



Designation: **D5457 – 15 D5457 – 17**

# Standard Specification for Computing Reference Resistance of Wood-Based Materials and Structural Connections for Load and Resistance Factor Design<sup>1</sup>

This standard is issued under the fixed designation D5457; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reappraisal. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reappraisal.

## INTRODUCTION

Load and resistance factor design (LRFD) is a structural design method that uses concepts from reliability theory and incorporates them into a procedure usable by the design community. The basic design equation requires establishing a reference resistance based on several material property parameters. A standard method for calculating the required material property input data is critical so that all wood-based structural materials can be treated equitably. This specification provides the procedures that are required for the generation of reference resistance for LRFD.

## 1. Scope

1.1 This specification covers procedures for computing the reference resistance of wood-based materials and structural connections for use in load and resistance factor design (LRFD). The format conversion procedure is outlined in Section 4. The test-based derivation procedure is outlined in Annex A1. The reference resistance derived from this specification applies to the design of structures addressed by the load combinations in ASCE 7-10.

1.2 A commentary to this specification is provided in Appendix X1.

1.3 Units—The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are mathematical conversions to SI units that are provided for information only and are not considered standard.

1.4 This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.

## 2. Referenced Documents

2.1 *ASTM Standards:*<sup>2</sup>

D9 Terminology Relating to Wood and Wood-Based Products

D143 Test Methods for Small Clear Specimens of Timber

D198 Test Methods of Static Tests of Lumber in Structural Sizes

D1037 Test Methods for Evaluating Properties of Wood-Base Fiber and Particle Panel Materials

D1761 Test Methods for Mechanical Fasteners in Wood

D1990 Practice for Establishing Allowable Properties for Visually-Graded Dimension Lumber from In-Grade Tests of Full-Size Specimens

D2718 Test Methods for Structural Panels in Planar Shear (Rolling Shear)

D2719 Test Methods for Structural Panels in Shear Through-the-Thickness

D2915 Practice for Sampling and Data-Analysis for Structural Wood and Wood-Based Products

D3043 Test Methods for Structural Panels in Flexure

<sup>1</sup> This specification is under the jurisdiction of ASTM Committee D07 on Wood and is the direct responsibility of Subcommittee D07.02 on Lumber and Engineered Wood Products.

Current edition approved May 1, 2015; Nov. 1, 2017. Published June 2015; December 2017. Originally approved in 1993. Last previous edition approved in 2012 as D5457 – 12; D5457 – 15. DOI: 10.1520/D5457-15.10.1520/D5457-17.

<sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

[D3500 Test Methods for Structural Panels in Tension](#)  
[D3501 Test Methods for Wood-Based Structural Panels in Compression](#)  
[D3737 Practice for Establishing Allowable Properties for Structural Glued Laminated Timber \(Glulam\)](#)  
[D4761 Test Methods for Mechanical Properties of Lumber and Wood-Base Structural Material](#)  
[D5055 Specification for Establishing and Monitoring Structural Capacities of Prefabricated Wood I-Joists](#)  
[D5456 Specification for Evaluation of Structural Composite Lumber Products](#)  
[E105 Practice for Probability Sampling of Materials](#)  
 2.2 *ASCE Standard*.<sup>3</sup>  
[ASCE 7-10 Minimum Design Loads for Buildings and Other Structures](#)

### 3. Terminology

#### 3.1 *Definitions:*

3.1.1 For general definitions of terms related to wood, refer to Terminology [D9](#).

#### 3.2 *Definitions: Definitions of Terms Specific to This Standard:*

3.1.1 For general definitions of terms related to wood, refer to Terminology [D9](#).

3.2.1 *coefficient of variation,  $CV_w$* —a relative measure of variability. ~~For this specification, the calculation of variability  $CV_w$  is based on the shape parameter of the 2-parameter Weibull distribution. It is not the traditional sample standard deviation of the data divided by the sample mean.~~

#### 3.2.1.1 *Discussion—*

~~It is not the traditional sample standard deviation of the data divided by the sample mean.~~

3.2.2 *data confidence factor,  $\Omega$* —a factor that is used to adjust member reference resistance for sample variability and sample size.

3.2.3 *distribution percentile,  $R_p$* —the value of the distribution associated with proportion,  $p$ , of the cumulative distribution function.

3.2.4 *factored resistance,  $\phi R_n$* —the product of the resistance factor and the reference or nominal resistance not including the time effect factor ( $\lambda$ ) and other adjustments for end-use conditions.

3.2.5 *format conversion factor,  $K_F$* —a factor applied to convert resistance from the allowable stress design (ASD) format to the LRFD format.

3.2.6 *lower tail*—a portion of an ordered data set consisting of all test specimens with the lowest property values (for example, lowest strengths).

3.2.7 *nominal resistance*—a term equivalent to the reference resistance used in reliability analysis and LRFD standards.

3.2.8 *reference resistance,  $R_n$* —the design value used in LRFD equations to represent member resistance (that is, strength or capacity) prior to application of the resistance factor, the time effect factor ( $\lambda$ ), and other adjustments for end-use conditions.

#### 3.2.8.1 *Discussion—*

The reference value represents member resistance at 10-minute load duration.

3.2.9 *reliability normalization factor,  $K_R$* —a factor used to establish the reference resistance to achieve a target reliability index for a reference set of conditions.

3.2.10 *resistance factor—factor,  $\phi$* —a factor applied to the resistance side of the LRFD equation.

### 4. Sampling

~~4.1 Samples selected for analysis and implementation with this specification shall be representative of the population about which inferences are to be made. Both manufacturing and material source variability shall be considered. The principles of Practice [E105](#) shall be maintained. Practice [D2915](#) provides methods for establishing a sampling plan. Special attention is directed to sampling procedures in which the variability is low and results can be influenced significantly by manufacturing variables. It is essential that the sampling plan address the relative magnitude of the sources of variability.~~

~~4.1.1 Data generated from a quality control program shall be acceptable if the criteria of [4.1](#) are maintained.~~

~~4.1.2 When data from multiple data sets are compiled or grouped, the criteria used to group such data shall be in keeping with the provisions of [4.1](#). When such procedures are available in applicable product standards, they shall be used.~~

#### ~~4.2 *Sample Size:*~~

<sup>3</sup> Available from The American Society of Civil Engineers (ASCE), 1801 Alexander Bell Dr., Reston, VA 20191.

4.2.1 For data sets in which all specimens are tested to failure, the minimum sample size shall be 30.

NOTE 1—The confidence with which population properties can be estimated decreases with decreasing sample size. For sample sizes less than 60, extreme care must be taken during sampling to ensure a representative sample.

4.2.2 For lower tail data sets, a minimum of 60 failed observations is required for sample sizes of  $n = 600$  or less. (This represents at least the lower 10 % of the distribution.) For sample sizes greater than 600, a minimum of the lowest 10 % of the distribution is required (for example, sample size,  $n = 720$ ,  $0.10(720) = 72$  failed test specimens in the lower tail). Only parameter estimation procedures designed specifically for lower tail data sets shall be used (see [Appendix X2](#)).

## 5. Testing

5.1 Testing shall be conducted in accordance with appropriate standard testing procedures. The intent of the testing shall be to develop data that represent the capacity of the product in service.

5.2 *Periodic Property Assessment*—Periodic testing is recommended to verify that the properties of production material remain representative of published properties.

## 4. Reference Resistance for LRF $\bar{D}$

6.1 The derivation of LRF $\bar{D}$  reference resistance is addressed in this section. Parameters required for the derivation of reference resistance are also presented. These parameters include the distribution percentile, coefficient of variation, data confidence factor, and reliability normalization factor. An example derivation of reference resistance is provided in [X1.7](#).

6.2 *Reference Resistance,  $R_n$* —The following equation establishes reference resistance for LRF $\bar{D}$ :

$$R_n = R_p \times \Omega \times K_R \quad (1)$$

where:

$R_p$  = distribution percentile estimate;  
 $\Omega$  = data confidence factor, and  
 $K_R$  = reliability normalization factor.

4.1 *Distribution Percentile Estimate,  $R_p$* —Reference resistance for LRF $\bar{D}$  shall be determined using one of the following procedures:

4.1.1 [Eq 2](#) is intended to be used to calculate any percentile of a two-parameter Weibull distribution. The percentile of interest depends on the property being estimated; or

$$R_p = \eta[-\ln(1-p)]^{1/\alpha} \quad (2)$$

where:

$\eta$  = Weibull scale parameter,  
 $p$  = percentile of interest expressed as a decimal (for example, 0.05), and  
 $\alpha$  = Weibull shape parameter.

4.1.2 The shape ( $\alpha$ ) and scale ( $\eta$ ) parameters of the two-parameter Weibull distribution shall be established to define the distribution of the material resistance. Algorithms for common estimation procedures are provided in [Appendix X2 Annex A1](#).

6.4 *Coefficient of Variation,  $CV_w$* —The coefficient of variation of the material is necessary when determining the data confidence factor,  $\Omega$ , and the reliability normalization factor,  $K_R$ . The  $CV_w$  can be estimated from the shape parameter of the Weibull distribution as follows:

$$CV_w \cong \alpha^{-0.92} \quad (3)$$

NOTE 2—The above approximation is within 1 % of the exact solution for  $CV_w$  values between 0.09 and 0.50. An exact relationship of  $CV_w$  and  $\alpha$  is shown in [Appendix X3](#).

6.5 *Data Confidence Factor,  $\Omega$* —The data confidence factor,  $\Omega$ , accounts for uncertainty associated with data sets.<sup>5</sup> This factor, which is a function of coefficient of variation, sample size, and reference percentile, is applied as a multiplier on the distribution estimate. [Table 1](#) provides data confidence factors appropriate for lower fifth-percentile estimates.

NOTE 3—When a distribution tolerance limit is developed on a basis consistent with  $\Omega$ , the data confidence factor is taken as unity.

6.6 *Reliability Normalization Factor,  $K_R$* —The reliability normalization factor,  $K_R$ , is used to adjust the distribution estimate (for example,  $R_{0.05}$ ) to achieve a target reliability index. The reliability normalization factor is the ratio of the computed resistance factor,  $\phi_c$  ([X1.7](#)), to the specified resistance factor,  $\phi_s$  ([Table 2](#)), adjusted by a scaling factor. This adjustment factor is a function of  $CV_w$  and is generated for specific target reliability indices. The  $K_R$  values presented in [Table 3](#) represent resistance factors ( $\phi_c$ ) computed at a live-to-dead load ratio of 3. Computations for determining reliability normalization factors for target reliability indices greater than  $\beta = 2.4$  are contained in Zahn.<sup>6</sup>

4.2 *Format Conversion: Conversion Procedure:*

4.2.1 As an alternative to the use of Resistance  $K_R$ , in which one chooses to adjust the design values to achieve a stated reliability index under the reference load conditions, it is permissible to generate LRFD reference resistance values for LRFD are permitted to be based on format conversion from code-recognized allowable stress design (ASD). It shall not be claimed that reference resistance values generated in this manner achieve a stated reliability index. Resistance factors for determining LRFD factored resistance,  $\phi R_n$ , are given in Table 1.

NOTE 1—Examples of standards that are used to generate code-recognized ASD values include Test Methods D143, D198, D1037, D1761, D2718, D2719, D3043, D3500, D3501, and D4761; Practices D1990 and D3737; and Specifications D5055 and D5456.

4.2.2 For standardization purposes, format conversion reference resistance values shall be based on the arithmetic conversion at a specified reference condition that results from the calibration (defined as providing an identical required section modulus, cross-sectional area, allowable load capacity, and so forth) of basic ASD and LRFD equations. The specified reference condition shall be chosen such that changes in design capacity over the range of expected load cases and load ratios is minimized.

4.2.3 Values of the format conversion factor,  $K_F$ , are given in Table 42.

4.2.4 The format conversion reference resistance is computed by multiplying the ASD resistance by  $K_F$ . For members and connections, the ASD resistance is based on a normal (10-year) load duration. For shear walls and diaphragms, the ASD resistance is based on a 10-minute load duration.

4.2.5 For lateral buckling (stability), compression perpendicular to grain, and rolling shear that is not subject to load duration or time effect adjustments, the value of  $K_F$  is based on the assumption that neither the ASD nor LRFD resistance values are modified by duration of load or time effect adjustments.

4.2.6 *Format Conversion Example*—An ASD bolt design value for a single shear connection,  $F_v$  is 800 lbf (3.56 kN) (based on normal 10-year load duration). From Table 42, the format conversion factor,  $K_F$ , is 3.32. The corresponding LRFD bolt reference resistance value is as follows:

$$R_n = 3.32 \times 800 \tag{1}$$

$$R_n = 2658 \text{ lbf}$$

$$R_n = K_F \times F_v = 3.32 \times 800 = 2658 \text{ lbf (11.82 kN)} \tag{1}$$

4.2.7 *Format Conversion Example for Shear Walls or Diaphragms*—An ASD shear wall design value,  $F_v$  is 395 lb/ft (5.76 kN/m) (based on a 10-minute load duration). From Table 42, the format conversion factor,  $K_F$ , is 2.00. The corresponding LRFD shear wall reference resistance value is as follows:

$$R_n = 2.00 \times 395 \tag{2}$$

$$R_n = 790 \text{ lb/ft}$$

$$R_n = K_F \times F_v = 2.00 \times 395 = 790 \text{ lb/ft (11.53 kN/m)} \tag{2}$$

7. Presentation of Results

7.1 Report the sampling plan and testing in accordance with applicable standards. When lower tail data sets are used, report the sample size and data used in the calculations. Report the estimated shape and scale parameters along with the calculated coefficient of variation. When appropriate, also report the mean and standard deviation (derived from the calculated coefficient of variation). Include a plot showing the data points and fitted Weibull distribution. In addition to these basic parameters, also report the data confidence factor, calculated percentile estimate, reliability normalization factor, and reference resistance.

5. Keywords

5.1 format conversion; load and resistance factor design (LRFD); reference resistance; structural connections; test-based derivation; wood-based materials

TABLE 1 Specified LRFD Resistance Factors,  $\phi_s$

Application	Property	$\phi_s$
Members	compression <sup>A</sup>	0.90
	bending, lateral buckling (stability)	0.85
	tension parallel	0.80
	shear, radial tension	0.75
Connections	all	0.65
	Shear Walls, diaphragms	shear

<sup>A</sup> Compression parallel-to-grain, compression perpendicular-to-grain, and bearing.

**TABLE 2 Format Conversion Factor,  $K_F$** 

Property	$K_F$
Compression Parallel to Grain	2.40
Bending	2.54
Tension Parallel to Grain	2.70
Shear	2.88 <sup>A</sup>
Radial Tension	2.88
Connections	3.32
Lateral Buckling (Stability)	1.76
Compression Perpendicular to Grain	1.67
Shear Wall and Diaphragm Shear	2.00 <sup>B</sup>

<sup>A</sup> The value of the format conversion factor is 2.00 where shear is not subject to load duration or time effect adjustments (e.g., rolling shear in cross-laminated timber).

<sup>B</sup> The format conversion factor for shear wall and diaphragm shear is only intended to be applied to the design capacity of shear wall or diaphragm assemblies, not to the design of individual members or subcomponents of these assemblies.

## ANNEX

### (Mandatory Information)

#### A1. TEST-BASED DERIVATION OF REFERENCE RESISTANCE FOR LRFD

A1.1 Parameters required for the derivation of reference resistance are presented in this Annex. These parameters include the distribution percentile,  $R_p$ , coefficient of variation,  $CV_w$ , data confidence factor,  $\Omega$ , and reliability normalization factor,  $K_R$ . An example derivation of reference resistance is provided in X1.8.5.

#### A1.2 Sampling:

A1.2.1 Samples selected for analysis and implementation with this specification shall be representative of the population about which inferences are to be made. Both manufacturing and material source variability shall be considered. The principles of Practice E105 shall be maintained. Practice D2915 provides methods for establishing a sampling plan. Special attention is directed to sampling procedures in which the variability is low and results can be influenced significantly by manufacturing variables. It is essential that the sampling plan addresses the relative magnitude of the sources of variability.

A1.2.1.1 Data generated from a quality control program shall be acceptable if the criteria of A1.2.1 are maintained.

A1.2.1.2 Multiple Data Sets—When data from multiple data sets are compiled or grouped, the criteria used to group such data shall be in accordance with the provisions of A1.2.1. When such procedures are available in applicable product standards, they shall be used.

#### A1.2.2 Sample Size:

A1.2.2.1 For data sets in which all specimens are tested to failure, the minimum sample size shall be 30.

NOTE A1.1—The confidence with which population properties can be estimated decreases with decreasing sample size. For sample sizes less than 60, extreme care must be taken during sampling to ensure a representative sample.

A1.2.2.2 For lower tail data sets, a minimum of 60 failed observations is required for sample sizes of  $n = 600$  or less. This represents at least the lower 10 % of the distribution. For sample sizes greater than 600, a minimum of the lowest 10 % of the distribution is required. For example, sample size,  $n = 720$ ,  $0.10 (720) = 72$  failed test specimens in the lower tail. Only parameter estimation procedures designed specifically for lower tail data sets shall be used (see Appendix X2).

#### A1.3 Testing:

A1.3.1 Testing shall be conducted in accordance with appropriate standard testing procedures. The intent of the testing shall be to develop data that represent the capacity of the product under standard conditions.

A1.3.2 Periodic Property Assessment—Periodic testing is recommended to verify that the properties of production material remain representative of published properties.

A1.4 Reference Resistance,  $R_n$ —The following equation establishes reference resistance for LRFD:

$$R_n = R_p \times \Omega \times K_R \quad (\text{A1.1})$$

where:

$R_p$  = distribution percentile estimate,  
 $\Omega$  = data confidence factor, and  
 $K_R$  = reliability normalization factor.

A1.4.1 Distribution Percentile Estimate,  $R_p$ :

A1.4.2 Eq A1.2 is intended to be used to calculate any percentile of a two-parameter Weibull distribution. The percentile of interest depends on the property being estimated.

$$R_p = \eta [-\ln(1 - p)]^{1/\alpha} \quad (\text{A1.2})$$

where:

$\eta$  = Weibull scale parameter,  
 $p$  = percentile of interest expressed as a decimal (for example, 0.05), and  
 $\alpha$  = Weibull shape parameter.

A1.4.3 The shape ( $\alpha$ ) and scale ( $\eta$ ) parameters of the two-parameter Weibull distribution shall be established to define the distribution of the material resistance (1).<sup>4</sup> Algorithms for common estimation procedures are provided in Appendix X2.

A1.4.4 Coefficient of Variation,  $CV_w$ —The coefficient of variation of the material is necessary when determining the data confidence factor,  $\Omega$ , and the reliability normalization factor,  $K_R$ . The  $CV_w$  can be estimated from the shape parameter of the Weibull distribution as follows:

$$CV_w \cong \alpha^{-0.92} \quad (\text{A1.3})$$

NOTE A1.2—The above approximation is within 1 % of the exact solution for  $CV_w$  values between 0.09 and 0.50. An exact relationship of  $CV_w$  and  $\alpha$  is shown in Appendix X3.

A1.5 Data Confidence Factor,  $\Omega$ —The data confidence factor,  $\Omega$ , accounts for uncertainty associated with data sets (2). This factor, which is a function of coefficient of variation, sample size, and reference percentile, is applied as a multiplier on the distribution estimate. Table A1.1 provides data confidence factors appropriate for lower fifth-percentile estimates.

NOTE A1.3—When a distribution tolerance limit is developed on a basis consistent with  $\Omega$ , the data confidence factor is taken as unity.

A1.6 Reliability Normalization Factor,  $K_R$ —The reliability normalization factor,  $K_R$ , which is a function of  $CV_w$  and is generated for specific target reliability indices, is used to adjust the distribution estimate (for example,  $R_{0.05}$ ) to achieve a target reliability index. The reliability normalization factor is the ratio of the computed resistance factor,  $\phi_c$  (X1.8.5), to the specified resistance factor,  $\phi_s$  (Table 1), adjusted by a scaling factor, which is a function of  $CV_w$  and is generated for specific target reliability indices. The  $K_R$  values presented in Table A1.2 were computed at a live-to-dead load ratio of 3. Computations for determining reliability normalization factors for target reliability indices  $\beta > 2.4$  are contained in Ref (3).

<sup>4</sup> Weibull, W., "A Statistical Theory of the Strength of Materials," *Proceedings of the Royal Swedish Institute of Engineering Research*, Stockholm, Sweden, Report No. 151, 1939, pp. 1–45. The boldface numbers in parentheses refer to a list of references at the end of this standard.

**TABLE 1A1.1 Data Confidence Factor,  $\Omega$  on  $R_{0.05}$ , for Two-Parameter Weibull Distribution with 75 % Confidence<sup>A</sup>**

$CV_w$	Sample Size, $n$									
	30	40	50	60	100	200	500	1000	2000	5000
0.10	0.95	0.95	0.96	0.96	0.97	0.98	0.99	0.99	0.99	1.0
0.15	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	0.99	0.99
0.20	0.89	0.91	0.92	0.93	0.94	0.96	0.98	0.98	0.99	0.99
0.25	0.87	0.88	0.90	0.91	0.93	0.95	0.97	0.98	0.98	0.99
0.30	0.84	0.86	0.88	0.89	0.92	0.94	0.96	0.97	0.98	0.99
0.35	0.81	0.84	0.86	0.87	0.90	0.93	0.96	0.97	0.98	0.99
0.40	0.79	0.81	0.84	0.85	0.89	0.92	0.95	0.96	0.97	0.98
0.45	0.76	0.79	0.82	0.85	0.87	0.91	0.94	0.96	0.97	0.98
0.50	0.73	0.77	0.80	0.81	0.86	0.90	0.94	0.95	0.97	0.98

<sup>A</sup> Interpolation is permitted. For  $CV_w$  values below 0.10, the values for 0.10 shall be used.

A1.7 Presentation of Results:

A1.7.1 Report the sampling plan and testing in accordance with applicable standards. When lower tail data sets are used, report the sample size and data used in the calculations. Report the estimated shape and scale parameters along with the calculated coefficient of variation. When appropriate, also report the mean and standard deviation (derived from the calculated coefficient of variation). Include a plot showing the data points and fitted Weibull distribution. In addition to these basic parameters, also report the data confidence factor,  $\Omega$ , calculated percentile estimate,  $R_p$ , reliability normalization factor,  $K_R$ , and reference resistance,  $R_m$ .

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**TABLE 2 Specified LRFD Resistance Factors,  $\phi_s$** 

Application	Property	$\phi_s$
Member	compression <sup>Δ</sup>	0.90
	bending, lateral buckling (stability)	0.85
	tension parallel	0.80
	shear, radial tension	0.75
Connection	all	0.65
	Shear Wall, diaphragm	0.80

<sup>Δ</sup>Compression parallel-to-grain, compression perpendicular-to-grain, and bearing.

**TABLE 3 Fifth-Percentile Based-A1.2 Fifth-Percentile-Based Reliability Normalization Factors,  $K_{FR}$** 

$CV_w, \%$	$K_{FR}$					
	Compression and Bearing	Bending	Tension Parallel	Shear (2.1 basis)	Shear (SCL, 3.15 basis)	Shear (I-Joist, 2.37 basis)
10	1.303	1.248	1.326	1.414	0.943	1.253
11	1.307	1.252	1.330	1.419	0.946	1.257
12	1.308	1.253	1.331	1.420	0.947	1.258
13	1.306	1.251	1.329	1.418	0.945	1.256
14	1.299	1.244	1.322	1.410	0.940	1.249
15	1.289	1.235	1.312	1.400	0.933	1.240
16	1.279	1.225	1.302	1.388	0.926	1.230
17	1.265	1.212	1.288	1.374	0.916	1.217
18	1.252	1.199	1.274	1.359	0.906	1.204
19	1.237	1.185	1.259	1.343	0.895	1.190
20	1.219	1.168	1.241	1.324	0.882	1.173
21	1.204	1.153	1.225	1.307	0.871	1.158
22	1.186	1.136	1.207	1.287	0.858	1.141
23	1.169	1.120	1.190	1.269	0.846	1.125
24	1.152	1.104	1.173	1.251	0.834	1.109
25	1.135	1.087	1.155	1.232	0.821	1.092
26	1.118	1.071	1.138	1.214	0.809	1.076
27	1.105	1.059	1.125	1.200	0.800	1.063
28	1.084	1.038	1.103	1.176	0.784	1.042
29	1.066	1.021	1.085	1.157	0.771	1.025
30	1.049	1.005	1.068	1.139	0.759	1.009

## APPENDIXES

<https://standards.iteh.ai/catalog/standards/sist/dbdf6bb9-aa50-421a-9973-291e5f8bf803/astm-d5457-17>  
 (Nonmandatory Information)

### X1. COMMENTARY TO THE TEXT

#### X1.1 *Commentary to the Introduction: Commentary to the Introduction:*

X1.1.1 Load and resistance factor design (LRFD) is a subset of a broader design methodology known as reliability-based design (RBD). The distinction between the two design procedures is significant. RBD implies, and often calculates, quantities related to the reliability of a member under a given set of conditions for a given reference period. A higher reliability corresponds to a lower probability of failure. One practical concern that arises when one attempts to apply RBD to real structural applications is that the calculations must idealize both the loads and the structural system response to reduce it to a mathematically tractable problem. This idealization process reduces the final calculation to a theoretically interesting, but often inapplicable, number. LRFD was developed by selecting a few of the basic concepts of RBD and using them to develop a format that is similar in many ways to current (allowable stress) design. LRFD provides incremental improvements in the design process in this way. The improvements provided by LRFD include the following:

X1.1.1.1 Consideration of the variability of various types of loads when assessing safety factors.

X1.1.1.2 Consideration of the consequences of various potential failure modes in a structure.

X1.1.1.3 Material resistance values that relate more closely to test data (member capacities).

X1.1.1.4 Consideration of resistance variability.



X1.1.2 Previous standards for developing allowable properties for many types of wood-based products directed the user to various ways of computing a population lower fifth-percentile estimate. This single number was the basis for an allowable strength property assignment. At the other extreme, a realistic RBD would require an accurate definition of a large portion of the lower tail of the material distribution and a large portion of the upper tail of the load distribution. LRFD requires somewhat more information than current procedures (for example, reference values and variability) but substantially less than RBD. In the most advanced LRFD procedures in use today, one needs only a distribution type and the parameters that describe that distribution. Refinements of these procedures suggest that estimates of the distribution and its parameters give the most accurate reliability estimates when they represent a tail portion of the distribution rather than the full distribution. This reflects the fact that, for common building applications, only the lower tail of the resistance and upper tail of the load distribution contribute to failure probabilities.

X1.1.3 Simulations have shown that the assumed distribution type can have a strong effect on computed LRFD resistance factors. However, much of this difference is due to the inability of standard distribution forms to fit the tail data precisely. By standardizing the distribution type, this procedure provides a consistent means for deriving these factors. In addition, by permitting tail fitting of the data, it provides a way of fitting data in this important region that is superior to full-distribution types.

X1.1.4 While the two-parameter Weibull distribution is the underlying basis for these calculations, the user of this specification is not burdened with applying statistical decisions. For LRFD purposes, the user must calculate the shape and scale parameters for the fitted Weibull distribution using the equations in the specification. All remaining steps in the calculations of a reference resistance are spelled out in the equations of the specification.

X1.2 *Commentary to Section 1, Scope*—~~Commentary to Section The 1, Scope~~—The calculation procedures identified in this specification are common statistical procedures. This specification gives the user a document for all calculations necessary to develop LRFD reference resistances. Format conversion per Section 4.2 and test-based derivation per Annex A1 represent two separate approaches for determination of reference resistance for LRFD. Due to the sensitivity of reliability to changes in some of the parameters, these procedures offer a limited set of options to ensure that LRFD reference resistances are generated in a consistent manner. Other methods for computing reference resistance that are beyond the scope of this standard are discussed in Appendix X4.

X1.3 *Commentary to Section 3, Terminology: Commentary to 4.1*—~~Some wood-based products exhibit extremely low variability when tested on a batch basis. On this basis, one would compute, for example, a fifth percentile that may be as high as 90 % of the mean value, as compared with a computed fifth percentile that may be less than 50 % of the mean value for a product with a substantially higher variability. The warning provided in this section is intended to caution the user of this specification to be certain that either the sampling plan or the daily quality control procedures are sufficiently sensitive to reflect population shifts caused by factors such as subtle manufacturing changes or shifts in material sources.~~

X1.3.1 The term “coefficient of variation” is specifically defined in terms related to the shape parameter of a 2-parameter Weibull distribution as used in Annex A1.

X1.3.2 The term “factored resistance” is specifically defined to differentiate it from the nominal (reference) resistance.

X1.3.3 The term “nominal resistance” is the most widely used term in reliability analysis and material specifications.

X1.3.4 *Commentary to 4.1.2*—~~Some test programs include a large number of replications of a single test cell. However, it is more common to develop a testing plan that includes a small number of replications in each test cell, repeating the testing across several configurations. For example, a joist hanger manufacturer might test less than ten replications of a given configuration, but the test is repeated across a range of wood species or hanger depths, or both. For such cases, it is advantageous to be able to pool the data. The term “reference resistance” is retained as the primary terminology in this version of the standard for continued compatibility with the NDS from (4) the various test cells to minimize the data confidence penalty. One technique for verifying the appropriateness of pooling across several test cells is to conduct pairwise significance tests using the Student “T” test. For this test, it is proposed that the minimum significance level be established at the 0.10 level. Another technique often used for data pooling is regression analysis and other design documents, but its definition is clarified to indicate that it does not include the resistance factor ( $\phi$ ), the time-effect factor ( $\lambda$ ) and other adjustments for end-use conditions that will be subsequently applied in the design checking equation.~~

X1.4 *Commentary to Section 4.2, Format Conversion—Commentary to Section 5, Testing*—While the most desirable and reliable method of defining reference resistance for a given property is by the direct testing of representative materials, estimation methods may be used when such data are not available. The preferred method of defining the characteristics for missing data is through the use of a known physical relationship. For example, Weibull’s theory is the method can be used to estimate reference resistance values for untested sizes of a certain product. Statistical relationships may be used in the case in which data used to develop format conversion factors to adjust reference ASD design values (based on normal 10-year load duration) to LRFD reference resistances (based on 10-minute load duration). Format conversion factors in Table 2 are missing and no sufficiently reliable physical relationship exists. Linear or nonlinear curve fitting methods can be applied to define the statistical relationship between a given property and the developed to provide similar member and connection sizes when considering specific ASD and LRFD load cases and specified values of the resistance factor,  $\phi$ , for LRFD as provided in Table 1 influencing variables.

X1.5 *Commentary to Table 2, Format Conversion Factor,  $K_F$ , for Compression Parallel to Grain, Bending, Tension Parallel to Grain, Shear, Radial Tension and Connections: Commentary to Section 6, Reference Resistance for LRFD:*

X1.5.1 The basis for establishing many of the allowable stresses for wood-based products has traditionally focused on the population lower fifth percentile. The primary emphasis of this section is on these types of values. Some classes of products or types of stresses (that is, connections and compression perpendicular to grain) have established stresses based on an average (or mean) value or based on serviceability criteria rather than an ultimate limit, or both, in the past. Regardless of past procedures, a resistance distribution is necessary for a reliability-based procedure.

X1.5.1 Eq X1.10 is the equivalent result of two alternative derivations. In what is referred to as the second derivation, the precise factor of 2.16 happens to Eq X1.10 is based on a graph be the algebraic solution for the ratio of  $R_n/F_x$  that was generated across a range of load ratios for three distinct live-load cases (occupancy floor, snow roof, and non-snow roof), where for  $RL/D_n = 3$ ,  $\lambda = 0.80$ , and  $FK_{wd}$  come directly from the LRFD and ASD design equations: = 1.15.

$$LRFD: \lambda \phi R_n \geq 1.2 D + 1.6 L \tag{X1.1}$$

$$ASD: K_d F_x \geq D + L$$

$$LRFD: \lambda \phi R_n > 1.2 D + 1.6 L \tag{X1.1}$$

$$ASD: K_d F_x > D + L$$

where:

- $\lambda$  = time effect factor,
- $\phi$  = resistance factor,
- $\phi$  = resistance factor,
- $R_n$  = reference resistance,
- $D, L$  = dead and live load effects, respectively,
- $K_d$  = load duration factor (ASD), and
- $F_x$  = allowable stress (ASD);
- $F_x$  = allowable value (ASD).

Substituting and solving for  $K_F$ :

$$K_F = 2.16/\phi, \tag{X1.2}$$

X1.5.2 Use of a single constant for the format conversion factor,  $K_F$ , is appropriate, based on the judgment of the committee, over a broad range of design cases. As shown in Fig. X1.1, this judgment produces exact calibration between ASD and LRFD at the reference condition. Differences between ASD and LRFD designs result for cases not associated with the reference condition. The algebraic format conversion solution for the precise constant in the numerator of Eq X1.2 is not to be confused as the RBD basis supporting Eq X1.2 (see Commentary to Annex A1 factor). The RBD basis of the format conversion factor involved first order, second moment reliability methods to graph  $R_n/F_x$  across a range of load ratios for three distinct live-load cases (occupancy floor, snow roof, and non-snow roof), where  $R_n$  and  $F_x$  come directly from the LRFD and ASD design equations. The factor in the numerator of Eq X1.10 X1.2 is in the range from 2.1 to 2.2 and resulted from the application of engineering judgment as a balance of increases for floors at low L/D ratios versus decreases for non-snow roofs at higher L/D ratios.