

# TECHNICAL REPORT

# IEC TR 62064

First edition  
1999-07

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## **Radio-frequency cables – Relationship between surface transfer impedance and screening attenuation (A background to the recommended limits contained in IEC 61196-1, clause 14)**

*Câblages pour fréquences radioélectriques –  
Relation entre l'impédance de transfert en surface  
et l'affaiblissement d'écran*

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\* See web site address on title page.

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## INTERNATIONAL ELECTROTECHNICAL COMMISSION

**RADIO-FREQUENCY CABLES – RELATIONSHIP BETWEEN SURFACE  
TRANSFER IMPEDANCE AND SCREENING ATTENUATION**  
(A background to the recommended limits contained  
in IEC 61196-1, clause 14)

## FOREWORD

- 1) The IEC (International Electrotechnical Commission) is a worldwide organization for standardization comprising all national electrotechnical committees (IEC National Committees). The object of the IEC is to promote international co-operation on all questions concerning standardization in the electrical and electronic fields. To this end and in addition to other activities, the IEC publishes International Standards. Their preparation is entrusted to technical committees; any IEC National Committee interested in the subject dealt with may participate in this preparatory work. International, governmental and non-governmental organizations liaising with the IEC also participate in this preparation. The IEC collaborates closely with the International Organization for Standardization (ISO) in accordance with conditions determined by agreement between the two organizations.
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Technical reports do not necessarily have to be reviewed until the data they provide are considered to be no longer valid or useful by the maintenance team.

IEC 62064, which is a technical report, has been prepared by subcommittee 46A: Coaxial cables, of IEC technical committee 46: Cables, wires, waveguides, R.F. connectors, and accessories for communication and signalling.

The text of this technical report is based on the following documents:

|               |                  |
|---------------|------------------|
| Enquiry draft | Report on voting |
| 46A/330/CDV   | 46A/348/RVC      |

Full information on the voting for the approval of this technical report can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 3.

This document which is purely informative is not to be regarded as an International Standard.

A bilingual version of this technical report may be issued at a later date.

# RADIO-FREQUENCY CABLES – RELATIONSHIP BETWEEN SURFACE TRANSFER IMPEDANCE AND SCREENING ATTENUATION (A background to the recommended limits contained in IEC 61196-1, clause 14)

## 1 Scope

This technical report describes the valuable background material used during the revision of IEC 61196-1, clause 14, guidance for surface transfer impedance and screening attenuation limits for flexible r.f. cables.

In this report the relationship between surface transfer impedance ( $Z_T$ ) and screening attenuation ( $a_s$ ) is given, also measurements of  $Z_T$  and  $a_s$  are provided to show the correlation of mean scanning attenuation between 200 MHz and 500 MHz and  $Z_T$  at both 30 MHz and 300 MHz.

The sensitivity of  $a_s$  and the relative velocity difference between the inner and outer system is shown, also the need for the cable data sheet to show the  $a_s$  values in a standardized form –  $\Delta v/v = 10\%$  and the characteristic impedance of the outer system is  $150\ \Omega$ . It is also shown that a relative velocity difference change from 10% to 40% gives an improvement of 12 dB in screening attenuation.

## 2 General

At high frequencies when the surface transfer impedance  $Z_T$  and effective transfer impedance  $Z_{TE_{n,f}} = |Z_F \pm Z_T|$ , and increases 6 dB per octave, its relation to the screening attenuation  $a_s$  is frequency independent and can be written as (see also figure 1):

$$a_{s_{n,f}} = -20 \times \log_{10} |T_{n,f}| \tag{1}$$

$$= -20 \times \log_{10} \frac{Z_T}{\sqrt{Z_1 Z_2} \omega \left| \frac{l}{v_2} \pm \frac{l}{v_1} \right|} = -20 \times \log_{10} \frac{Z_T c_0}{\sqrt{Z_1 Z_2} \omega \left| \sqrt{\epsilon_{r2}} \pm \sqrt{\epsilon_{r1}} \right|} \tag{2}$$

$$\text{and } T_{n,f} = \frac{U_{2n} / \sqrt{Z_2}}{U_1 / \sqrt{Z_1}}$$

where

- $l$  is the length of the cable under test;
- $T_{n,f}$  are the coupling transfer functions;
- 'n' for the near end and 'f' for the far end;
- $Z_1$  is the characteristic impedance of the cable;
- $Z_2$  is the impedance of the outer circuit;
- $\epsilon_{r1}$  is the cable dielectric permittivity;
- $\epsilon_{r2}$  is the permittivity of the outer circuit;
- $c_0$  is the velocity of light in vacuum;
- $v_1$  is the propagation velocity of the inner circuit;