4.2.5
$z_{\rm a}$	number of teeth of driving gear	<u>5.3.2</u>
$z_{\rm b}$	number of teeth of driven gear	<u>5.3.2</u>
$z_0$	number of teeth of pinion-type cutter	<u>11.1.1</u>
$Z_1$	point on z axis of coordinate system of surface 1	<u>D.1</u>
$Z_2$	point on z axis of coordinate system of surface 2	<u>D.1</u>
$\alpha_{\rm a}$	pressure angle at tip circle	5.5.8.3
$\alpha_{\rm Fa}$	pressure angle at the tip form diameter $d_{\mathrm{Fa}}$	<u>A.2.1</u>
$\alpha_{\rm Fa0}$	pressure angle on the radius $r_{\rm Fa0}$ of pinion-type cutter	<u>11.1.1</u>
$\alpha_{\mathrm{Ff}}$	pressure angle at root form circle	<u>9.7</u>
$\alpha_{\mathrm{KP0}}$	normal chamfering pressure angle of the counterpart rack tooth profile	8.2.2
$\alpha_{\rm KP0t}$	transverse chamfering pressure angle of the counterpart rack tooth profile	8.2.2
$\alpha_{\rm Mt0}$	transverse pressure angle for the radius at the point M of the pinion-type cutter	11.1.1
$\alpha_{\rm NP}$	pressure angle at start of active profile	5.5.2.2
$\alpha_{\rm n}$	normal pressure angle	4.4.4
$\alpha_{\rm P}$	pressure angle of the basic rack tooth profile	4.4.4