
Kovinski materiali - Enotna preskusna metoda za določanje kvazistatične lomne žilavosti (ISO 12135:2021)

Metallic materials - Unified method of test for the determination of quasistatic fracture toughness (ISO 12135:2021)

Metallische Werkstoffe - Vereinheitlichtes Prüfverfahren zur Bestimmung der quasistatischen Bruchzähigkeit (ISO 12135:2021)

Matériaux métalliques - Méthode unifiée d'essai pour la détermination de la ténacité quasi statique (ISO 12135:2021)

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77.040.10 Mehansko preskušanje kovin Mechanical testing of metals

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EN ISO 12135

July 2026

ICS 77.040.10

English Version

**Metallic materials - Unified method of test for the
determination of quasistatic fracture toughness (ISO
12135:2021, including corrected version 2022-08)**

Matériaux métalliques - Méthode unifiée d'essai pour
la détermination de la ténacité quasi statique (ISO
12135:2021, y compris version corrigée 2022-08)

Metallische Werkstoffe - Vereinheitlichtes
Prüfverfahren zur Bestimmung der quasistatischen
Bruchzähigkeit (ISO 12135:2021, einschließlich
korrigierte Fassung 2022-08)

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European foreword

The text of ISO 12135:2021, including corrected version 2022-08 has been prepared by Technical Committee ISO/TC 164 "Mechanical testing of metals" of the International Organization for Standardization (ISO) and has been taken over as EN ISO 12135:2026 by Technical Committee CEN/TC 459/SC 1 "Test methods for steel (other than chemical analysis)" the secretariat of which is held by AFNOR.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by January 2027, and conflicting national standards shall be withdrawn at the latest by January 2027.

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INTERNATIONAL STANDARD

ISO
12135

Third edition
2021-07

Corrected version
2022-08

Metallic materials — Unified method of test for the determination of quasistatic fracture toughness

*Matériaux métalliques — Méthode unifiée d'essai pour la
détermination de la ténacité quasi statique*

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 164, *Mechanical testing of metals*, Subcommittee SC 4, *Fatigue, fracture and toughness testing*.

This third edition cancels and replaces the second edition (ISO 12135:2016), which has been technically revised.

The main changes compared to the previous edition are as follows:

- formulae to calculate CTOD have been replaced with those based on rigid rotation assumption throughout; replacing the previous *R*-curve formulae based on CTOD from *J*. CTOD formulae for SENBs are now those based on recent research to include the material yield to tensile strength ratio in the CTOD formulae;
- the determination of *J* directly from displacement defined in terms of CMOD has been included, in addition to the methods based on load line displacement;
- where fatigue precrack straightness requirements cannot be met due to internal residual stresses, the application of modification techniques, originally developed for weld specimens, is now permitted;
- the rotation correction factor for compact specimens has been revised with a new formula;
- editorial changes have been made to improve consistency of terms and definitions used throughout the document.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

This corrected version of ISO 12135:2021 incorporates the following corrections:

- in [Figure 6](#) a) the envelope tip angle was corrected from 60° to 30°;

- in [7.3.1](#), [Formula \(35\)](#) was corrected, with the addition of " Δ " before " a ", to read:

$$J = \left[\frac{F \cdot S}{(B \cdot B_N)^{0,5} W^{1,5}} g_1 \left(\frac{a_0}{W} \right) \right]^2 \cdot \frac{1-v^2}{E} + \frac{\eta_p U_p}{B_N (W-a_0)} \cdot \left[1 - \frac{\gamma_p \cdot \Delta a}{(W-a_0)} \right];$$

- in [7.3.2](#), [Formula \(38\)](#) was corrected, with the deletion of "+z", to read:

$$\delta = \left[\frac{F \cdot S}{(B \cdot B_N)^{0,5} W^{1,5}} g_1 \left(\frac{a_0}{W} \right) \right]^2 \cdot \frac{1-v^2}{mR_{p0,2}E} + \frac{(1-r_p)\Delta a + r_p B_N}{(1-r_p)\Delta a + r_p B_N + a_0} \cdot V_p;$$

- in [7.3.2](#), [Formula \(43\)](#) was corrected, with the deletion of "+z", to read:

$$\delta = \left[\frac{F}{(B \cdot B_N \cdot W)^{0,5}} g_2 \left(\frac{a_0}{W} \right) \right]^2 \cdot \frac{1-v^2}{2R_{p0,2}E} + \frac{0,54\Delta a + 0,46(W-a_0)}{0,54(a_0 + \Delta a) + 0,46W} \cdot V_p;$$

- in [Table C.3](#) the small "v" was corrected to capital "V";

- in [Annex D](#), [Formula \(D.7\)](#) was corrected, with the replacement of $1 - \left(\frac{a}{W} \right)^2$ with $\left(1 - \frac{a}{W} \right)^2$, to read:

$$g_4 \left(\frac{a}{W} \right) = \frac{15,8}{\left(1 - \frac{a}{W} \right)^2} \left\{ 0,121 + 1,21 \frac{a}{W} - 0,159 \left(\frac{a}{W} \right)^2 - 1,47 \left(\frac{a}{W} \right)^3 + 1,30 \left(\frac{a}{W} \right)^4 \right\};$$

- in [Annex H](#), [Formula \(H.13\)](#) was corrected, with the replacement of " g_6 " with " g_4 ", to read:

$$\text{coefficient } \lambda = \frac{g_4 \left(\frac{a_0}{W} \right)}{g_4 \left(\frac{a_{0,est}}{W} \right)} \text{ and the function to read: } g_4 \left(\frac{a}{W} \right).$$

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Metallic materials — Unified method of test for the determination of quasistatic fracture toughness

1 Scope

This document specifies methods for determining fracture toughness in terms of K , δ , J and R -curves for homogeneous metallic materials subjected to quasistatic loading. Specimens are notched, precracked by fatigue and tested under slowly increasing displacement. The fracture toughness is determined for individual specimens at or after the onset of ductile crack extension or at the onset of ductile crack instability or unstable crack extension. In cases where cracks grow in a stable manner under ductile tearing conditions, a resistance curve describing fracture toughness as a function of crack extension is measured. In some cases in the testing of ferritic materials, unstable crack extension can occur by cleavage or ductile crack initiation and growth, interrupted by cleavage extension. The fracture toughness at crack arrest is not covered by this document. Special testing requirements and analysis procedures are necessary when testing weldments, and these are described in ISO 15653 which is complementary to this document.

Statistical variability of the results strongly depends on the fracture type, for instance, fracture toughness associated with cleavage fracture in ferritic steels can show large variation. For applications that require high reliability, a statistical approach can be used to quantify the variability in fracture toughness in the ductile-to-brittle transition region, such as that given in ASTM E1921. However, it is not the purpose of this document to specify the number of tests to be carried out nor how the results of the tests are to be applied or interpreted.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3785, *Metallic materials — Designation of test specimen axes in relation to product texture*

ISO 7500-1, *Metallic materials — Calibration and verification of static uniaxial testing machines — Part 1: Tension/compression testing machines — Calibration and verification of the force-measuring system*

ISO 9513, *Metallic materials — Calibration of extensometer systems used in uniaxial testing*

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

3.1

stress intensity factor

K

magnitude of the elastic stress-field singularity for a homogeneous, linear-elastic body

Note 1 to entry: The stress intensity factor is a function of applied force, crack length, specimen size and specimen geometry.