



Designation: ~~D5540~~—~~08~~ D5540 – 13

# Standard Practice for Flow Control and Temperature Control for On-Line Water Sampling and Analysis<sup>1</sup>

This standard is issued under the fixed designation D5540; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This practice covers the conditioning of a flowing water sample for the precise measurement of various chemical and physical parameters of the water, whether continuous or grab. This practice addresses the conditioning of both high- and low-temperature and pressure sample streams, whether from steam or water.

1.2 This practice provides procedures for the precise control of sample flow rate to minimize changes of the measured variable(s) due to flow changes.

1.3 This practice provides procedures for the precise control of sample temperature to minimize changes of the measured variable(s) due to temperature changes.

1.4 The values stated in either SI or inch-pound units are to be regarded as the standard. The values given in parentheses are for information only. mathematical conversions to inch-pound units that are provided for information only and are not considered standard.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

## 2. Referenced Documents

2.1 *ASTM Standards:*<sup>2</sup>

[D1066 Practice for Sampling Steam](#)

[D1129 Terminology Relating to Water](#)

[D3370 Practices for Sampling Water from Closed Conduits](#)

[D3864 Guide for On-Line Monitoring Systems for Water Analysis](#)

## 3. Terminology

3.1 *Definitions*—For definitions of terms used in this practice, refer to Terminology [D1129](#).

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *approach temperature*—~~temperature,  $n$ —this is a term that is used in heat exchanger applications. It applies to all types of heat exchangers and is defined as: the difference in outlet temperature in one stream and the inlet temperature on the other stream. The definition as it applies to sample coolers used for cooling water or steam samples as noted in this standard is as follows:~~ Approach Temperature—the difference in temperature between cooling water temperature in and sample temperature out.

<sup>1</sup> This practice is under the jurisdiction of ASTM Committee D19 on Water and is the direct responsibility of Subcommittee D19.03 on Sampling Water and Water-Formed Deposits, Analysis of Water for Power Generation and Process Use, On-Line Water Analysis, and Surveillance of Water.

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<sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

### 3.2.1.1 *Discussion*—

This term is used in heat exchanger applications and applies to all types of heat exchangers. The term is defined as: the difference between the outlet temperature in one stream and the inlet temperature in the other stream.

3.2.2 ~~crud deposition—deposition, n—deposition~~ on interior surfaces of sample tubing or other hardware, the disposition of fine insoluble particles of (of iron oxides and other byproducts of metallic corrosion) that are present throughout the system. The term “crud” is generally used for all types of fouling.

### 3.2.2.1 Discussion—

The term “crud” is generally used for all types of fouling.

3.2.3 ~~sample conditioning—conditioning, n—reduction of the temperature and pressure of a flowing sample from process conditions to a controlled temperature and pressure, and maintenance of a constant flow rate both in incoming sample lines and through on-line analyzers.~~

3.2.4 ~~sample cooler—cooler, n—a small heat exchanger designed to cool small streams of water or steam.~~

3.2.5 ~~temperature compensation—compensation, n—adjustment by the use of electronic adjustment or data manipulation, the adjustment of the analyzer’s measured value~~ temperature for variation in temperature of the sample—sample temperature from a preestablished value by the use of electronic adjustment or data manipulation—value.

## 4. Summary of Practice

4.1 This practice covers the system design, operating procedures, and selection of equipment to help ensure the appropriate flow and temperature control for analysis of water and steam samples. This control is essential to ensure the accuracy and repeatability of on-line analyzers. Variations in types of analysis, sample characteristics, and their effect on sample conditioning are included.

4.2 The equipment and procedures described in this practice are intended to represent current state-of-the art technology available from major manufacturers of sample conditioning equipment. Refer to Practices **D1066** and **D3370** and Guide **D3864** for additional information on sampling.

## 5. Significance and Use

5.1 Sample conditioning systems must be designed to accommodate a wide range of sample source temperatures and pressures. Additionally, efforts must be made to ensure that the resultant sample has not been altered during transport and conditioning and has not suffered excessive transport delay. Studies have shown that sample streams will exhibit minimal deposition of ionic and particulate matter on wetted surfaces at specific flow rates **(41-5-5)**.<sup>3</sup>

5.1.1 To ensure that the physical and chemical properties of the sample are preserved, this flow rate must be controlled throughout the sampling process, regardless of expected changes of source temperature and pressure, for example, during startup, or changing process operating conditions.

5.2 The need to use analyzer temperature compensation methods is dependent on the required accuracy of the measurement. Facilities dealing with ultra-pure water will require both closely controlled sample temperature and temperature compensation to ensure accurate measurements. The temperature can be controlled by adding a second or trim cooling stage. The temperature compensation must be based on the specific contaminants in the sample being analyzed. In other facilities in which some variation in water chemistry can be tolerated, the use of either trim cooling or accurate temperature compensation may provide sufficient accuracy of process measurements. This does not negate the highly recommended practice of constant temperature sampling, especially at 25°C, as the most proven method of ensuring repeatable and comparable analytical results.

5.3 A separate class of analysis exists that does not require or, in fact, cannot use the fully conditioned sample for accurate results. For example, the collection of corrosion product samples requires that the sample remain at near full system pressure, but cooled below the flash temperature, in order to ensure a representative collection of particulates. Only some of the primary conditioning criteria apply in this case, as in others. Temperature compensation is not applicable since the material being analyzed is not in a liquid state.

## 6. Interferences

6.1 Samples can be degraded by the loss of ionic or particulate components, introduction of contaminants by components or leaks, changes of sample flow rate through an analyzer, excessively long sample lines, sample temperature changes, and inaccurate temperature compensation of on-line analysis equipment.

6.2 Studies **(33-5-5)** have shown that the loss of ionic and particulate components is minimized by maintaining the water sample velocity at 1.8 m/s in the sample tubing transporting the sample. The turbulent flow at 1.8 m/s (6 ft/s) presents a stable condition of deposition and removal. Changes in sample flow rate or flow rates beyond a median range of approximately 1.8 m/s can upset this equilibrium condition.

<sup>3</sup> The boldface numbers in parentheses refer to the list of references at the end of this practice standard.

6.3 Saturated steam and superheated steam samples present difficult transport problems between the source and the primary sample cooling equipment (4). Saturated steam samples with transport velocities typically above 11 m/s (36 ft/s) provide adequate turbulent flow to ensure the transport of most particulates and ionic components. Excessively large or small steam sample lines can affect the sample quality and quantity significantly. If the sample tubing has too large an inside diameter, the steam velocity may be too low to transport the condensed portion of the steam along with the vapor. If the sample tubing has too small an inside diameter, the pressure drop may be excessive, reducing the quantity of sample available at the sample panel. In the case of super-heated steam, significant ionic deposition can occur in the sample tubing transport as the steam desuperheats. This can affect sample analysis accuracy significantly. Superheated samples should use a process to inject cooled sample into the sample line at or near the nozzle outlet to desuperheat the sample so as to minimize deposition in the initial portion of the tubing run.

6.4 Samples may become contaminated by products introduced into the stream by the tubing, valves, or other associated conditioning hardware. To minimize contamination of the sample, high-grade tubing, such as Type 316 SS, must be used. Cobalt contamination from valve hardening material can introduce significant error in transition metal analysis by ion chromatography.

6.5 Air leakage into sample lines can affect pH, conductivity (specific, cation, and degassed), and especially dissolved oxygen measurements.

6.6 The operation of a sample system includes periodically taking grab samples and adding and removing on-line analyzers. The accuracy of the analyses can be affected if the flow rate through any on-line analyzer changes because of these procedures. The same is true if these actions change the flow rate in the incoming sample line to the system.

6.7 Changing the temperature of the sample flowing through an on-line analyzer can alter the accuracy of the analysis. Sample temperature can change because of a change in flow rate through the heat exchangers, because of a change of flow rate of the cooling water in the heat exchangers, or from a change in temperature of the heat exchanger cooling water supply. Every effort should be made to ensure constant sample temperature. The ideal sample temperature is  $25 \pm 0.5^\circ\text{C}$  ( $77 \pm 1^\circ\text{F}$ ) because this is the standard for comparing readings of temperature-sensitive analyses.

6.8 Electronic compensation is able to compensate for the deviations in sample temperature for a known chemical matrix (contamination). If an unknown source of contamination is introduced, the analyzer may not be programmed, or programmable, to respond to the new solution. An error is introduced as a result. The further the sample temperature deviates from  $25^\circ\text{C}$  ( $77^\circ\text{F}$ ), the greater the error.

6.9 In sliding pressure or cycling power plants, or both, in which sample inlet pressures vary, the sample flow methodology detailed in this practice should be modified to automate the flow control process to ensure constant sample flow for high-accuracy analysis.

## 7. Apparatus

7.1 *Sample Tubing*—Tubing should be high quality such as Type 316 SS and be sized to maintain appropriate flow to minimize sample analysis errors. The tubing inside diameter is the critical dimension. Heavy-wall tube with an appropriate inside diameter size selected to provide proper flow rate (see 6.2) can be used for construction strength.

7.2 *Primary Sample Coolers*—Heat exchangers, designed to handle high-pressure and high-temperature samples and provide efficient cooling typically with approach temperatures of below  $1^\circ\text{C}$  ( $1.8^\circ\text{F}$ ), should be selected. Generally, Type 316 SS is an appropriate sample tube material; however, other material selections may be necessary based on incoming sample temperature and cooling water impurities, that is, chlorides.

7.3 *Pressure Reducers*—Pressure reduction is accomplished with a variable orifice. A high-quality needle valve performs well for source pressure less than 34.5 bar (500 psig). A variable rod-in-tube device performs well for pressures 34.5 bar and greater because it is basically non-wearing and minimizes sample dissociation during pressure reduction.

7.4 *Pressure Regulating Device*—To maintain constant sample pressure at the inlet to each analyzer train, a variable or fixed back pressure regulating valve may be used.

7.5 *Secondary or Trim Sample Cooler*—Similar to the primary sample cooler, this heat exchanger should be a device capable of maintaining a sample outlet temperature within  $0.5^\circ\text{C}$  ( $1^\circ\text{F}$ ) of the incoming cooling water temperature to ensure constant outlet temperature, even with significant variations in sample flow or heat load.

7.6 *Sample Flow Indicator(s)*—A non-valved rotameter or other flow indication device in the main sample line or flow indication device, or both, in all branch lines (analysis, grab, and bypass) is typically used. A method of measuring total sample flow in accordance with recommended velocities must be used (see 6.2 and 8.4).

7.7 *Temperature Indicator*—A mechanical or electronic indication of sample temperature must be provided to help the operator monitor sample conditions and confirm the efficiency of the heat exchangers.

7.8 *Pressure Indicator*—A mechanical or electronic indication of the upstream pressure of the pressure regulating device (V4) to confirm proper operation of the device.