



Designation: **E1225—09 E1225 – 13**

Standard Test Method for Thermal Conductivity of Solids by Means of Using the Guarded-Comparative-Longitudinal Heat Flow Technique¹

This standard is issued under the fixed designation E1225; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense.

1. Scope

1.1 This test method describes a steady state technique for the determination of the thermal conductivity, λ , of homogeneous-opaque solids (see [Notes 1 and 2](#)). This test method is ~~for applicable to~~ materials with effective thermal conductivities in the approximate-range $0.2 < \lambda < 200 \text{ W/(m}\cdot\text{K)}$ over the approximate-temperature range between 90 and 1300 K. It can be used outside these ranges with decreased accuracy.

NOTE 1—For purposes of this technique, a system is homogeneous if the apparent thermal conductivity of the specimen, λ_A , does not vary with changes of thickness or cross-sectional area by more than $\pm 5\%$. For composites or heterogeneous systems consisting of slabs or plates bonded together, the specimen should be more than 20 units wide and 20 units thick, respectively, where a unit is the thickness of the thickest slab or plate, so that diameter or length changes of one-half unit will affect the apparent λ_A by less than $\pm 5\%$. For systems that are non-opaque or partially transparent in the infrared, the combined error due to inhomogeneity and photon transmission should be less than $\pm 5\%$. Measurements on highly transparent solids must be accompanied with infrared absorption coefficient information, or the results must be reported as apparent thermal conductivity, λ_A .

NOTE 2—This test method may also be used to evaluate the contact thermal conductance/resistance of materials.

1.2 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.3 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

~~E177 Test Method for Steady-State Heat Flux Measurements and Thermal Transmission Properties by Means of the Guarded-Hot-Plate Apparatus~~

~~E408 Test Method for Thermal Conductivity of Whiteware Ceramics~~

~~E1045 Practice for Calculating Thermal Transmission Properties Under Steady-State Conditions~~

~~D4351 Test Method for Measuring the Thermal Conductivity of Plastics by the Evaporation-Calorimetric Method (Withdrawn 1990)³~~

~~E220 Test Method for Calibration of Thermocouples By Comparison Techniques~~

~~E230 Specification and Temperature-Electromotive Force (EMF) Tables for Standardized Thermocouples~~

~~F433 Practice for Evaluating Thermal Conductivity of Gasket Materials~~

3. Terminology

3.1 Descriptions of Terms and Symbols Specific to This Standard:

3.1.1 Terms:

3.1.1.1 *thermal conductivity, λ* —the time rate of heat flow, under steady conditions, through unit area, per unit temperature gradient in the direction perpendicular to the area;

¹ This test method is under the jurisdiction of ASTM Committee E37 on Thermal Measurements and is the direct responsibility of Subcommittee E37.05 on Thermophysical Properties.

Current edition approved March 15, 2009. Oct. 1, 2013. Published April 2010. November 2013. Originally approved in 1987. Last previous edition approved in 2004. 2009 as E1225—04. E1225—09. DOI: 10.1520/E1225-09.10.1520/E1225-13.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

3.1.1.2 *apparent thermal conductivity*—when other modes of heat transfer through a material are present in addition to conduction, the results of the measurements performed according to this test method will represent the apparent or effective thermal conductivity for the material tested.

3.1.2 Symbols:

$\lambda_{M_1}(T)$	= thermal conductivity of meter bars (reference materials) as a function of temperature, (W/(m·K)),
λ_{M_2}	= thermal conductivity of top meter bar (W/(m·K)),
λ_M	= thermal conductivity of bottom meter bar (W/(m·K)),
$\lambda_S(T)$	= thermal conductivity of specimen corrected for heat exchange where necessary, (W/(m·K)),
$\lambda'_S(T)$	= thermal conductivity of specimen calculated by ignoring heat exchange correction, (W/(m·K)),
$\lambda_I(T)$	= thermal conductivity of insulation as a function of temperature, (W/(m·K)),
T	= absolute temperature (K),
Z	= position as measured from the upper end of the column, (m),
l	= specimen length, (m),
T_i	= the temperature at Z_i , (K),
q'	= heat flow per unit area, (W/m ²),
$\delta\lambda, \delta T$, etc.	= uncertainty in λ, T , etc.,
r_A	= specimen radius, (m),
r_B	= guard cylinder inner radius, (m), and
$T_g(z)$	= guard temperature as a function of position, z , (K).

4. Summary of Test Method

4.1 A test specimen is inserted under load between two similar specimens of a material of known thermal properties. A temperature gradient is established in the test stack and heat losses are minimized by use of a longitudinal guard having approximately the same temperature gradient. At equilibrium conditions, the thermal conductivity is derived from the measured temperature gradients in the respective specimens and the thermal conductivity of the reference materials.

4.2 General Features of Test Method:

4.2.1 The general features of the guarded longitudinal heat flow technique are shown in Fig. 1. A specimen of unknown thermal conductivity, λ_S , but having an estimated thermal conductance of λ_S/l_S , is mounted between two meter bars of known thermal conductivity, λ_M , of the same cross-section and similar thermal conductance, λ_M/l_M . A more complex but suitable arrangement is a column consisting of a disk heater with a specimen and a meter bar on each side between heater and heat sink. Approximately one-half of the power would then flow through each specimen. When the meter bars and specimen are right-circular cylinders of equal diameter the technique is described as the cut-bar method. When the cross-sectional dimensions are larger than the thickness, it is described as the flat slab comparative method. Essentially, any shape can be used, as long as the meter bars and specimen have the same conduction areas.

4.2.2 A force is applied to the column to ensure good contact between specimens. The stack is surrounded by an insulation material of thermal conductivity, λ_I . The insulation is enclosed in a guard shell with a radius, r_B , held at the temperature, $T_g(z)$. A temperature gradient is imposed on the column by maintaining the top at a temperature, T_T , and the bottom at temperature T_B . $T_g(z)$ is usually a linear temperature gradient matching approximately the gradient established in the test stack. However, an isothermal guard with $T_g(z)$ equal to the average temperature of the specimen may also be used. An unguarded system is not recommended due to the potential very large heat losses, particularly at elevated temperatures (1).³ At steady state, the temperature gradients along the sections are calculated from measured temperatures along the two meter bars and the specimen. The value of λ_S , as uncorrected for heat shunting) can then be determined using the following equation where the notation is shown in Fig. 1:

$$\lambda_s = \frac{Z_4 - Z_3}{T_4 - T_3} \cdot \frac{\lambda_M}{2} \left(\frac{T_2 - T_1}{Z_2 - Z_1} + \frac{T_6 - T_5}{Z_6 - Z_5} \right) \quad (1)$$

This is a highly idealized situation, however, since it assumes no heat exchange between the column and insulation at any position and uniform heat transfer at each meter bar-specimen interface. The errors caused by these two assumptions vary widely and are discussed in Section 10. Because of these two effects, restrictions must be placed on this test method, if the desired accuracy is to be achieved.

5. Significance and Use

5.1 The comparative method of measurement of thermal conductivity is especially useful for engineering materials including ceramics, polymers, metals and alloys, refractories, carbons, and graphites including combinations and other composite forms of each.

³The last approved version of this historical standard is referenced on www.astm.org.

³ The boldface numbers in parentheses refer to a list of references at the end of this test method.

FIG. 1

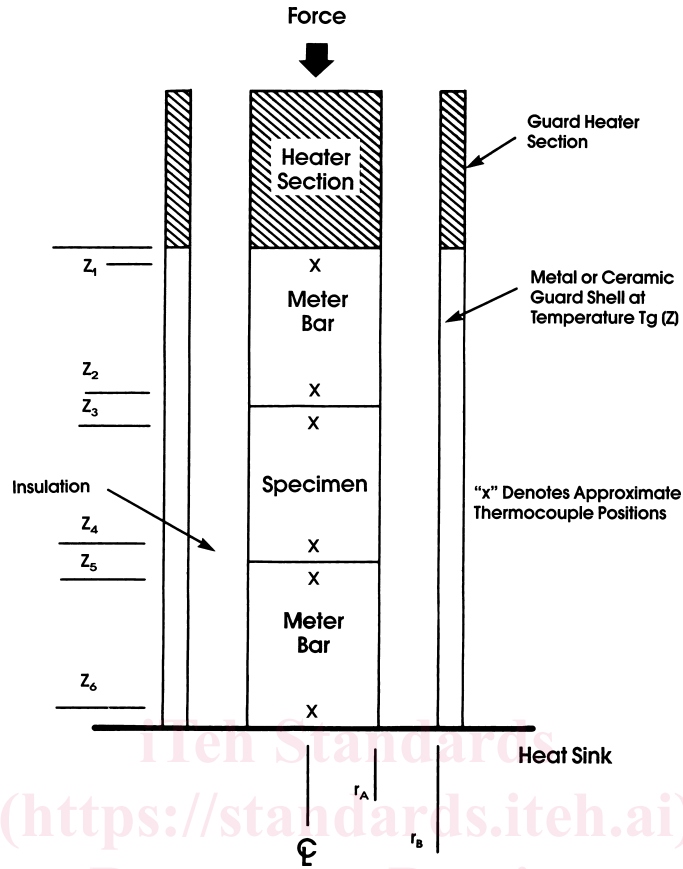


FIG. 1(a) Schematic of a Comparative-Guarded-Longitudinal Heat Flow System Showing Possible Locations of Temperature Sensors

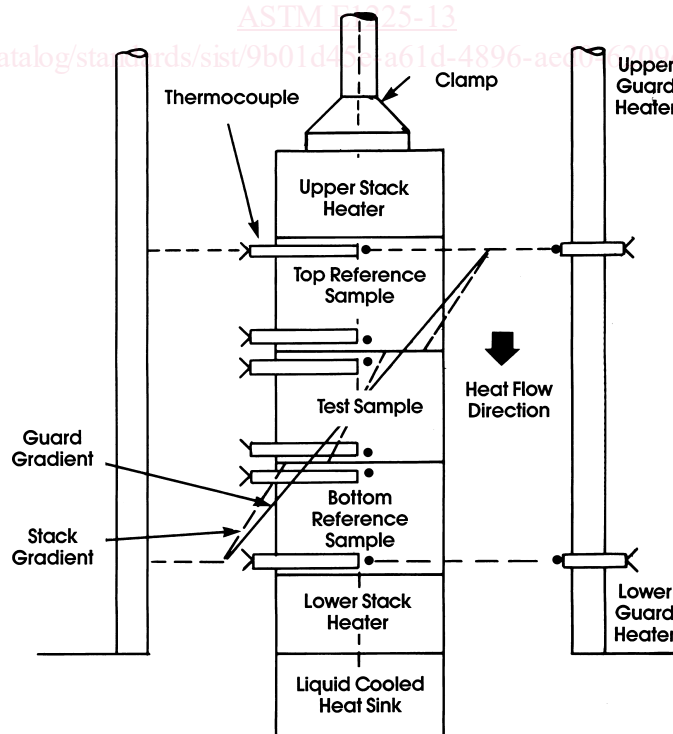
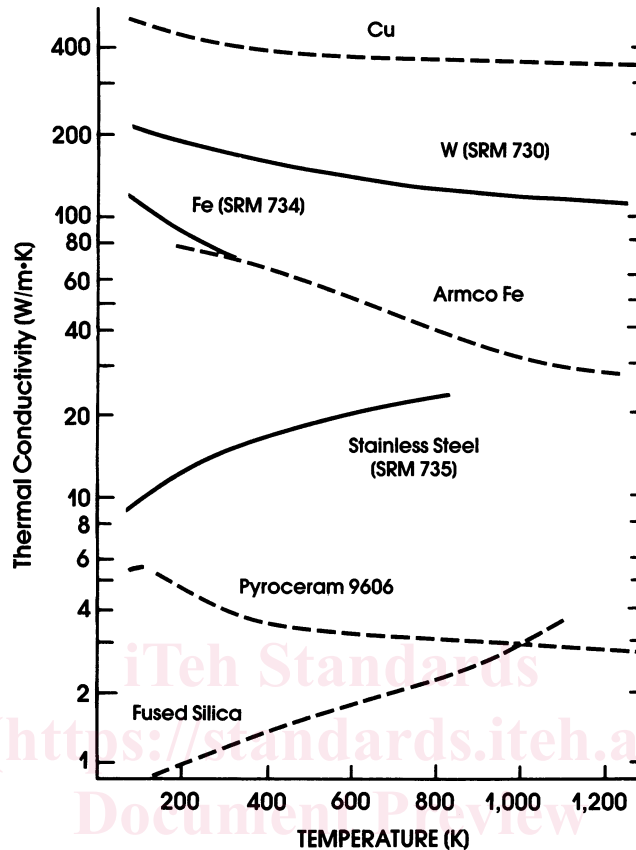


FIG. 1(b) Schematic of Typical Test Stack and Guard System Illustrating Matching of Temperature Gradients



NOTE 1—The material selected for the meter bars should have a thermal conductivity as near as possible to the thermal conductivity of the unknown.

FIG. 2 Approximate Values for the Thermal Conductivity of Several Possible Reference Materials for Meter Bars

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<https://standards.iteh.ai/catalog/standards/sist/9b01d45e-a61d-4896-aed0-6209e33478d4/astm-e1225-13>

5.2 Proper design of a guarded-longitudinal system is difficult and it is not practical in a method of this type to try to establish details of construction and procedures to cover all contingencies that might offer difficulties to a person without technical knowledge concerning theory of heat flow, temperature measurements, and general testing practices. Standardization of this test method is not intended to restrict in any way the future development by research workers of new or methods or improved procedures. However, new or improved techniques must be thoroughly tested. Requirements for qualifying an apparatus are outlined in Section 10.

6. Requirements

6.1 Meter Bar Reference Materials:

6.1.1 Reference materials or transfer standards with known thermal conductivities must be used for the meter bars. Since the minimum measurement error of the method is the uncertainty in λ_M , it is preferable to use standards available from a national standards laboratory, National Metrology Institute. Other reference materials are available because numerous measurements of λ have been made and general acceptance of the values has been obtained. Table 1 lists the currently available recognized reference materials including those available from National Institute of Standards and Technology. some of the recognized reference materials. Fig. 2 shows the approximate variation of λ_M with temperature.

6.1.2 Table 1 is not exhaustive and other materials may be used as references. The reference material and the source of λ_M values shall be stated in the report.

6.1.3 The requirements for any reference material include stability over the temperature range of operation, compatibility with other system components, reasonable cost, ease of thermocouple temperature sensor attachment, and an accurately known thermal conductivity. Since heat shunting errors for a specific λ_f increase as λ_M/λ_s varies from unity, (1) the reference which has a λ_M nearest to λ_s should be used for the meter bars.

6.1.4 If a sample's thermal conductivity λ_s is between the thermal conductivity values of two types of reference materials, the reference material with the higher λ_M should be used to reduce the total temperature drop along the column.

TABLE 1 Reference Materials For Use as Meter Bars

Material	Temperature Range (K)	Percentage Uncertainty in λ (\pm %)	λ_M (W/m·K)	Material-Source
Electrolytic Iron ^A	2 to 1000	2	λ	NIST ^A
Tungsten ^B	4 to 300	2	λ_M Dependent on T^A	NIST ^A
	300 to 2000	2 to 5		
	>2000	5 to 8		
Austenitic Stainless SRM-735	200 to 1200	<5 %	$\lambda_M = 1.22T^{0.432}$	NIST ^A
Iron	80 to 1200	2	λ_M should be calculated from measured values ^{B,C}	---
Copper	90 to 1250	<2	$\lambda_M = 416.3 - 0.05904T + 7.087 \times 10^{-7}T^{3.0}$ <i>E,F,G</i>	manufacturer
Pyroceram ^{Code 9606}	90 to 1270			IRMM, -Belgium
		6 for $T > 300$ K ^F 4 for $T > 300$ K ^G	$\lambda = 2.331 + 515.2T^{-1}$ $\lambda = 3.65367 - 6.64042 \times 10^{-4}T - 218.937T^{-1} + 116163T^{-2}$ $\lambda_M = (84.7/T) + 1.484 + 4.94 \times 10^{-4}T - T + 9.6 \times 10^{-13}T^{4.1}$ <i>E,K</i>	
Fused Silica ^H	1300	<8		manufacturer
Pyrex ⁷⁷⁴⁰	90 to 600 200 to 570	<2 for $T > 200$ K ^K	$\lambda = 1.1036 + 1.659 \times 10^{-3}(T-273.15) - 3.982 \times 10^{-6}(T-273.15)^2 + 6.746 \times 10^{-9}(T-273.15)^3$ <i>K,K</i>	IRMM, -Belgium
		3 for T from 140 K to 200 K ^K		
310 Stainless Steel	300 to 1000	4	$\lambda = 12.338 + 1.781 \times 10^{-2}(T-273.15)^4$	NPL
430 Stainless Steel	300 to 1070	4	$\lambda = 20.159 + 1.589 \times 10^{-2}(T-273.15) - 1.283 \times 10^{-5}(T-273.15)^2$	NPL
Inconel 600	300 to 1000	4	$\lambda = 12.479 + 1.648 \times 10^{-2}(T-273.15) + 3.741 \times 10^{-6}(T-273.15)^2$	NPL
Nimonic 75	300 to 1000	4	$\lambda = 11.958 + 1.657 \times 10^{-2}(T-273.15) + 3.252 \times 10^{-6}(T-273.15)^2$	NPL

TABLE 1 Reference Materials For Use as Meter Bars

Material	Temperature Range (K)	Percentage Uncertainty (\pm %)	Thermal Conductivity (W/m·K)
Electrolytic Iron ^{A,B}	2 to 1000	2	See Table 3.
Tungsten ^C	4 to 300	2	See Table 4.
	300 to 2000	2 to 5	
	>2000	5 to 8	
Austenitic Stainless ^D	200 to 1200	<5 %	See Table 5.
Copper ^E	85 to 1250	<2	$\lambda_M = 416.31 - 0.05904T + 7.0872 \times 10^{-7}T^3$
Pyroceram ^{F,G,H,I,J,K}	298 to 1025 K	6.5 4 for $T > 300$ K	$\lambda = 2.332 + 515.2/T$ $\lambda = 3.65367 - 6.64042 \times 10^{-4}T - 218.937T^{-1} + 116163T^{-2}$ $\lambda_M = (84.7/T) + 1.484 + 4.94 \times 10^{-4}T - T + 9.6 \times 10^{-13}T^4$
Fused Silica ^{L,M}	1300	<8	
Pyrex ^{N,K,O,P,Q}	90 to 600 140 to 470	Up to 900 K <2 for $T > 200$ K	$\lambda = 1.1036 + 1.659 \times 10^{-3}(T-273.15) - 3.982 \times 10^{-6}(T-273.15)^2 + 6.746 \times 10^{-9}(T-273.15)^3$ <i>K</i>
310 Stainless Steel ^{K,R}	300 to 1020	4	$\lambda = 12.338 + 1.781 \times 10^{-2}(T-273.15)$
430 Stainless Steel ^{K,R}	300 to 770	4	$\lambda = 20.159 + 1.589 \times 10^{-2}(T-273.15) - 1.283 \times 10^{-5}(T-273.15)^2$
Inconel 600 ^{S,K,R}	300 to 1020	4	$\lambda = 12.479 + 1.648 \times 10^{-2}(T-273.15) + 3.741 \times 10^{-6}(T-273.15)^2$
Nimonic 75 ^{T,K,R}	300 to 1020	4	$\lambda = 11.958 + 1.657 \times 10^{-2}(T-273.15) + 3.252 \times 10^{-6}(T-273.15)^2$

^ANational SRM 8420 is available from National Institute of Standards and Technology, Washington, D.C. 20234. Technology (NIST), Gaithersburg, MD. ^USee Special Publications 260-52 and 260-46.

^BFulkerson W., et al.; Hurst, J. G., Physics Review and Lankford, 167, p. 765, (1968). A. B., "Report of Investigation, Research Materials 8420 and 8421, Electrolytic Iron, Thermal Conductivity and Electrical Resistivity as a Function of Temperature from 2 to 1000K," National Institutes of Standards and Technology (nee National Bureau of Standards), Gaithersburg, MD, 1984.

^CLueke C. F., Journal Hurst, J. G., and Giarratano, P. J., Certificate, Standard Reference Material 730, *Thermal Conductivity – Tungsten*, National Institutes of Testing and Evaluation, ASTM 1 (5), 422 (1973). Standards and Technology (nee National Bureau of Standards), Gaithersburg, MD, 1976.

^DHurst, J. G., Sparks, L. L., and Giarratano, P. J., Certificate, Standard Reference Material 735, *Thermal Conductivity – Austenitic Stainless Steel*, National Institutes of Standards and Technology (nee National Bureau of Standards), Gaithersburg, MD, USA, 1975.

^EMoore, J. P., Graves, R. S., and McElroy, D. L., "Thermal Conductivity and Electrical Resistivity of High-Purity Copper from 78 to 400 °K," *Canadian Journal of Physics*, 45, 3849 (1967). Vol 45, 1967, pp. 3849–3865.

^F"Thermal Conductivity of Selected Materials," Report NSRDS-NBS 8, National Bureau of Standards, 1966. Pyroceram is a trademark by Corning Incorporated, Corning, NY.

^Q D. R. Salmon, G. Roebben, R. Brandt, 2007. Salmon, D. R., Roebben, G., and Brandt, R., "Certification of Thermal Conductivity and Thermal Diffusivity up to 1025 K of Glass-Ceramic Reference Material BCR-720," EUR Report 21764, IRMM, Geel, Belgium. Institute for Reference Materials and Measurements (IRMM), Geel, Belgium, 2007.

^R D. E. Stroe, M. A. Thermitus, R. A. Stroe, D. E., Thermitus, M. A., and Jacobs - Fedore, in R. A., "Thermophysical Properties of Pyroceram™ 9606," *Thermal Conductivity 27 / Thermal Expansion 15*, H. H. Wang, W. Porter, eds., DEStech Publications, Inc., Lancaster, PA, USA, 2004, 2005, pp. 382-390; 382-390.

^L Hurst J. G., Cryogenics Division, NBS, Boulder, Colorado 80302. BCR-2013 is available from the Institute for Reference Materials and Measurements (IRMM), Geel, Belgium.^U

^Q BCR-724 is available from the Laboratory of the Government Chemists (LGC), Teddington, Middlesex, UK.^U

^R Tye, R. P., and Salmon, D. R., "Development of New Thermal Conductivity Reference Materials: A Summary of Recent Contributions by National Physical Laboratory," *Thermal Conductivity 27 / Thermal Expansion 15*, H. Wang (ed.), DEStech Publications, Lancaster PA, 2005, pp. 372-381.

^L Above 700 K a large fraction of heat conduction in fused silica will be by radiation and the actual effective values may depend on the emittances of bounding surfaces and meter bar size.

^M Recommended values from Table 3017 A-R-2 of the Thermophysical Properties Research Center Data Book, Vol. 3, "Nonmetallic Elements, Compounds, and Mixtures," Purdue University, Lafayette, Indiana.

^N Pyrex is a trademark by Corning Incorporated, Corning, NY.

^O R. P. Tye, D. R. Salmon, in Tye, R. P., and Salmon, D. R., "Thermal Conductivity Certified Reference Materials: Pyrex 7740 and Polymethylmethacrylate," *Thermal Conductivity 26 / Thermal Expansion 14*, 14, Ralph Dinwiddie R. Dinwiddie, ed., DEStech Publications, Inc., Lancaster, PA, USA, 2005, pp. 437-451; 437-451.

^P BCR-39 is available from the Institute for Reference Materials and Measurements (IRMM), Geel, Belgium.^U

^Q Salmon, D., "Thermal Conductivity of Insulations Using Guarded Hot Plates, including Recent Developments and Sources of Reference Materials," *Measurement Science and Technology*, Vol 12, 2001, pp. R89-R98.

^R J. Clark, R. Tye, Clark, J., and Tye, R., "Thermophysical Properties Reference Data for Some Key Engineering Alloy," *High Temperatures - High Pressures*, 2003/2004, volume 35/36, pp. 1-14; Vols 35/36, 2003/2004, pp. 1-14.

^S Inconel is a trademark by Special Metals Corporation, Huntington WV.

^T Nimonic is a trademark by Special Metals Corporation, Huntington WV.

^U This is the sole source of supply of this material known to the committee at this time. If you are aware of alternative suppliers, please provide this information to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

TABLE 3 Thermal Conductivity of Electrolytic Iron^A

Temperature, K	Thermal Conductivity, (W/m·K)
2	12.32
3	18.48
4	24.62
5	30.76
6	36.88
7	42.97
8	49.0
9	55.0
10	61.0
12	72.8
14	84.2
16	95.2
18	105.7
20	115.7
25	137.4
30	153.9
35	164.5
40	169.1
45	168.3
50	163.6
60	149.1
70	134.9
80	123.8
90	115.4
100	108.9
150	92.7
200	86.7
250	81.5
300	76.4
400	67.5
500	60.2
600	53.6
700	47.49
800	41.96
900	37.12
1000	32.98

^A Hurst, J. G., and Lankford, A. B., Report of Investigation, Research Material 8420 and 8421, Electrolytic Iron, Thermal Conductivity and Electrical Resistivity as a Function of Temperature from 2 to 1000K, National Institute of Standards and Technology (nee Bureau of Standards), 1984.

TABLE 4 Thermal Conductivity of Tungsten^A

Temperature, K	Thermal Conductivity, (W/m·K)
4	154
6	231
8	306
10	377
12	444
14	503
16	553
18	591
20	618
30	585
40	438
50	330
60	275
70	245
80	229
90	218
100	211
120	202
140	197
160	194
180	190
200	187
250	180
300	172
350	164
400	157
450	151
500	146
600	138
700	132
800	127
900	123
1000	120
1200	114
1400	110
1600	107
1800	105
2000	102
2200	101
2400	99
2600	98
2800	97
3000	97

^A Hurst, J. G., and Giarratano, P. J., Certificate, Standard Reference Material 730, Thermal Conductivity — Tungsten, National Institute of Standards and Technology (nee National Bureau of Standards), 1976.